

possible insufficiency in the response and/or the accuracy of the temperature measuring devices or owing to the incomplete sweep of the wiper.

Comparison with the 16 mm pictures of the drop growth process taken simultaneously makes us possible to relate the maximum drop size at each instant with the heat transfer coefficient. A couple of examples are shown in Fig. 5. The curve *a* in the figure corresponds to the result of Fig. 4, while the curve *b* to another measurement. Both examples exhibit rise of the heat transfer coefficient where the maximum diameter is small. Such tendency, however, is not considered to be very reliable, because the accuracy at small maximum drop size is dependent on the accuracy of measurement of the very rapidly changing temperature. The results previously obtained by the authors are also shown in Fig. 5 as a dot-dash line and a two-dots-dash line. The former⁵⁾ corresponds to the relationship between the heat transfer coefficient and the departing drop diameter, which is varied by the vapor shear force, the centrifugal force and the inclination of the condensing surface. The latter⁴⁾ is for the correlation between the heat transfer coefficient and the maximum drop diameter which is controlled by removing the drops on the surface with the wiper.

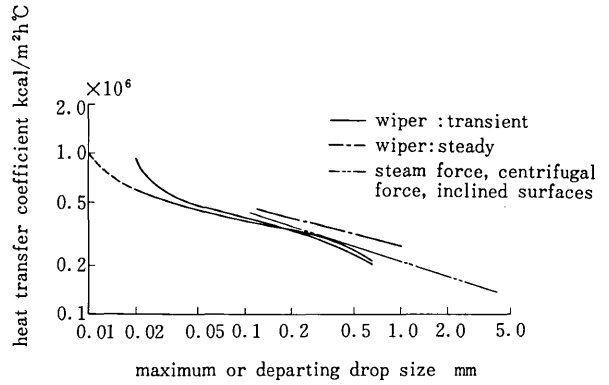


Fig. 5 Heat transfer coefficient and drop size

Although these results seem to exhibit similar tendency, a definite conclusion is not derived for the present. (Manuscript received, February 26, 1976)

References

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- 2) Chiba, Y. et al.: *Kagaku-Kogaku (Chemical Engng.)* (in Japanese), 36 (1972), 412.
- 3) Takeyama, T. and S. Shimizu: *Proc. 5th Int. Heat Transfer Conf.*, Vol. 3 (1974), 255.
- 4) Tanasawa, I. et al.: *Seisan-kenkyu*, 27 (1975), 519.
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正誤表 (4月号)

頁	段	行	種 別	正	誤
25	左	↑ 5	本 文	下段に破線	上段に実線
"	"	↑ 1	"	漸減	漸増
"	"	↑ 1	"	上段に実線	下段に破線
"	右	↑ 7	"	750kg	950kg
"	"	↑ 6	"	破線	実線
"	"	↑ 4	"	50m/secに上昇	40m/secに低下
26	左		図 4	FとVとを入換え	