

*Gravity Survey along the Lines of Precise Levels  
throughout Japan by Means of  
a WORDEN Gravimeter.*

Part VII. Tôhoku District.

By Chuji TSUBOI, Akira JITSUKAWA and Hirokazu TAJIMA,  
Earthquake Research Institute.

(Read Oct. 27, 1953.—Received Sept. 27, 1955.)

CONTENTS

	Page
1. Introduction .....	312
2. Lines of Precise Levels in the Tôhoku District .....	313
3. Methods of Measurements and Reductions .....	316
4. Results .....	316
5. Acknowledgements .....	322
References .....	322
Table I      Number of Gravimeter Stations .....	314
Table II      Apparent Rate of Drift of the Gravimeter Spring for Various Loops .....	317
Table III     Results along the Routes 24 <sub>1</sub> , 24 <sub>2</sub> , 24 <sub>3</sub> , 24 <sub>4</sub> , 24 <sub>5</sub> , 24 <sub>6</sub> , 24 <sub>7</sub> , 24 <sub>8</sub> , 24 <sub>9</sub> , 24 <sub>10</sub> .....	324
Table IV     Results along the Routes 25 <sub>1</sub> , 25 <sub>2</sub> , 25 <sub>3</sub> , 25 <sub>4</sub> , 25 <sub>5</sub> , 25 <sub>6</sub> , 25 <sub>7</sub> , 25 <sub>8</sub> , 25 <sub>9</sub> , 25 <sub>10</sub> , 25 <sub>11</sub> , 25 <sub>12</sub> , 25 <sub>13</sub> , 25 <sub>14</sub> .....	330
Table V      Results along the Routes 26 <sub>1</sub> , 26 <sub>2</sub> , 26 <sub>3</sub> , 26 <sub>4</sub> , 26 <sub>5</sub> , 26 <sub>6</sub> , 26 <sub>7</sub> , 26 <sub>8</sub> , 26 <sub>9</sub> , 26 <sub>10</sub> , 26 <sub>11</sub> , 26 <sub>12</sub> , 26 <sub>13</sub> , 26 <sub>14</sub> , 26 <sub>15</sub> .....	338
Table VI     Results along the Routes 27 <sub>1</sub> , 27 <sub>2</sub> , 27 <sub>3</sub> , 27 <sub>4</sub> , 27 <sub>5</sub> , 27 <sub>6</sub> , 27 <sub>7</sub> .....	349
Table VII    Results along the Route 30 <sub>6</sub> .....	355
Table VIII   Results along the Routes 32 <sub>1</sub> , 32 <sub>2</sub> , 32 <sub>3</sub> , 32 <sub>4</sub> , 32 <sub>5</sub> , 32 <sub>6</sub> , 32 <sub>7</sub> , 32 <sub>8</sub> , 32 <sub>9</sub> , 32 <sub>10</sub> .....	356
Table IX     Results along the Routes 34 <sub>1</sub> , 34 <sub>2</sub> , 34 <sub>3</sub> , 34 <sub>4</sub> , 34 <sub>5</sub> , 34 <sub>6</sub> ..	364
Table X      Synoptic Results for Aomori Prefecture .....	371
Table XI     Synoptic Results for Iwate Prefecture .....	377
Table XII    Synoptic Results for Miyagi Prefecture .....	383
Table XIII   Synoptic Results for Akita Prefecture .....	389
Table XIV    Synoptic Results for Yamagata Prefecture .....	395

Table XV	Synoptic Results for Fukushima Prefecture .....	399
Fig. 1.	Topographical Map of the Tôhoku District.....	313
Fig. 2.	Average Topographical Profile and Average Variation of BOUGUER Anomaly along the EW Cross Section of the Tôhoku District .....	314
Fig. 3.	Lines of Precise Levels in the Tôhoku District with the Prefecture Boundaries.....	315
Fig. 4.	BOUGUER Anomalies in the Tôhoku District Based on the International Formula .....	Pl. XII (in pocket)
Fig. 5.	Simplified Map Showing the BOUGUER Anomaly Distribution in the Tôhoku District .....	319
Fig. 6.	The Morioka-Shirakawa Line .....	320
Fig. 7.	Simple Structure Model of the Tôhoku District .....	320
Fig. 8.	Structure Model of the Tôhoku District as Proposed by the Research Group for Explosion Seismology .....	321
Fig. 9.	Pleistocene and Recent Formation in the Tôhoku District..	321
Fig. 10.	Gravity Stations in Aomori Prefecture .....	Pl. XIII
Fig. 11.	Gravity Stations in Iwate Prefecture .....	Pl. XIV
Fig. 12.	Gravity Stations in Miyagi Prefecture .....	Pl. XV
Fig. 13.	Gravity Stations in Akita Prefecture .....	388
Fig. 14.	Gravity Stations in Yamagata Prefecture .....	394
Fig. 15.	Gravity Stations in Fukushima Prefecture .....	Pl. XVI

## 1. Introduction

Since the spring of 1951, the writers have been engaged in an extensive gravimeter survey along the entire length of the lines of precise levels throughout Japan by means of a WORDEN gravimeter. The network of the lines of precise levels belonging to the Geographical Survey Institute covers the whole country densely as was shown in Fig. 1 of Part I, and it reaches approximately 20,000 km in total length. The bench marks are laid at an average interval of 2 km measured along these level lines. In the present survey, the gravity values have been measured at every other one of these bench marks, that is, at intervals of 4 km. The results of the gravimeter measurements that were obtained in the Shikoku, Chûgoku, Kinki and Chûbu Districts were already published as Pt. I, Pt. II, Pt. III, Pt. V and Pt. VI of these serial reports (TSUBOI et al.: 1953, 1954, 1955). The present report is the seventh in the series and is particularly concerned with the results obtained in the Tôhoku District (TSUBOI et al.: 1953).

## 2. Lines of Precise Levels in the Tōhoku District

Tōhoku District occupies the northernmost part of Honshū, the main island of Japan, as shown in Fig. 1. The District is approximately 200 km wide in the EW direction and 450 km long in the NS directions. It

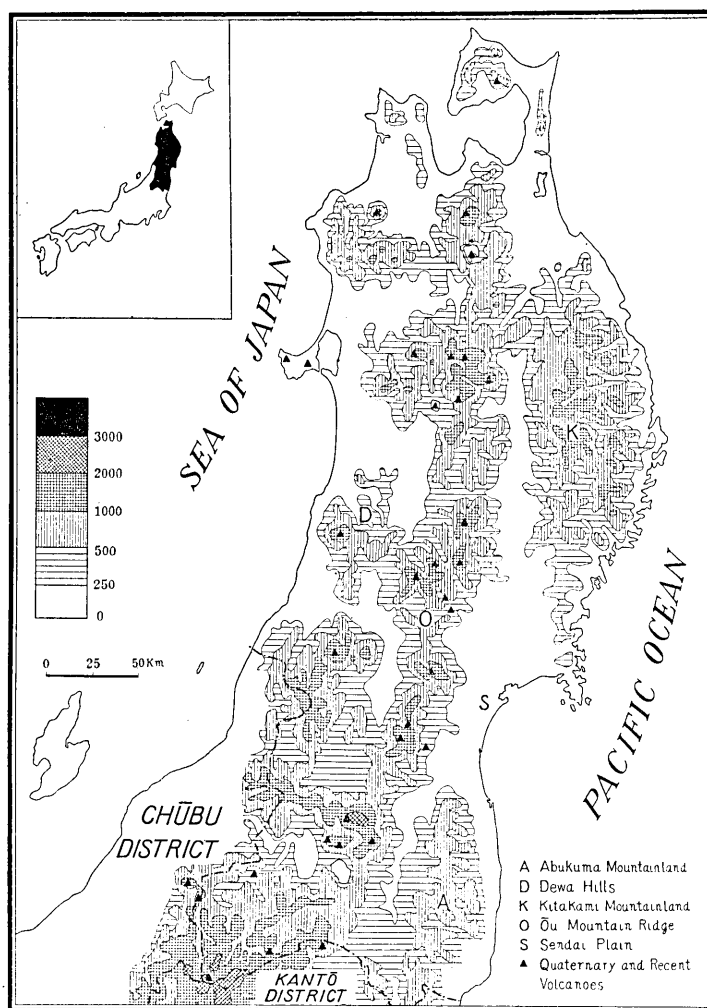


Fig. 1. Topographical Map of the Tōhoku District.

is approximately 67,000 km<sup>2</sup> in area. Fig. 1 also shows the topography of the District. Topographically, the District has longitudinal features consisting of three systems of mountain zones as can be seen from the

map in Fig. 1. Fig. 2 shows the average topographical profile of the District taken in the EW direction. On the easternmost or the Pacific zone, there are Kitakami and Abukuma mountainlands, which are built chiefly of Palaeozoic formations and granites intruding them and which are apparently separated by a terrain of Tertiary and Quaternary formations including a plain around Sendai. The Ôu mountains which form the central backbone zone of the District exceed 1,000 m in height at many places and are a system of Tertiary block mountains with numerous volcanoes which have erupted through them. The westernmost zone, Dewa Hills, is made up of thick and folded Tertiary formations. Along this zone also are situated many volcanoes.

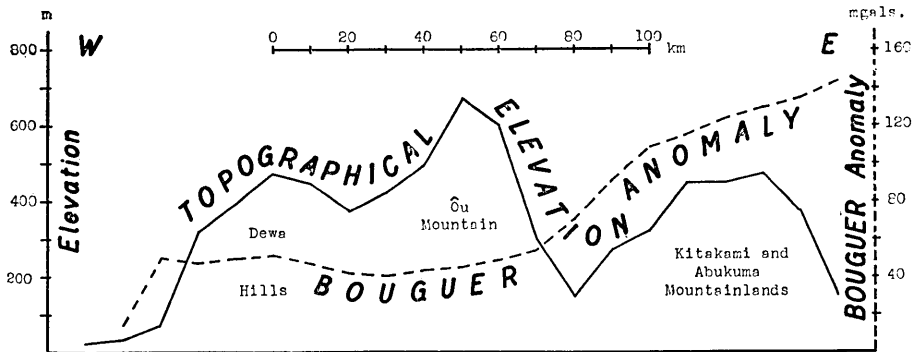


Fig. 2. Average Topographical Profile and Average Variation of BOUGUER Anomaly along the EW Cross Section of the Tôhoku District.

The Tôhoku District comprises six administrative prefectures, viz.,

Table I.  
Number of Gravimeter Stations.

Prefecture	Number
(1) Aomori	122
(2) Iwate	130
(3) Miyagi	85
(4) Akita	106
(5) Yamagata	81
(6) Fukushima	143
Total	667

(1) Aomori, (2) Iwate, (3) Miyagi, (4) Akita, (5) Yamagata and (6) Fukushima. The networks of the lines of precise levels in this district, along which the gravity values were measured, are shown in Fig. 3 together with the prefecture boundaries. The lines are altogether about 2,500 km in length, and at 667 points along them, the gravity values were determined. In this number are also included several identifiable points, such as local weather stations, of which the altitudes are known with sufficient accuracy for the purpose of our gravity reductions. The number of points at which the gravity values

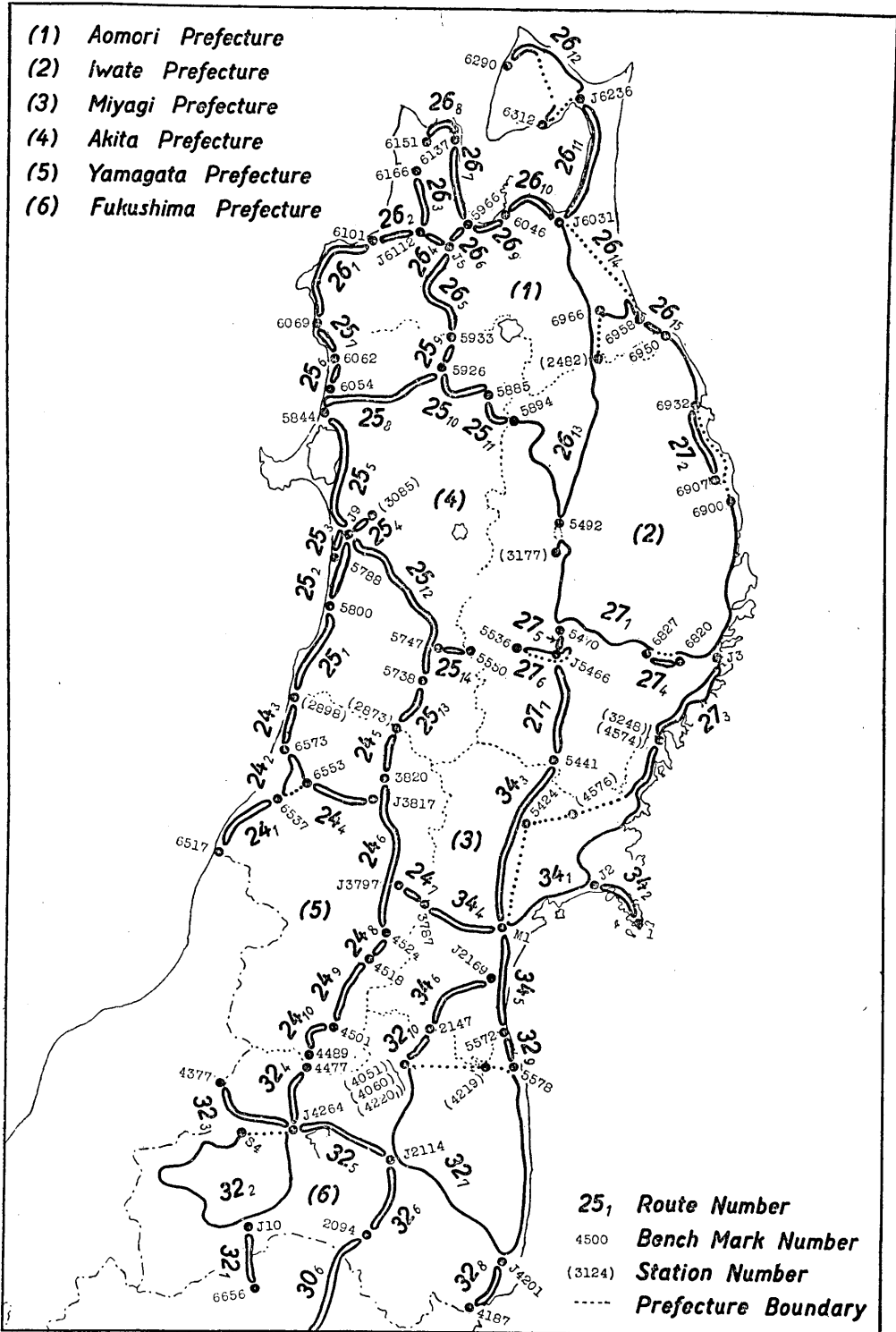


Fig. 3. Lines of Precise Levels in the Tohoku District with the Prefecture Boundaries.

were determined in each of the six prefectures is given in Table I.

The gravimeter survey in this District was made in various periods, namely in September, November and December, 1952, and in July, August and September, 1953.

### 3. Methods of Measurements and Reductions

Since the methods of measurements and reductions are the same as those already stated in previous reports, no repeated description will be necessary, nor further comments need be added. The one important thing which must be mentioned is that no attempt has been made here, as in the previous reports, to adjust the measured gravity values by simultaneous net calculations. Actually, the whole length of the lines of measurements is a connected chain consisting of a number of small gravimetric loops, for each of which the drift rate of the gravimeter spring was determined severally. These small loops are numbered as illustrated in Fig. 3. After the relative gravity values at the sites of bench marks situated along each one of the loops were determined separately, the results were merely connected in succession. This procedure is admittedly not a kind from which very accurate results can be expected, but unavoidable circumstances regarding transportation facilities on the one hand and the rather hastily demand for getting a picture of the distribution of the gravity anomalies on the other, have made us adopt this procedure as the second best. Although we do not claim that the results given in this report are of the highest attainable accuracy, it is not likely that any difference in the procedure of reduction will alter sensibly the final results. It is of course our wish to make a simultaneous net adjustment when the survey over the whole country is completely finished.

Our WORDEN gravimeter has been working with admirable perfection, only the rate of drift of the gravimeter spring differed sensibly from one loop to another. It will be interesting to compare the rate for each of the loops given in Table II.

### 4. Results

The gravity values at all the stations in this District are given in Tables III~IX for each of the loops separately. In Tables X~XV, the materials are arranged synoptically according to the six prefectures of the District separately. The explanation of the tables precedes them. The lines of equal BOUGUER anomalies based on the International Gravity

Table II. Apparent Rate of Drift of the Gravimeter Spring for Various Loops.

Route	Residual (0.01 mgal.)	Time (hour)	R (mgal./hour)
24 <sub>1</sub>	33	5.0	0.0660
24 <sub>2</sub>	22	4.2	0.0524
24 <sub>3</sub>	28	4.1	0.0683
24 <sub>4</sub>	17	3.0	0.0567
24 <sub>5</sub>	30	6.1	0.0492
24 <sub>6</sub>	28	8.9	0.0315
24 <sub>7</sub>	15	2.1	0.0714
24 <sub>8</sub>	26	1.5	0.1733
24 <sub>9</sub>	16	3.3	0.0485
24 <sub>10</sub>	8	4.7	0.0170
25 <sub>1</sub>	1	5.6	0.0018
25 <sub>2</sub>	6	2.3	0.0261
25 <sub>3</sub>	35	4.3	0.0814
25 <sub>4</sub>	23	5.5	0.0418
25 <sub>5</sub>	62	6.7	0.0925
25 <sub>6</sub>	8	1.6	0.0500
25 <sub>7</sub>	14	2.2	0.0636
25 <sub>8</sub>	33	9.4	0.0351
25 <sub>9</sub>	- 2	1.2	-0.0167
25 <sub>10</sub>	20	2.6	0.0769
25 <sub>11</sub>	16	3.7	0.0432
25 <sub>12</sub>	26	9.8	0.0265
25 <sub>13</sub>	31	3.9	0.0795
25 <sub>14</sub>	9	2.2	0.0409
26 <sub>1</sub>	60	9.8	0.0612
26 <sub>2</sub>	24	3.5	0.0686
26 <sub>3</sub>	30	4.1	0.0732
26 <sub>4</sub>	26	2.9	0.0897
26 <sub>5</sub>	46	3.5	0.1314
26 <sub>6</sub>	-10	3.6	-0.0278
26 <sub>7</sub>	25	4.6	0.0544
26 <sub>8</sub>	53	6.3	0.0841
26 <sub>9</sub>	37	3.0	0.1233
26 <sub>10</sub>	30	4.5	0.0667
26 <sub>11</sub>	56	7.9	0.0709
26 <sub>12</sub>	98	16.7	0.0587
26 <sub>13</sub>	198	19.5	0.1015
26 <sub>14</sub>	17	6.0	0.0283
26 <sub>15</sub>	22	2.2	0.1000
27 <sub>1</sub>	27	31.1	0.0087
27 <sub>2</sub>	- 32	8.6	-0.0372
27 <sub>3</sub>	12	14.4	0.0083
27 <sub>4</sub>	- 8	1.8	-0.0444
27 <sub>5</sub>	- 7	1.2	-0.0583
27 <sub>6</sub>	4	2.3	0.0174
27 <sub>7</sub>	39	6.2	0.0629
30 <sub>6</sub>	43	8.2	0.0524
32 <sub>1</sub>	42	3.4	0.1235
32 <sub>2</sub>	145	14.0	0.1036
32 <sub>3</sub>	129	13.3	0.0970
32 <sub>4</sub>	33	3.6	0.0917
32 <sub>5</sub>	84	6.9	0.1217
32 <sub>6</sub>	67	5.8	0.1155

(to be continued.)

Table II. (Continued.)

Route	Residual (0.01 mgal.)	Time (hour)	$R$ (mgal./hour)
32 <sub>7</sub>	154	18.3	0.0842
32 <sub>8</sub>	41	3.5	0.1171
32 <sub>9</sub>	5	1.2	0.0417
32 <sub>10</sub>	38	2.6	0.1462
34 <sub>1</sub>	144	25.9	0.0556
34 <sub>2</sub>	67	11.3	0.0593
34 <sub>3</sub>	48	7.6	0.0632
34 <sub>4</sub>	32	6.0	0.0533
34 <sub>5</sub>	48	5.1	0.0941
34 <sub>6</sub>	30	5.6	0.0536

Formula are shown in Fig. 4 with 2 mgal. intervals. The figure is in the pocket attached to the back cover of the present report. The locations of the contour lines are accurate where they meet the lines of precise levels, but obviously no great accuracy can be claimed for those in the intervenient parts. It may be noticed in several parts in Fig. 4 that, from the given data alone, the contour lines can hardly be drawn as they are actually. This is due to the fact that there are here many points which we could not visit and at which the gravity values were determined later by the teams sent from the Geographical Survey Institute and that we have taken the results of these measurements into consideration also. Such points are marked differently in Fig. 4. Fig. 5 is a simplified map showing the same distribution with 5 mgal. intervals.

Reserving the detailed and quantitative geophysical interpretations of the distribution of the BOUGUER anomalies for future studies, we will briefly enumerate the especially notable facts found in Figs. 4 and 5.

1) The Tôhoku District, as a whole, is characterised by exclusively positive BOUGUER anomalies. There is no area in this district at which the BOUGUER anomaly is negative, except for an insignificantly small area near the southern boundary of the district. This would mean that, in this District, the denser subcrustal material lies much closer to the earth's surface than in any other district where the anomalies are evenly positive and negative. In other words, the earth's crust is thin here. It is already a well-known fact that P-waves of deep-seated earthquakes near Japan arrive one second or so too early in the Tôhoku District. This may also be accounted for by the said thinness of the earth's crust in this District.

2) As can be seen in Figs. 4 and 5 and also in Fig. 2 which shows the average variation of  $\Delta g_0''$  along the EW cross section of the District,



the anomaly increases towards east. To be precise, however, the increase is not uniform. In the western two-thirds of the cross section, the anomaly is more or less constant. It increases remarkably across the low lands lying between the middle and eastern mountain zones. The horizontal gradient of gravity reaches about  $20 \times 10^{-9}$  C.G.S. here on the

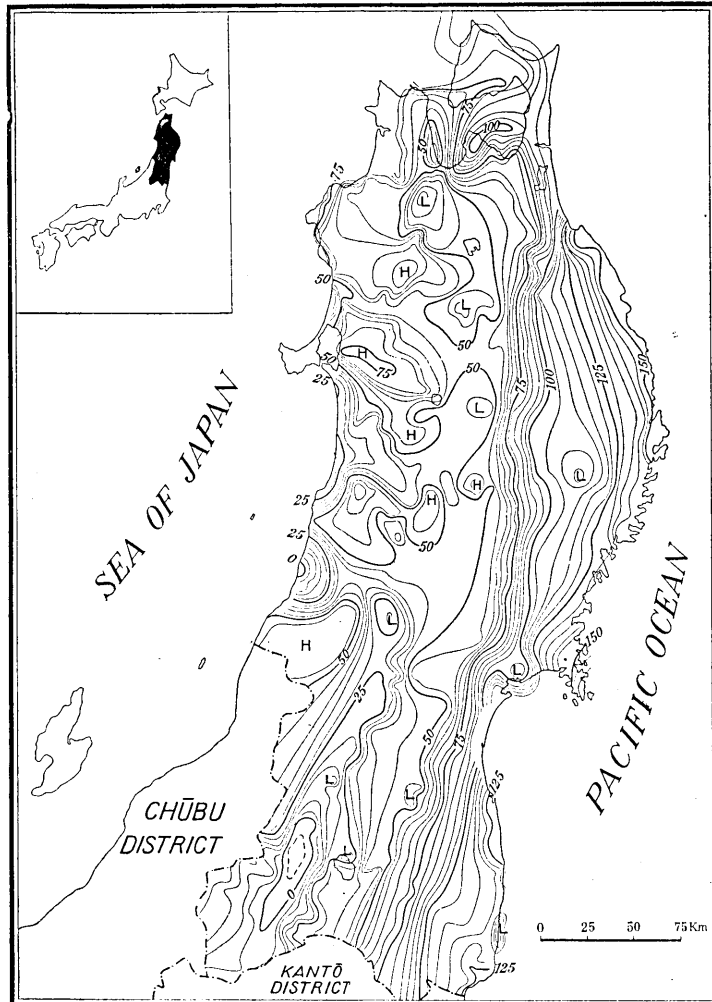


Fig. 5. Simplified Map Showing the BOUGUER Anomaly Distribution in the Tōhoku District.

average. In the area to the east of this line of the steepest increase, the isoanomaly lines are nearly parallel with each other and the anomaly increases eastwards gently. As will be stated in the next number of

the series, this line of the steepest slope of gravity anomaly runs still southwards into the Kantô District at about the middle of which, it bends sharply to east as shown in Fig. 6.

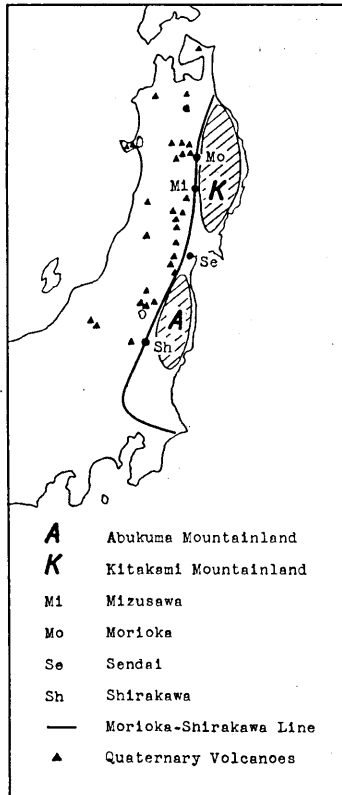


Fig. 6. The Morioka-Shirakawa Line.

This important line will be referred to as the "Morioka-Shirakawa Line" after the names of the two cities which are situated on it. There can be a number of explanations which will account for the steep slope of gravity anomaly across this Morioka-Shirakawa Line. One of the simplest solutions will be to assume a sudden change in the thickness of the earth's crust across this line as shown in Fig. 7. If the average anomalies on both sides of the line are assumed to differ by 70 mgals., and the average densities of the crustal and subcrustal materials to differ by 0.4, the difference in the thickness of the earth's crust on both sides of this line will be 6-7 km. Of course, this is not the only possible solution, nor have the writers the intention to insist that this is the most probable solution. In fact, the Research Group for Explosion Seismology, Japan (1952), which has made several explosion experiments near the area in question, proposes another solution by which not only the observed

time-distance relation of explosion seismic waves, but also the distribution of gravity anomalies can be explained. The model is shown in Fig. 8.

It is interesting to observe that the Quaternary volcanoes in this district are located only on the west side of the Morioka-Shirakawa Line and are arranged in two rows parallel to the Morioka-Shirakawa Line. The eastern row which is usually called the Nasu volcanic zone, keeps an almost uniform distance of about

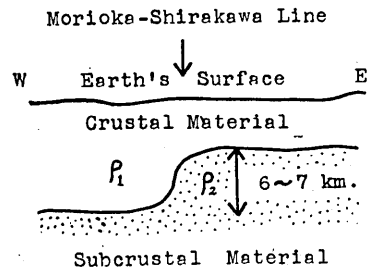


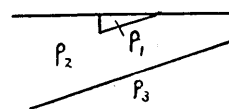
Fig. 7. Simple Structure Model of the Tōhoku District.

30 km from the line as shown in Fig. 6. It is also important to note that "conspicuous" and "rather conspicuous" earthquakes of shallow origin in and near the Tôhoku District occur almost exclusively on the east side of this Morioka-Shirakawa Line. At Mizusawa International Latitude Observatory, which is situated on or very close to the Morioka-Shirakawa Line, the fact has long been noted that earthquake waves coming from east and west are of remarkably different forms; the former being rich in short period vibrations which are lacking in the latter. At any rate, the Morioka-Shirakawa Line is of an important geophysical significance and deserves a further study.

The fact that the Morioka-Shirakawa Line runs along the western margins of the two mountainlands, Kitakami and Abukuma, and that the isoanomaly lines are nearly



Fig. 9. Pleistocene and Recent Formations in the Tôhoku District.



$$P_1 < P_2 < P_3$$

Fig. 8. Structure Model of the Tôhoku District as Proposed by the Research Group for Explosion Seismology.

parallel to each other on the east side of that line, all running in the NS direction, suggest that the two mountainlands are structurally continuous, although they are apparently separated by the Sendai Plain.

3) In the area to the west of the Morioka-Shirakawa Line the isoanomaly lines are irregularly curved, in contradistinction to the nearly straight isoanomaly lines in the area to the east of it. Geologically, these western zones are characterised by thick Tertiary formations which are developed only poorly in the east zone. The irregularities in the trend of the isoanomaly lines in the western zones are mostly due to the existence of several local gravity minima in patches. Each of these minima corresponds to a small basin consisting geologically of young formations and this is undoubtedly related to

the lower densities of the materials lying near the surface of the basins.

In the east zone, on the other hand, no such gravity minimum can be found except the one near Sendai. This again corresponds to the young formations lying between the Kitakami and Abukuma mountainlands.

In the northernmost part of the District, the lines of equal BOUGUER anomalies are apparently irregular. Among the irregularities, the eastward bulge of the gravity low appears to be due to the light young deposits lying at that place.

Fig. 9 shows the distribution of Pleistocene and Recent geological formations in the Tôhoku District. When compared with Fig. 4 or 5, the correspondence of gravity minima in this district to these young formations is remarkable. If we could correct the anomaly values by eliminating the effects of these young deposits with lower densities, the results obtained would serve as a useful clue for clarifying the deeper-seated and perhaps simpler structure of the earth's crust in this District. Particularly, after these corrections, the eastward bulge of the gravity low in the northernmost part would disappear and the parallel and narrowly spaced isoanomaly lines existing to the south of it would be seen running northwards still farther.

### 5. Acknowledgements

The writers cannot close this report without expressing their grati- tudes to the many officials and individuals who helped them in various ways in accomplishing this survey. It is practically impossible to mention the name of all these persons. Particularly the writers wish to thank Mrs. S. INOUE and Miss K. SEKI who have helped the writers greatly in numerical computations and in preparing the present report. A part of the expense necessary for this survey was defrayed from the Grant in Aid of Scientific Research from the Ministry of Education.

### References

Research Group for Explosion Seismology:

1952 "Crustal Structure of the Southern Tôhoku District."

Report of the Research Group for Explosion Seismology, No. 10.

TSUBOI, C., et al.:

1953 "Gravity Measurements along the Lines of Precise Levels over Whole Japan by Means of a WORDEN Gravimeter. IV. Tôhoku District."

Proc. Japan Acad., **29**, 503.

"Gravity Survey along the Lines of Precise Levels throughout Japan by Means of a WORDEN Gravimeter. Part I. Shikoku District."

- Bull. Earthq. Res. Inst., Suppl. Vol., IV, Part I.
- 1954 "Gravity Survey along the Lines of Precise Levels throughout Japan by Means of a WORDEN Gravimeter. Part II. Chûgoku District."  
 ibid., Part II.  
 "Supplement to the Previous Report of the Gravity Survey in Shikoku."  
 ibid., Part II.  
 "Gravity Survey along the Lines of Precise Levels throughout Japan by Means of a WORDEN Gravimeter. Part V. Kinki District."  
 ibid., Part IV.
- 1955 "Gravity Survey along the Lines of Precise Levels throughout Japan by Means of a WORDEN Gravimeter. Part VI. Chûbu District."  
 ibid., Part V.

### Explanation of Tables

#### Tables III-IX Results along Each of the Routes

Pref. ....	Prefecture
No. ....	Number of Measurement
B.M. ....	Bench Mark Number
Time .....	Time of Measurement
$\Sigma \delta T$ .....	Net Time needed to arrive at the Station from the Starting Point
<i>LD</i> .....	Large Dial Reading
<i>SD</i> .....	Small Dial Reading
$0.9150 \times SD$ ...	Conversion of Small Dial Reading to 0.01 mgal.
<i>h</i> .....	Height of the Gravimeter above the Bench Mark Head
$0.3086 \times h$ ...	Free-air Reduction to the Bench Mark Head
<i>E.T.</i> .....	Correction for the Earth Tides (Factor 1.20)
Drift .....	Correction for Drift
$\Sigma \delta g$ .....	Gravity Difference from the Starting Point
<i>g</i> .....	Gravity Value (Corrected for Drift and Earth Tides)

#### Tables X-XV Synoptic Results for Each of the Prefectures

$\varphi$ .....	Latitude
$\lambda$ .....	Longitude
<i>H</i> .....	Height of the Bench Mark above the Sea Level
<i>g</i> .....	Gravity Value (Corrected for Drift and Earth Tides)
$g_0$ .....	Gravity Value after the Free-air Reduction
$g_0''$ .....	Gravity Value after the BOUGUER Reduction
$\gamma$ .....	Normal Gravity
$\Delta g_0$ .....	Free-air Anomaly
$\Delta g_0''$ .....	BOUGUER Anomaly

Table III. Results along the Route 24. (0.01 m gal.).  
Route 24<sub>1</sub> B.M. 6537—B.M. 6517—B.M. 6537.

Pref.	No.	B.M.	Date 1952	Time	$\Sigma\delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$6.60 \times \Sigma\delta T$ Drift	$\Sigma\delta g$	$g$ 980.	Field Note No.
5	2904	6537	XI 8	14 48	0 00	5894	5393	36	11	- 4	0	0	10162	60
"	2905	6535	"	14 57	9	6115	5595	64	20	- 4	1	210	10372	"
"	2906	6533	"	15 10	22	6242	5711	36	11	- 4	3	315	10477	"
"	2907	6530	"	15 27	39	6586	6026	51	16	- 4	5	633	10795	"
"	2908.1		"	15 41	53	6547	5991	—	—	- 4	6	581	10743	"
"	2908.2		"	15 43		3574	3270	—	—	- 4				"
"	2909	6526	"	16 04	1 14	3949	3613	64	20	- 4	8	942	11104	"
"	2910	6524	"	16 16	1 26	3982	3644	47	15	- 4	9	967	11129	"
"	2911	6522	"	16 35	1 45	3838	3512	57	18	- 4	12	835	10997	61
"	2912	6519	"	16 56	2 06	3396	3107	36	11	- 4	14	421	10583	"
"	2913	6517	"	17 11	2 21	3323	3041	59	18	- 4	16	360	10522	"
"	2914	6522	"	17 44	2 54	3848	3521	56	17	- 4	19	836	10998	"
"	2915	"	XI 9	9 34		3941	3606	"	"	- 2				"
"	2916	6537	"	11 40	5 00	3053	2793	36	11	- 5	33	0	10162	"

Route 24<sub>2</sub> B.M. 6573—B.M. 6537—B.M. 6553—B.M. 6573.

Pref.	No.	B.M.	Date 1952	Time	$\Sigma\delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$5.24 \times \Sigma\delta T$ Drift	$\Sigma\delta g$	$g$ 980.	Field Note No.
5	2899	6573	XI 8	13 02	0 00	0485	0444	63	19	- 5	0	0	08463	60
"	2900.1	6546	"	13 43	41	0883	0808	52	16	- 5	4	357	08620	"
"	2900.2	"	"	13 46	"	4418	4042	"	"	- 5	"	"	"	"
"	2901	6544	"	14 00	55	4085	3738	47	15	- 5	5	51	08514	"
"	2902	6542	"	14 12	1 07	4237	3877	52	16	- 5	6	190	08653	"

2903	6540	"	14 25	1 20	4653	4257	38	12	5	7	565	09028	"
"	6537	"	14 48	1 43	5894	5393	36	11	- 4	9	1699	10162	"
"	"	XI 9	11 40	2 33	3053	2793	"	"	- 5	14	692	09155	61
"	6553	"	12 30	2 33	1951	1785	58	18	- 6				"
"	"	XI 7	17 29		4189	3833	62	19	- 6				60
2884	6551	"	17 41	2 45	4057	3712	62	19	- 6	15	570	09033	"
2885	6548	"	18 15	3 19	4039	3696	67	21	- 6	17	554	09017	"
2886	6571	"	18 33	3 37	3295	3015	42	13	- 6	19	-137	08326	"
2887	6573	"	19 09	4 13	3445	3152	52	16	- 6	22	0	08463	"

Route 24 <sub>3</sub> B.M. 6573—Prefecture Boundary (No. 2898)—B.M. 6573.														
5	2890	6573	Date	Time	$\sum \delta T$	SD	$0.9150 \times SD$	h	$0.3086 \times h$	E.T.	$6.83 \times \sum \delta T$	$\sum \delta g$	g	Field Note No.
"	2891	6575	XI 8	8 50	0 00	3521	3222	57	18	- 2	0	0	08463	60
"	2892	6577	"	9 16	0 26	4027	3685	63	19	- 2	3	461	08924	"
"	2893	6579	"	9 30	0 40	4490	4108	41	13	- 4	5	874	09337	"
"	2894	6581	"	9 40	0 50	5333	4880	57	18	- 4	8	1651	10114	"
"	2895-1	6582	"	9 53	1 03	6045	5531	62	19	- 4	8	2300	10763	"
"	2895-2	"	"	10 15	1 25	7054	6454	47	15	- 4	10	3217	11680	"
"	2896	6583	"	10 21	1 34	3985	3646	"	"	- 4	11	4064	12527	"
"	2897	6585	"	10 31	1 50	4915	4497	41	13	- 5	12	4774	13237	"
"	2898	P.B.*	"	10 46	2 20	5690	5206	50	15	- 5	16	5190	13653	"
"	2899	6573	"	11 16	4 06	6142	5620	68	21	- 5	28	0	08463	"
"	2899	6573	"	13 02	4 06	0485	0444	63	19	- 5	28	0	08463	"

\* Prefecture Boundary.

Route 24<sub>4</sub> B.M.J. 3817—B.M. 6553—B.M.J. 3817.

Pref.	No.	B.M.	Date 1952	Time	$\Sigma\delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$5.67 \times \Sigma\delta T$ Drift	$\Sigma\delta g$	$g$ 980.	Field Note No.
5	2875	J. 3817	XI 7	15 36	0 00	3945	3610	63	19	5	0	0	07429	60
"	2876	6568	"	15 52	16	4597	4206	51	16	5	2	591	08020	"
"	2877 <sub>-1</sub>	6566	"	16 04	28	7209	6596	63	19	5	3	2983	10412	"
"	2877 <sub>-2</sub>	"	"	16 06	"	2228	2039	"	"	5	"	"	"	"
"	2878	6563	"	16 21	43	3456	3162	69	21	5	4	4107	11536	"
"	2879	6561	"	16 34	56	3606	3299	59	18	6	5	4239	11668	"
"	2880	6559	"	16 46	1 08	3704	3389	64	20	6	6	4330	11759	"
"	2881	6557	"	17 00	1 22	2999	2744	65	20	6	8	3683	11112	"
"	2882	6555	"	17 13	1 35	1694	1550	62	19	6	9	2487	09916	"
"	2883 <sub>-1</sub>	6553	"	17 26	1 48	0863	0790	62	19	6	10	1726	09155	"
"	2917	"	XI 9	12 30	3 01	1951	1785	58	18	6	17	0	07429	61
"	2918 <sub>-1</sub>	J. 3817	"	13 43	"	0072	0066	57	18	6	"	"	"	"

Route 24<sub>5</sub> B.M. 3820—Okachi Pass (No. 2873)—B.M. 3820.

Pref.	No.	B.M.	Date 1952	Time	$\Sigma\delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$4.92 \times \Sigma\delta T$ Drift	$\Sigma\delta g$	$g$ 980.	Field Note No.
5	2865	3820	XI 7	8 47	0 00	3924	3590	57	18	5	0	0	07440	60
"	2866	5712	"	8 57	10	4746	4343	67	21	5	1	755	08195	"
"	2867	5714	"	9 07	20	5672	5190	55	17	5	1	1598	09038	"
"	2868	5716	"	9 42	55	4201	3844	60	19	6	4	250	07690	"
"	2869	5718	"	10 00	1 13	6337	5798	48	15	6	6	2198	09638	"
"	2870	5720	"	10 19	1 32	6032	5519	67	21	6	7	1924	09364	"
"	2871	5722	"	10 56	2 09	3513	3214	49	15	6	11	391	07049	"
"	2872	5724	"	11 32	2 45	5867	5368	69	21	5	14	1767	09207	"
5-4	2873	Okachi Pass P.B.*	"	12 08	3 21	2354	2154	70	22	5	17	1449	05991	"
4	2874	3820	"	14 55	6 08	3954	3618	60	19	4	30	0	07440	"

\* Okachi Pass Prefecture Boundary.



Gravity Survey along the Lines of Precise Levels.

Route 24<sub>6</sub> B.M. 3820—B.M.J. 3817—B.M. 4524—B.M.J. 3797—B.M. 3820.

Pref.	No.	B.M.	Date 1952	Time <sup>h. m.</sup>	$\Sigma \delta T$ <sup>h. m.</sup>	SD	$0.9150 \times$ SD	<i>h</i> (cm)	$0.3086 \times$ <i>h</i>	<i>E.T.</i>	$3.15 \times$ $\Sigma \delta T$ Drift	$\Sigma \delta g$	<i>g</i> 980.	Field Note No.
5	2874	3820	XI 7	14 55	0 00	3954	3618	60	19	4	0	0	07440	60
"	2875	J. 3817	"	15 36	41	3945	3610	63	19	5	2	11	07429	"
"	2918.2	"	XI 9	13 50		7759	7099	57	18	6				61
"	2919	4524	"	16 18	3 09	2523	2309	56	17	4	10	-4808	02632	"
"	2840	"	XI 6	9 27		5437	4975	57	18	7				59
"	2841	4526	"	9 50	3 32	6196	5669	75	23	7	11	-4110	03330	"
"	2842	4528	"	10 01	3 43	6487	5936	71	22	7	12	-3845	03595	"
"	2843.1	4529	"	10 27	4 09	6776	6200	79	24	7	13	-3580	03860	"
"	2843.2	"	"	10 29		1992	1823	"	"	7				"
"	2844	4531	"	10 42	4 22	3825	3500	62	19	6	14	-1908	05532	"
"	2845	4533	"	11 11	4 51	2746	2513	80	25	6	15	-2890	04550	"
"	2846	J. 3797	"	11 22	5 02	3800	3477	42	13	6	16	-1939	05501	"
"	2853	"	"	13 32		1654	1513	41	13	4				60
"	2854	3799	"	14 37	6 07	3140	2873	66	20	5	19	-576	06864	"
"	2855	3802	"	14 52	6 22	2519	2305	35	11	5	20	-1154	06286	"
"	2856	3804	"	15 03	6 33	2616	2394	70	22	5	21	-1055	06385	"
"	2857	3806	"	15 14	6 44	2742	2509	49	15	5	21	-947	06493	"
"	2858	3808	"	15 25	6 55	2619	2396	68	21	5	22	-1055	06385	"
"	2859	3810	"	15 38	7 08	3317	3035	69	21	6	22	-417	07023	"
"	2860	3812	"	15 51	7 21	1782	1631	50	15	6	23	-1828	05612	"
"	2861	3814	"	16 08	7 38	3136	2869	72	22	6	24	-584	06856	"
"	2862	3816	"	16 20	7 50	3256	2979	54	17	6	25	-480	06960	"
"	2863	3818	"	17 03	8 33	3831	3505	51	16	6	27	43	07483	"
"	2864	3820	"	17 21	8 51	3781	3460	61	19	6	28	0	07440	"

Route 247 B.M.J. 3797—B.M. 3787—B.M.J. 3797.

Pref.	No.	B.M.	Date	Time	$\sum \delta T$	$SD$	$\frac{0.9150}{SD} \times h$	$h$	$0.3086 \times h$	$E.T.$	$\frac{7.14 \times \sum \delta T}{\text{Drift}}$	$\sum \delta g$	$g$	Field Note No.
5	2846	J. 3797	XI 6	11 22	0 00	3800	3477	42	13	6	0	0	05501	59
"	2847	"	"	11 36	14	2491	2279	52	16	5	1	-1195	04306	"
"	2848	"	"	11 49	27	2035	1862	57	18	5	4	-1613	03888	"
"	2849-1	"	"	12 00	38	2219	2030	63	19	5	4	-1444	04057	"
"	2849-2	"	"	12 03		7563	6920	"	"	5				"
"	2850	3789	"	12 17	52	5501	5033	39	12	5	6	-3340	02161	"
"	2851	3787	"	12 32	1 07	0664	0608	39	12	4	8	-7766	97735	60
"	2852-1	3791	"	13 01	1 36	7580	6936	62	19	4	11	-1434	04067	"
"	2852-2	"	"	13 04		0075	0069	"	"	4				"
"	2853	J. 3797	"	13 32	2 04	1654	1513	41	13	4	15	0	05501	"

Route 248 B.M. 4524—B.M. 4518—B.M. 4524.

Pref.	No.	B.M.	Date	Time	$\sum \delta T$	$SD$	$\frac{0.9150}{SD} \times h$	$h$	$0.3086 \times h$	$E.T.$	$\frac{17.33 \times \sum \delta T}{\text{Drift}}$	$\sum \delta g$	$g$	Field Note No.
5	2817	4524	XI 5	9 19	0 00	4049	3705	57	18	8	0	0	02632	59
"	2818	4522	"	9 45	26	3535	3235	57	18	6	7	-475	02157	"
"	2819	4520	"	9 57	38	3977	3639	56	17	6	10	-75	02557	"
"	2820	4518	"	10 08	49	3459	3165	57	18	6	14	-552	02080	"
"	2839	"	XI 6	8 46		4821	4411	58	18	7				"
"	2840	4524	"	9 27	1 30	5437	4975	57	18	7	26	0	02632	"

Route 24<sub>9</sub> B.M. 4518—B.M. 4501—B.M. 4518.

Pref.	No.	B.M.	Date 1952	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$4.85 \times \Sigma \delta T$ Drift	$\Sigma \delta g$	$g$ 980.	Field Note No.
5	2820	4518	XI 5	<sup>h</sup> 10 08	<sup>m</sup> 0 00	3459	3165	57	18	- 6	0	0	02080	59
"	2821	4516	"	<sup>h</sup> 10 20	<sup>m</sup> 12	3077	2815	64	20	- 6	1	- 349	01731	"
"	2822	4514	"	<sup>h</sup> 10 30	<sup>m</sup> 22	1650	1510	56	17	- 5	2	- 1657	00423	"
"	2823-1	4512	"	<sup>h</sup> 11 05	<sup>m</sup> 57	0323	0296	55	17	- 5	5	- 2874	979	"
"	2823-2	"	"	<sup>h</sup> 11 07	<sup>m</sup>	7391	6763	"	"	- 5			99206	"
"	2824	4510	"	<sup>h</sup> 11 20	<sup>m</sup> 1 10	5389	4931	34	10	- 5	6	- 4714	97366	"
"	2825	4507	"	<sup>h</sup> 11 38	<sup>m</sup> 1 28	6753	6179	45	14	- 4	7	- 3462	98618	"
"	2826	4505	"	<sup>h</sup> 11 51	<sup>m</sup> 1 41	6917	6329	63	19	- 4	8	- 3308	98772	"
"	2827	4503	"	<sup>h</sup> 12 02	<sup>m</sup> 1 52	6845	6263	65	20	- 4	9	- 3374	98706	"
"	2828	4501	"	<sup>h</sup> 12 14	<sup>m</sup> 2 04	5867	5368	54	17	- 4	10	- 4273	97807	"
"	2837-2	"	"	<sup>h</sup> 17 09	<sup>m</sup>	0056	0051	52	16	- 7			980	"
"	2838	4518	"	<sup>h</sup> 18 21	<sup>m</sup> 3 16	4730	4328	61	19	- 8	16	0	02080	"

Route 24<sub>0</sub> B.M. 4501—B.M. 4489—B.M. 4501.

Pref.	No.	B.M.	Date 1952	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$1.70 \times \Sigma \delta T$ Drift	$\Sigma \delta g$	$g$ 979.	Field Note No.
5	2828	4501	XI 5	<sup>h</sup> 12 14	<sup>m</sup> 0 00	5867	5368	54	17	- 4	0	0	97807	59
"	2829	4499	"	<sup>h</sup> 13 43	<sup>m</sup> 1 29	4230	3870	62	19	- 4	3	- 1499	96308	"
"	2830-1	4497	"	<sup>h</sup> 13 55	<sup>m</sup> 1 41	1270	1162	60	19	- 4	3	- 4207	93600	"
"	2830-2	"	"	<sup>h</sup> 13 57	<sup>m</sup>	7693	7039	"	"	- 4				"
"	2831	4494	"	<sup>h</sup> 14 12	<sup>m</sup> 1 56	6708	6138	70	22	- 4	3	- 5105	92702	"
"	2832	4491	"	<sup>h</sup> 14 49	<sup>m</sup> 2 33	4112	3762	55	17	- 5	4	- 7488	90319	"
"	2833-1	4490	"	<sup>h</sup> 15 13	<sup>m</sup> 2 57	2791	2554	73	23	- 5	5	- 8691	89116	"
"	2833-2	"	"	<sup>h</sup> 15 15	<sup>m</sup>	7517	6878	"	"	- 5				"
"	2834-1	4489	"	<sup>h</sup> 15 33	<sup>m</sup> 3 15	5703	5218	64	20	- 6	6	- 10356	87451	"
"	2834-2	"	"	<sup>h</sup> 15 35	<sup>m</sup>	0083	0076	"	"	- 6				"

Table III. (Continued)

Pref.	No.	B.M.	Date 1952	Time	$\Sigma\delta T$	SD	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	E.T.	$1.70 \times \Sigma\delta T$ Drift	$\Sigma\delta g$	$g$ 979.	Field Note No.
5	2835 <sub>1</sub>	4497	XI 5	<sup>h</sup> <sub>m</sub> 16 32	<sup>h</sup> <sub>m</sub> 4 12	6809	6230	59	18	7	7	-4206	93601	59
"	2835 <sub>2</sub>	"	"	16 35	0193	0177	"	"	"	7	7	-1501	96306	"
"	2836	4499	"	16 46	4 23	3148	2880	64	20	7	7	-1501	96306	"
"	2837 <sub>1</sub>	4501	"	17 06	4 43	4793	4386	52	16	7	8	0	97807	"

Table IV. Results along the Route 25. (0.01 mgal.).  
Route 25, B.M. 5800—Prefecture Boundary (No. 3078)—B.M. 5800.

Pref.	No.	B.M.	Date 1952	Time	$\Sigma\delta T$	SD	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	E.T.	$0.18 \times \Sigma\delta T$ Drift	$\Sigma\delta g$	$g$ 980.	Field Note No.
4	3068	5800	XI 25	<sup>h</sup> <sub>m</sub> 12 00	<sup>h</sup> <sub>m</sub> 0 00	4368	3997	59	18	7	0	0	14848	63
"	3069	5802	"	12 10	10	3357	3072	47	15	7	0	-928	13920	"
"	3070	5804	"	12 27	27	4260	3898	75	23	7	0	94	14754	"
"	3071	5809	"	13 28	1 28	2466	2256	57	18	8	0	-1742	13106	"
"	3072	5812	"	13 47	1 47	2617	2395	54	17	8	0	-1604	13244	"
"	3073	5814	"	14 00	2 00	2770	2535	63	19	8	0	-1462	13386	"
"	3074	6595	"	14 16	2 16	3147	2880	56	17	8	0	-1119	13729	"
"	3075	6592	"	14 31	2 31	3771	3450	54	17	6	0	-547	14301	"
"	3076	6590	"	14 42	2 42	4805	4397	41	13	6	0	396	15244	"
"	3077	6587	"	15 00	3 00	3568	3265	29	9	6	1	-741	14107	"
4.5	3078	P.B.*	"	15 17	3 17	3060	2800	66	20	6	1	-1195	13653	"
4	3079	6589	"	15 41	3 41	4886	4471	70	22	3	1	481	15329	"
"	3080	5806	"	16 46	4 46	2026	1854	45	14	1	1	-2142	12706	"
"	3081	5804	"	17 04	5 04	4250	3889	75	23	1	1	-98	14750	"
"	3082	"	XI 26	9 40	4336	3967	74	"	"	3	1	0	14848	"
"	3083 <sub>1</sub>	5800	"	10 11	5 35	4448	4070	59	18	3	1	0	14848	"

\* Prefecture Boundary.

Route 25<sub>2</sub> B.M.J. 9—B.M. 5800—B.M.J. 9.

Pref.	No.	B.M.	Date	Time	$\Sigma\delta T$	$SD$	$0.9150 \times SD$	$h$	$0.3086 \times h$	$E.T.$	$2.61 \times \Sigma\delta T$	$\Sigma\delta g$	$g$	Field Note No.
4	3062	J. 9	XI 25	<sup>h</sup> 10 36	<sup>m</sup> 0 00	2648	2423	73	23	- 7	0	0	18617	63
"	3063 <sup>1</sup>	5790	"	<sup>h</sup> 11 03	<sup>m</sup> 27	0726	0664	22	7	- 7	1	-1776	16841	"
"	3063 <sup>2</sup>	"	"	<sup>h</sup> 11 06	"	6555	5998	"	"	- 7	2	-1993	16624	"
"	3064	5792	"	<sup>h</sup> 11 15	<sup>m</sup> 36	6310	5774	49	15	- 7	2	-2158	16459	"
"	3065	5794	"	<sup>h</sup> 11 26	<sup>m</sup> 47	6130	5609	47	15	- 7	2	-2158	16459	"
"	3066	5796	"	<sup>h</sup> 11 38	<sup>m</sup> 59	4981	4558	47	15	- 7	3	-3210	15407	"
"	3067	5798	"	<sup>h</sup> 11 48	<sup>m</sup> 1 09	4826	4416	20	6	- 7	3	-3361	15256	"
"	3068	5800	"	<sup>h</sup> 12 00	<sup>m</sup> 1 21	4368	3997	59	18	- 7	4	-3769	14848	"
"	3083 <sup>2</sup>	"	XI 26	<sup>h</sup> 10 15	<sup>m</sup> 03	0364	0333	"	"	- 3	6	0	18617	"
"	3084	J. 9	"	<sup>h</sup> 11 12	<sup>m</sup> 2 18	4483	4102	74	23	- 6	6	0	18617	"

Route 25<sub>3</sub> B.M.J. 9—B.M. 5788—B.M.J. 9.

Pref.	No.	B.M.	Date	Time	$\Sigma\delta T$	$SD$	$0.9150 \times SD$	$h$	$0.3086 \times h$	$E.T.$	$8.14 \times \Sigma\delta T$	$\Sigma\delta g$	$g$	Field Note No.
4	2950 <sup>2</sup>	J. 9	XI 20	<sup>h</sup> 11 11	<sup>m</sup> 0 00	3437	3145	74	23	- 6	0	0	18617	61
"	2951	W.S.*	"	<sup>h</sup> 11 32	<sup>m</sup> 21	3406	3116	27	8	- 5	3	46	18571	"
"	2952	5786	"	<sup>h</sup> 14 50	<sup>m</sup> 3 39	2694	2465	74	23	- 7	30	- 711	17906	"
"	2953	5788	"	<sup>h</sup> 15 07	<sup>m</sup> 3 56	2069	1893	66	20	- 7	32	-1288	17329	"
"	2954	J. 9	"	<sup>h</sup> 15 27	<sup>m</sup> 4 16	3476	3181	73	23	- 7	35	0	18617	"

\* Weather Station, on the Block for the Pyrheliometer Observation.

Route 25<sub>t</sub> B.M.J. 9—(No. 3085)—B.M.J. 9.

Pref.	No.	B.M.	Date	Time	$\Sigma\delta T$	$SD$	$\frac{0.9150}{SD} \times h$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$4.18 \times \Sigma\delta T$ Drift	$\Sigma\delta g$	$g$ 980.	Field Note No.
4	3084	J. 9	XI 26	11 12	0 00	4483	4102	74	23	6	0	0	18617	63
"	3085	Akita Univ.**	"	12 22	1 10	5180	4740	27	8	8	5	616	19233	"
"	3086	"	"	12 27	1 15	5184	4743	27	8	8	5	619	19236	"
"	3087	Akita P.O.***	"	12 45	1 33	4835	4424	27	8	8	7	298	18915	"
"	3088.1	J. 9	"	16 36	5 27	4500	4118	76	23	1	23	0	18617	"

\* Akita University, Faculty of Mining.

\*\* Akita University, Entrance.

\*\*\* Akita Prefecture Office.

Route 25<sub>s</sub> B.M.J. 9—B.M. 5844—B.M.J. 9.

Pref.	No.	B.M.	Date	Time	$\Sigma\delta T$	$SD$	$\frac{0.9150}{SD} \times h$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$9.25 \times \Sigma\delta T$ Drift	$\Sigma\delta g$	$g$ 980.	Field Note No.
4	2994	J. 9	XI 22	16 32	0 00	4842	4430	72	22	6	0	0	18617	62
"	2995	5817	"	18 20	1 48	4000	3660	63	19	7	17	791	17826	"
"	2996	5819	"	18 36	2 04	4641	4247	65	20	7	19	205	18412	"
"	2997	5821	"	18 47	2 15	4822	4412	67	21	7	21	41	18576	"
"	2998	5823	"	18 59	2 27	5623	5145	61	19	7	23	688	19305	"
"	2999.1		"	19 36	3 04	7783	7121	—	—	7	29	2639	21256	"
"	2999.2		"	19 38	3 10	0095	0087	—	—	7	30	2787	21404	"
"	3000	5826	"	19 44	3 25	0234	0214	70	22	7	31	3620	22237	"
"	3001	5828	"	19 59	3 25	1146	1049	67	21	7	33	4528	23145	"
"	3002	5829	"	20 07	3 33	2146	1964	52	16	7	33	4528	23145	"
"	3003	5831	"	20 22	3 48	4316	3949	71	22	7	35	6517	25134	"
"	3004	5834	"	20 43	4 09	4190	3834	53	16	5	39	6394	25011	"
"	3005	5836	"	20 53	4 19	3645	3335	62	19	5	40	5897	24514	"
"	3006	5838	"	21 03	4 29	3417	3127	49	15	5	42	5683	24300	"
"	3007	5840	"	21 13	4 39	1951	1785	64	20	5	43	4345	22962	"

"	3008	5842	"	21 25	4 51	1248	1142	55	17	- 5	45	3697	22314	"
"	3009	5844	"	21 36	5 02	1400	1281	49	15	- 2	46	3836	22453	"
"	3060 <sub>2</sub>	"	XI 24	19 34	"	6772	6196	47	15	- 1	"	"	63	"
"	3061	J. 9	"	21 13	6 41	2589	2369	72	22	- 1	62	0	18617	"

Route 25<sub>0</sub> B.M. 6054—B.M. 6062—B.M. 6054.

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$	$0.3086 \times h$	$E.T.$	$5.00 \times \Sigma \delta T$	$\Sigma \delta g$	$g$	Field Note No.
4	3013	6054	XI 23	9 43 <sup>h.m</sup>	0 00	1924	1760	197	61	- 7	0	0	22880	62
"	3014	6056	"	10 04	21	2439	2232	62	19	- 7	2	428	23308	"
"	3015	6058	"	10 18	35	3713	3397	56	17	- 7	3	1590	24470	"
"	3016	6060	"	10 33	50	5364	4908	61	19	- 8	4	3101	25981	"
"	3017 <sub>1</sub>	6062	"	10 46	1 03	7203	6591	34	10	- 8	6	4773	27653	"
"	3022 <sub>2</sub>	"	"	13 07	"	7633	6984	29	9	- 7	"	"	"	"
"	3023	6054	"	13 40	1 36	2362	2161	195	60	- 6	8	0	22880	"

Route 25<sub>7</sub> B.M. 6062—B.M. 6069—B.M. 6062.

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$	$0.3086 \times h$	$E.T.$	$6.36 \times \Sigma \delta T$	$\Sigma \delta g$	$g$	Field Note No.
4	3017 <sub>2</sub>	6062	XI 23	10 50	0 00 <sup>h.m</sup>	1278	1169	34	10	- 8	0	0	27653	62
"	3018	6064	"	11 09	19	2718	2487	46	14	- 8	2	1320	28973	"
"	3019	6066	"	11 21	31	3407	3117	59	18	- 8	3	1953	29606	"
"	3020	6068	"	11 49	59	3420	3129	49	15	- 8	6	1959	29612	"
1	3021	6069	"	12 04	1 14	3972	3634	59	18	- 8	8	2465	30118	"
4	3022 <sub>1</sub>	6062	"	13 03	2 13	1293	1183	29	9	- 7	14	0	27653	"

Route 25s B.M. 6054—B.M. 5926—B.M. 5844—B.M. 6054.

Pref.	No.	B.M.	Date 1952	Time	$\Sigma\delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$3.51 \times \Sigma\delta T$ Drift	$\Sigma\delta g$	$g$ 980.	Field Note No.
4	3023	6054	XI 23	<sup>h</sup> 13 40	<sup>m</sup> 0 00	2362	2161	195	60	—	0	0	22880	62
"	3024	5846	"	14 48	1 08	2220	2031	67	21	—	4	172	22708	"
"	3025	5849	"	15 02	1 22	5589	5114	52	16	—	5	2905	25785	"
"	3026	5851	"	15 16	1 36	4446	4068	57	18	—	5	1860	24740	"
"	3027	5852	"	15 14	1 44	4435	4058	61	19	—	6	1851	24731	"
"	3028	5854	"	15 35	1 55	4453	4074	60	19	—	7	1867	24747	"
"	3029	5856	"	15 48	2 08	4770	4365	63	19	—	4	2158	25038	"
"	3030	5859	"	17 22	3 42	5210	4767	59	18	—	3	2554	25434	"
"	3031	5861	"	17 38	3 58	4793	4386	59	18	—	4	2171	25051	"
"	3032	5863	"	18 06	4 26	4657	4261	54	17	—	4	2044	24924	"
"	3033	5865	"	18 17	4 37	5544	5073	63	19	—	4	2857	25737	"
"	3034	5867	"	18 28	4 48	6384	5841	37	11	—	4	3616	26496	"
"	3035	5869	"	18 40	5 00	6324	5786	68	21	—	4	3570	26450	"
"	3036	5871	"	18 55	5 15	5006	4580	58	18	—	4	2360	25240	"
"	3037	J. 4	"	19 04	5 24	4709	4309	64	20	—	4	2091	24971	"
"	3038	5926	"	19 33	5 53	5555	5083	62	19	—	4	2862	25742	"
"	3058	"	XI 24	16 44	4 910	4910	4493	59	18	—	1	235	23115	63
"	3059	5847	"	18 22	7 31	2043	1869	66	20	—	1	26	23115	"
"	3060.1	5844	"	19 29	8 38	1328	1215	47	15	—	0	30	22453	"
"	3011	"	XI 23	9 00	1500	1500	1373	"	"	—	4	—	—	62
"	3012	J. 1	"	9 24	9 02	1500	1373	52	16	—	4	—	22452	"
"	3013	6054	"	9 43	9 21	1924	1760	197	61	—	7	0	22880	"



Route 25<sub>9</sub> B.M. 5926—B.M. 5933—B.M. 5926.

Pref.	No.	B.M.	Date 1952	Time	$\sum \delta T$	$SD$	$SD$	$0.9150$ $\times$ $SD$	$h$ (cm)	$0.3086$ $\times$ $h$	$E.T.$	$-1.67$ $\times$ $\sum \delta T$ Drift	$\sum \delta g$	$g$ 980.	Field Note No.
4	3039	5926	XI 24	<sup>h</sup> <sub>m</sub> 9 16	<sup>h</sup> <sub>m</sub> 0 00	5646	5166	5166	59	18	- 1	0	0	25742	62
"	3040	5928	"	9 26	10	5814	5320	5320	58	18	- 1	0	154	25896	"
"	3041	5930	"	9 37	21	5326	4873	4873	58	18	- 4	- 1	- 295	25447	"
"	3042	5932	"	9 50	34	4424	4048	4048	56	17	- 4	- 1	- 1121	24621	"
"	3043	5933	"	9 58	42	2912	2664	2664	57	18	- 4	- 1	- 2504	23238	"
"	3044	5926	"	10 27	1 11	5646	5166	5166	60	19	- 4	- 2	0	25742	"

Route 25<sub>10</sub> B.M. 5926—B.M. 5885—B.M. 5926.

Pref.	No.	B.M.	Date 1952	Time	$\sum \delta T$	$SD$	$SD$	$0.9150$ $\times$ $SD$	$h$ (cm)	$0.3086$ $\times$ $h$	$E.T.$	$7.69 \times$ $\sum \delta T$ Drift	$\sum \delta g$	$g$ 980.	Field Note No.
4	3044	5926	XI 24	<sup>h</sup> <sub>m</sub> 10 27	<sup>h</sup> <sub>m</sub> 0 00	5646	5166	5166	60	19	- 4	0	0	25742	62
"	3045	5873	"	10 54	27	4185	3829	3829	63	19	- 7	4	- 1344	24398	"
"	3046	5875	"	11 05	38	3830	3504	3504	60	19	- 7	5	- 1670	24072	"
"	3047	5877	"	11 15	48	3509	3211	3211	62	19	- 7	6	- 1964	23778	"
"	3048	5879	"	11 27	1 00	3731	3414	3414	39	12	- 7	8	- 1770	23972	"
"	3049	5881	"	11 40	1 13	3254	2977	2977	64	20	- 8	9	- 2201	23541	63
"	3050	5883	"	11 52	1 25	3587	3282	3282	57	18	- 8	11	- 1900	23842	"
"	3051	5885	"	12 03	1 36	1353	1238	1238	55	17	- 3	12	- 3946	21796	"
"	3057. <sup>2</sup>	"	"	15 46	0592	0542	0542	0542	54	17	- 8	0	0	25742	"
"	3058	5926	"	16 44	2 34	4910	4493	4493	59	18	- 1	20	0	25742	"

Route 25<sub>11</sub> B.M. 5885—B.M. 5894—B.M. 5885.

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$l$	$0.3086 \times l$	$E.T.$	$4.32 \times \Sigma \delta T$	$\Sigma \delta g$	$g$	Field Note No.
			1952	<sup>h</sup> <sup>m</sup>	<sup>h</sup> <sup>m</sup>	<sup>h</sup> <sup>m</sup>	<sup>h</sup> <sup>m</sup>	(cm)			Drift		980.	
4	3051-2	5885	XI 24	12 05	0 00	6100	5582	55	17	8	0	0	21796	63
"	3052	5887	"	12 17	12	5289	4839	70	22	8	1	-739	21057	"
"	3053	5889	"	12 32	27	3857	3529	51	16	8	2	-2056	19740	"
"	3054	5891	"	12 44	39	3785	3463	56	17	8	3	-2122	19674	"
"	3055	5893	"	13 00	55	2296	2101	66	20	8	4	-3482	18314	"
2	3056	5894	"	13 12	1 07	2247	2056	68	21	8	5	-3527	18269	"
4	3057-1	5885	"	15 44	3 39	6113	5593	54	17	3	16	0	21796	"

Route 25<sub>12</sub> B.M.J. 9—B.M. 5747—B.M. 5738—B.M.J. 9.

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$l$	$0.3086 \times l$	$E.T.$	$2.65 \times \Sigma \delta T$	$\Sigma \delta g$	$g$	Field Note No.
			1952	<sup>h</sup> <sup>m</sup>	<sup>h</sup> <sup>m</sup>	<sup>h</sup> <sup>m</sup>	<sup>h</sup> <sup>m</sup>	(cm)			Drift		980.	
4	2955	J. 9	XI 21	8 57	0 00	3681	3368	73	23	8	0	0	18617	61
"	2956	5783	"	9 12	15	3824	3499	52	16	8	1	123	18740	"
"	2957	5781	"	9 26	29	3574	3270	52	16	8	1	-106	18511	"
"	2958	5779	"	9 40	43	4451	4073	66	20	9	2	699	19316	"
"	2959	5777	"	9 55	58	3720	3404	50	15	9	3	24	18641	"
"	2960	5775	"	10 06	1 09	3139	2872	57	18	9	3	-505	18112	"
"	2961	5773	"	10 17	1 20	1620	1482	36	11	9	3	-1902	16715	"
"	2962	5770	"	10 36	1 39	3745	3427	74	23	8	5	54	18671	"
"	2963	5767	"	10 53	1 56	2820	2580	73	23	8	5	793	17824	"
"	2964	5765	"	11 07	2 10	3128	2862	62	19	8	6	-516	18101	"
"	2965	5763	"	11 17	2 20	3003	2748	53	16	8	6	633	17984	"
"	2966	5761	"	11 27	2 30	3235	2960	44	14	7	7	-423	18194	"
"	2967	5759	"	11 44	2 47	2970	2718	72	22	6	7	-656	17961	"
"	2968	5757	"	11 59	3 02	2401	2197	56	17	6	8	-1183	17434	"
"	2969	5755	"	12 10	3 13	1877	1717	66	20	6	8	-1660	16957	"

"	2970.1	5752	"	12 24	3 27	0864	0791	64	20	- 6	9	- 2587	16030	"
"	2970.2	"	"	12 27	"	7410	6780	"	"	- 6	"	"	"	"
"	2971	5749	"	12 39	3 39	6951	6360	49	15	- 4	10	- 3011	15606	"
"	2972	5747	"	13 44	4 44	7229	6615	71	22	- 4	12	- 2751	15866	"
"	2978	"	"	15 56	"	7241	6626	72	22	- 6	"	"	"	"
"	2979	5746	"	16 07	4 55	6546	5990	35	11	- 6	13	- 3399	15218	"
"	2980	5744	"	16 17	5 05	5446	4983	58	18	- 6	14	- 4400	14217	"
"	2981	5742	"	16 28	5 16	4910	4493	44	14	- 6	14	- 4894	13723	"
"	2982	5740	"	16 39	5 27	5623	5145	71	22	- 8	15	- 4237	14380	"
"	2983	5738	"	16 53	5 41	5522	5053	45	14	- 8	15	- 4337	14280	"
"	2993.2	"	XI 22	12 27	"	0101	0092	43	13	- 7	26	0	18617	62
"	2994	J. 9	"	16 32	9 46	4842	4430	72	22	- 6	"	"	"	"

Route 2513 B.M. 5738—Okachi Pass (No. 2991)—B.M. 5738.

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$	$0.3086 \times h$	$E.T.$	$7.95 \times \Sigma \delta T$	Drift	Adjustment	$\Sigma \delta g$	$g$	Field Note No.
4	2984	5738	XI 22	<sup>h</sup> 8 26	0 00	5639	5160	43	13	- 4	0	0	0	0	14280	61
"	2985	5736	"	8 43	17	4779	4373	45	14	- 6	2	2	2	- 792	13488	"
"	2986	5734	"	8 55	29	4404	4030	35	11	- 6	4	4	3	- 1141	13139	"
"	2987	5732	"	9 06	40	2515	2301	70	22	- 6	6	6	9	- 2867	11413	"
"	2988	5730	"	9 18	52	1391	1273	66	20	- 6	7	7	12	- 3901	10379	"
"	2989.1	5728	"	9 36	1 10	0694	0635	64	20	- 8	10	10	14	- 4546	09734	"
"	2989.2	"	"	9 40	"	7545	6904	"	"	- 8	"	"	"	"	"	"
"	2990	5726	"	10 17	1 47	5396	4937	65	20	- 8	14	14	20	- 6523	07757	"
4.5	2991	Okachi Pass P.B.	"	10 45	2 15	3474	3179	69	21	- 8	18	18	25	- 8289	05991	62
4	2992.1	5728	"	11 33	3 03	7570	6927	63	19	- 7	25	25	14	- 4538	09742	"
"	2992.2	"	"	11 35	"	0177	0162	"	"	- 7	"	"	0	0	14280	"
"	2993.1	5738	"	12 24	3 52	5134	4698	43	13	- 7	31	31	0	0	"	"

Route 25<sub>11</sub> B.M. 5747—B.M. 5550—B.M. 5747.

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$4.09 \times \Sigma \delta T$	$\Sigma \delta g$	$g$ 980.	Field Note No.
4	2972	5747	1952	13 44	0 00	7229	6615	71	22	- 4	0		15866	61
"	2973	5558	"	13 59	15	6894	6308	38	12	- 4	1	- 318	15548	"
"	2974	5556	"	14 13	29	5934	5430	66	20	- 4	2	- 1189	14677	"
"	2975	5554	"	14 26	42	5643	5163	58	18	- 4	3	- 1459	14407	"
"	2976	5552	"	14 41	57	3840	3514	61	19	- 5	4	- 3109	12757	"
2	2977	5550	"	15 02	1 18	0526	0481	63	19	- 5	5	- 6143	09723	"
4	2978	5747	"	15 56	2 12	7241	6626	72	22	- 6	9	0	15866	"

Table V. Results along the Route 26. (0.01 mgal.)  
Route 26<sub>1</sub> B.M. 6101—B.M. 6069—B.M. 6101.

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$6.12 \times \Sigma \delta T$	$\Sigma \delta g$	$g$ 980.	Field Note No.
1	2418	6101	1952	8 49	0 00	3660	3349	44	14	- 1	0	0	31161	53
"	2419	6100	"	9 04	15	4136	3784	56	17	- 1	2	436	31597	"
"	2420	6098	"	9 18	29	3383	3095	59	18	- 1	3	- 253	30908	"
"	2421	6095	"	9 37	48	2006	1835	58	18	3	5	- 1511	29650	"
"	2422	6093	"	9 55	1 06	4387	4014	53	16	3	7	664	31825	"
"	2423	6091	"	10 11	1 22	4630	4236	58	18	3	9	886	32047	"
"	2424	6089	"	10 25	1 36	5029	4602	53	16	3	10	1249	32410	"
"	2425	6087	"	10 48	1 59	4030	3687	58	18	5	12	336	31497	"
"	2426	6085	"	11 08	2 19	4247	3886	53	16	5	14	531	31692	"
"	2427	6083	"	11 27	2 38	4361	3990	58	18	5	16	635	31796	54
"	2428	6081	"	11 48	2 59	2687	2459	63	19	5	18	- 897	30264	"
"	2429	6079	"	12 11	3 22	2500	2288	67	21	5	21	- 1069	30092	"
"	2430	6077	"	14 00	5 11	2490	2278	64	20	0	32	- 1096	30065	"
"	2431	6075	"	14 12	5 23	1867	1708	53	16	0	33	- 1671	29490	"
"	2432-1	6073	"	14 28	5 39	0982	0899	55	17	0	35	- 2481	28680	"

"	2432.2	"	"	"	14 32	2100	1922	"	"	4	36	-1094	30067	"
"	2433	6071	"	"	14 48	5 55	3618	55	17	- 4	38	-1043	30118	"
"	2434.1	6069	"	"	15 06	6 13	3673	3310	19	- 4	38	-1043	30118	"
"	2434.2	"	"	"	15 12	0305	0279	"	"	- 4	60	0	31161	"
"	2435	6101	"	"	18 48	9 49	1479	1353	14	- 8	60	0	31161	"

Route 26<sub>2</sub> B.M.J. 6112—B.M. 6101—B.M.J. 6112.

Pref.	No.	B.M.	Date	Time	$\Sigma\delta T$	$SD$	$0.9150 \times SD$	$h$	$0.3086 \times h$	E.T.	$6.86 \times \Sigma\delta T$	$\Sigma\delta\theta$	$g$	Field Note No.
1	2411	J. 6112	IX 19	<sup>h</sup> 16 39	<sup>m</sup> 0 00	3099	2836	52	16	- 8	0	0	32346	53
"	2412	6110	"	17 26	47	2113	1933	50	15	- 8	5	- 909	31437	"
"	2413	6108	"	17 41	1 02	1382	1265	42	13	- 9	7	-1582	30764	"
"	2414.1	6106	"	17 56	1 17	1002	0917	52	16	- 9	9	-1929	30417	"
"	2414.2	"	"	18 01		6853	6270	"	"	- 9				"
"	2415	6104	"	18 15	1 31	6259	5727	58	18	- 9	10	-2471	29875	"
"	2416	6102	"	18 29	1 45	6896	6310	54	17	- 7	12	-1891	30455	"
"	2417.1	6101	"	19 02	2 18	7673	7021	44	14	- 7	16	-1185	31161	"
"	2435	"	IX 20	18 48		1479	1353	"	"	- 8				54
"	2436	J. 6112	"	20 01	3 31	2777	2541	53	16	- 5	24	0	32346	"

Route 26<sub>3</sub> B.M.J. 6112—B.M. 6166—B.M.J. 6112.

Pref.	No.	B.M.	Date	Time	$\Sigma\delta T$	$SD$	$0.9150 \times SD$	$h$	$0.3086 \times h$	E.T.	$7.32 \times \Sigma\delta T$	$\Sigma\delta\theta$	$g$	Field Note No.
1	2403	J. 6112	IX 19	<sup>h</sup> 12 36	<sup>m</sup> 0 00	3053	2793	53	16	5	0	0	32346	53
"	2404	6178	"	12 58	22	2874	2630	69	21	5	3	161	32185	"
"	2405	6176	"	13 11	35	3252	2976	66	20	5	4	183	32529	"
"	2406	6174	"	14 05	1 29	3850	3523	65	20	2	11	720	33066	"
"	2407	6172	"	14 21	1 45	4293	3928	46	14	2	13	1117	33463	"

Table V. (Continued)

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$7.32 \times \Sigma \delta T$ Drift	$\Sigma \delta g$	$g$ 980.	Field Note No.
1	2408	6170	1952 IX 19	<sup>h</sup> 14 38	<sup>m</sup> 2 02	4217	3859	34	10	- 2	15	1038	33384	53
"	2409	6168	" "	<sup>h</sup> 14 56	<sup>m</sup> 2 20	4495	4114	68	21	- 2	17	1302	33648	"
"	2410	6166	" "	<sup>h</sup> 15 12	<sup>m</sup> 2 36	5549	5169	36	11	- 2	19	2345	34691	"
"	2411	J. 6112	" "	<sup>h</sup> 16 39	<sup>m</sup> 4 03	3099	2836	52	16	- 8	30	0	32346	"

Route 26<sub>1</sub> B.M.J. 5-B.M.J. 6112-B.M.J. 5.

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$8.97 \times \Sigma \delta T$ Drift	$\Sigma \delta g$	$g$ 980.	Field Note No.
1	2400.2	J. 5	1952 IX 19	<sup>h</sup> 11 16	<sup>m</sup> 0 00	3000	2745	49	15	7	0	0	27003	53
"	2401	6117	" "	<sup>h</sup> 11 56	<sup>m</sup> 40	5397	4938	44	14	7	6	2186	29189	"
"	2402.1	6115	" "	<sup>h</sup> 12 11	<sup>m</sup> 55	7557	6915	56	17	7	8	4164	31167	"
"	2402.2	"	" "	<sup>h</sup> 12 14	<sup>m</sup> 1756	1607	1607	"	"	7	5	5343	32346	"
"	2403	J. 6112	" "	<sup>h</sup> 12 36	<sup>m</sup> 1 17	3053	2793	53	16	5	12	0	27003	"
"	2437	"	1952 IX 21	<sup>h</sup> 8 21	<sup>m</sup> 2878	2633	2633	54	17	- 7	22	2711	29714	54
"	2438.1	"	" "	<sup>h</sup> 9 35	<sup>m</sup> 0024	0022	0022	-	-	- 1	1	0	27003	"
"	2438.2	"	" "	<sup>h</sup> 9 39	<sup>m</sup> 7695	7041	7041	-	-	- 1	26	0	27003	"
"	2439	J. 5	" "	<sup>h</sup> 10 02	<sup>m</sup> 2 54	4721	4320	44	14	- 1	0	0	27003	"

Route 265 B.M.J. 5—B.M. 5933—B.M.J. 5.

Pref.	No.	B.M.	Date 1952	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$13.14 \times \Sigma \delta T$ Drift	Adjust- ment	$\Sigma \delta g$	$g$ 980.	Field Note No.
1	2439	J. 5	IX 21	10 02	0 00	4721	4320	44	14	—	0	0	0	27003	54
"	2440	5957	"	10 14	12	4508	4125	34	10	—	3	- 2	- 200	26803	"
"	2441	5955	"	10 26	24	4380	4008	63	19	—	5	- 3	- 309	26694	"
"	2442	5953	"	10 36	34	4517	4133	49	15	—	8	- 2	- 189	26814	"
"	2443	5951	"	10 46	44	5377	4920	50	15	—	9	5	590	27593	"
"	2444	5949	"	10 57	55	5054	4624	51	16	—	12	3	294	27297	"
"	2445	5947	"	11 08	1 06	5177	4737	50	15	—	14	4	403	27406	"
"	2446	5945	"	11 21	1 19	3897	3566	63	19	—	17	7	756	26247	"
"	2447	5943	"	11 33	1 31	4141	3789	61	19	—	20	5	535	26467	"
"	2448	5941	"	11 43	1 41	5176	4736	51	16	—	22	4	397	27400	"
"	2449	5939	"	11 56	1 54	2442	2234	55	17	—	25	- 19	- 2084	24919	"
"	2450. <sup>1</sup>	5937	"	12 10	2 08	1318	1206	53	16	—	28	- 28	- 3107	23896	"
"	2450. <sup>2</sup>	"	"	12 12	"	3688	3375	"	"	—	4	4	—	"	"
"	2451	5935	"	12 24	2 20	3189	2918	67	21	—	4	- 32	- 3557	23446	"
4	2452	5933	"	12 37	2 33	2978	2725	28	9	—	34	- 34	- 3765	23238	"
1	2453. <sup>1</sup>	*	"	13 16	3 12	7649	6999	—	—	—	42	4	454	27457	"
"	2453. <sup>2</sup>	"	"	13 20	"	0994	0910	—	—	—	3	0	0	27003	"
"	2454	J. 5	"	13 35	3 27	0484	0443	47	15	—	46	0	0	27003	"

\* Front of the Ôwani Village Office.

Route 26<sub>6</sub> B.M. 5966—B.M.J. 5—B.M. 5966.

Pref.	No.	B.M.	Date 1952	Time	$\Sigma\delta T$	$SD$	$\frac{0.9150}{SD}$	$h$ (cm)	$\frac{0.3086}{h}$	$E.T.$	$\frac{-2.78}{\Sigma\delta T}$ Drift	$\Sigma\delta g$	$g$ 980.	Field Note No.
1	2396	5966	IX 19	<sup>h</sup> <sub>10 15</sub>	0 00	4668	4271	58	18	4	0	0	30782	53
"	2397	5964	"	<sup>h</sup> <sub>10 26</sub>	11 35	3548	3246	44	14	4	1	-1028	29754	"
"	2398	5962	"	<sup>h</sup> <sub>10 43</sub>	28 41	3427	3136	65	20	7	1	-1129	29653	"
"	2399	5960	"	<sup>h</sup> <sub>10 56</sub>	41 59	1734	1587	47	15	7	2	-2682	28100	"
"	2400. <sub>1</sub>	J. 5	"	<sup>h</sup> <sub>11 14</sub>	59 05	0531	0489	49	15	7	3	-3779	27003	"
"	2454	"	IX 21	<sup>h</sup> <sub>13 35</sub>	3 37	0484	0443	47	15	1	-10	0	30782	54
"	2455	5966	"	<sup>h</sup> <sub>16 13</sub>	3 37	4612	4220	56	17	6	-10	0	30782	"

Route 26<sub>7</sub> B.M. 5966—B.M. 6137—B.M. 5966.

Pref.	No.	B.M.	Date 1952	Time	$\Sigma\delta T$	$SD$	$\frac{0.9150}{SD}$	$h$ (cm)	$\frac{0.3086}{h}$	$E.T.$	$\frac{5.44}{\Sigma\delta T}$ Drift	$\Sigma\delta g$	$g$ 980.	Field Note No.
1	2377	5966	IX 18	<sup>h</sup> <sub>9 00</sub>	0 00	3457	3163	57	18	5	0	0	30782	53
"	2378	6121	"	<sup>h</sup> <sub>9 14</sub>	14 14	2616	2394	47	15	5	1	-773	30009	"
"	2379	6123	"	<sup>h</sup> <sub>9 30</sub>	30 50	2092	1914	58	18	7	3	-1250	29532	"
"	2380	6125	"	<sup>h</sup> <sub>9 50</sub>	50 29	2291	2096	59	18	7	4	-1069	29713	"
"	2381	6127	"	<sup>h</sup> <sub>10 09</sub>	1 09	2364	2621	34	10	7	7	-555	30227	"
"	2382	6129	"	<sup>h</sup> <sub>10 27</sub>	1 27	3580	3276	30	9	7	8	98	30880	"
"	2383	6131	"	<sup>h</sup> <sub>10 44</sub>	1 44	4037	3694	82	25	8	9	532	31314	"
"	2384	6133	"	<sup>h</sup> <sub>11 00</sub>	2 00	4728	4326	36	11	8	11	1148	31930	"
"	2385	6135	"	<sup>h</sup> <sub>11 28</sub>	2 28	6240	5710	109	34	8	14	2552	33334	"
"	2386	6137	"	<sup>h</sup> <sub>11 51</sub>	2 51	6515	5961	-5	-2	7	16	2764	33546	"
"	2394. <sub>2</sub>	"	"	<sup>h</sup> <sub>18 23</sub>	4 36	7569	6926	-7	-2	8	25	0	30782	"
"	2395	5966	"	<sup>h</sup> <sub>20 08</sub>	4 36	4530	4145	58	18	2	25	0	30782	"



Route 26<sub>8</sub> B.M. 6137—B.M. 6151—B.M. 6137.

Pref.	No.	B.M.	Date 1952	Time	$\Sigma\delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$8.41 \times \Sigma\delta T$ Drift	$\Sigma\delta g$	$g$ 980.	Field Note No.
1	2386	6137	IX 18	11 51 <sup>m</sup>	0 00 <sup>m</sup>	6515	5961	- 5	- 2	7	0	0	33546	53
"	2387	6139	"	12 12	21	7160	6551	75	23	7	3	612	34158	"
"	2388 <sub>1</sub>	"	"	12 49	58	7801	7138	-	-	4	8	1168	34714	"
"	2388 <sub>2</sub>	"	"	12 54		5411	4951	-	-	4				"
"	2389	6141	"	13 03	1 07	5844	5347	54	17	4	9	1580	35126	"
"	2390 <sub>1</sub>	6151	"	16 12	4 16	5048	4619	6	2	- 7	36	799	34345	"
"	2390 <sub>2</sub>	"	"	16 16		2228	2039	"	"	- 7				"
"	2391	6148	"	16 51	4 51	2514	2300	65	20	- 9	41	1071	34617	"
"	2392	6146	"	17 13	5 13	4437	4060	74	23	- 9	44	2831	36377	"
"	2393	6144	"	17 33	5 33	5477	5011	48	15	- 8	47	3772	37318	"
"	2394 <sub>1</sub>	6137	"	18 19	6 19	1379	1262	- 7	- 2	- 8	53	0	33546	"

\* Hill in the Ishizaki Wireless Station.

Route 26<sub>9</sub> B.M. 5966—B.M. 6046—B.M. 6120—B.M. 5966.

Pref.	No.	B.M.	Date 1952	Time	$\Sigma\delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$12.33 \times \Sigma\delta T$ Drift	$\Sigma\delta g$	$g$ 980.	Field Note No.
1	2455	5966	IX 21	16 13 <sup>m</sup>	0 00 <sup>m</sup>	4612	4220	56	17	- 6	0	0	30782	54
"	2456 <sub>1</sub>	6050	"	16 53	40	7088	6486	61	19	- 8	9	2257	33039	"
"	2456 <sub>2</sub>	"	"	16 58		2932	2683	"	"	- 8				"
"	2457	6047	"	17 29	1 11	3814	3490	49	15	- 8	15	3054	33836	"
"	2458	6046	"	17 42	1 24	4885	4470	37	11	- 9	17	4027	34809	"
"	2525	"	IX 26	9 02		5252	4806	56	17	0				55
"	2526 <sub>1</sub>	6120	"	10 05	2 27	0705	0645	71	22	- 2	31	- 145	30637	"
"	2526 <sub>2</sub>	"	"	10 08		4212	3854	"	"	- 2				"
"	2527	Aomori W.S.*	"	10 19	2 38	3279	3000	27	8	- 2	32	-1014	29768	"
"	2528 <sub>1</sub>	5966	"	10 39	2 58	4384	4011	58	18	- 4	37	0	30782	"

\* Weather Station Seismometer Room, on the Surface of the Concrete Block for Seismometer Installation.

Route 26<sub>10</sub> B.M. 6046—B.M.J. 6031—B.M. 6046.

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$6.67 \times \Sigma \delta T$ Drift	$\Sigma \delta g$	$g$ 980.	Field Note No.
1	2459	6046	IX 22	16 07 <sup>h m</sup>	0 00 <sup>h m</sup>	5043	4614	37	11	— 5	0	0	34809	54
"	2460	6043	"	16 23	16	5688	5205	56	17	— 5	2	595	35404	"
"	2461	6041	"	16 36	29	6626	6063	63	19	— 7	3	1452	36261	"
"	2462	6039	"	16 49	42	5793	5301	68	21	— 7	5	690	35499	"
"	2463	6037	"	17 00	53	4221	3862	61	19	— 7	6	— 752	34057	"
"	2464	6035	"	17 12	1 05	3726	3409	53	16	— 7	7	— 1209	33600	"
"	2465	6033	"	17 25	1 18	3970	3633	62	19	— 7	9	— 984	33825	"
"	2466	J. 6031	"	17 47	1 40	2710	2480	64	20	— 9	11	— 2140	32669	"
"	2523	"	IX 25	20 27	2829	2589	52	16	— 7	— 7	—	—	—	55
"	2524	6046	"	23 17	4 30	5183	4742	56	17	— 2	30	0	34809	"

Route 26<sub>11</sub> B.M.J. 6031—B.M.J. 6236—B.M.J. 6031.

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$7.09 \times \Sigma \delta T$ Drift	$\Sigma \delta g$	$g$ 980.	Field Note No.
1	2497	J. 6031	IX 24	8 52 <sup>h m</sup>	0 00 <sup>h m</sup>	1506	1378	61	19	— 6	0	0	32669	55
"	2498-1	6261	"	9 21	29	1091	9998	54	17	— 6	4	— 386	32283	"
"	2498-2	"	"	9 24	3578	3274	26	8	"	— 6	6	606	33275	"
"	2499	6259	"	9 45	50	4673	4276	26	8	— 5	6	3046	35715	"
"	2500-1	6255	"	10 45	1 50	7333	6710	66	20	— 4	13	—	—	"
"	2500-2	"	"	10 48	1576	1442	"	"	"	— 4	—	—	—	"
"	2501	6253	"	11 10	2 12	2477	2266	34	10	— 4	16	3857	36526	"
"	2502	6251	"	11 26	2 28	2183	1997	47	15	— 4	18	3591	36260	"
"	2503	6246	"	12 34	3 36	2787	2550	42	13	— 2	26	4136	36805	"
"	2504	6243	"	13 01	4 03	3016	2760	56	17	— 2	29	4347	37016	"



Route 2613 B.M.J. 6031—Prefecture Boundary (No. 2482)—B.M.J. 5496—Morioka (No. 3176)—B.M. 5492—B.M.J. 5496—B.M. 5894.

Pref.	No.	B.M.	Date 1952	Time <sup>h</sup> <sub>m</sub>	$\Sigma \delta T$	SD	$0.9150 \times SD$	h (cm)	$0.3086 \times h$	E.T.	$10.15 \times \Sigma \delta T$ Drift	$\Sigma \delta g$	g 980.	Field Note No.
1	2466	J. 6031	IX 22	17 47	0 00	2710	2480	64	20	— 9	0	0	32669	54
"	2467	6029	"	18 15	0 28	1702	1557	56	17	— 9	5	931	31738	"
"	2468 <sup>1</sup>	6026	"	18 55	1 08	0268	0245	56	17	— 8	11	2248	30421	"
"	2468 <sup>2</sup>	"	"	19 00	"	5743	5255	"	"	— 8	"	"	"	"
"	2469	6023	"	19 23	1 31	5805	5312	50	15	— 8	15	2197	30472	"
"	2470	6020	"	20 14	2 22	4556	4169	77	24	— 6	24	3338	29331	"
"	2471 <sup>1</sup>	6016	"	20 53	3 01	3682	3369	41	13	— 2	30	4151	28518	"
"	2472 <sup>2</sup>	"	IX 23	8 55	"	3770	3450	40	12	— 6	"	"	"	"
"	2473	6017	"	9 48	3 54	4065	3719	46	14	— 4	40	3888	28781	"
"	2474	6013	"	10 17	4 23	4105	3756	60	19	— 4	45	3851	28818	"
"	2475	6011	"	10 28	4 34	2994	2740	46	14	— 4	47	4874	27795	"
"	2476	6008	"	10 58	5 04	2655	2429	66	20	— 2	52	5182	27487	"
"	2477	6005	"	11 12	5 18	3846	3519	45	14	— 2	54	4100	28569	"
"	2478	6003	"	11 22	5 28	3565	3262	32	10	— 2	56	4363	28306	"
"	2479	6001	"	11 35	5 41	2412	2207	55	17	— 2	58	5413	27256	"
"	2480	5999	"	11 47	5 53	5690	5206	64	20	— 2	60	2413	30256	"
"	2481	5997	"	12 02	6 08	3301	3020	60	19	— 2	62	4602	28067	"
1-2	2482	P.B.*	"	12 54	7 00	3603	3297	27	8	— 1	71	4344	28325	"
"	3158	"	XII 10	14 47	"	4004	3664	"	"	— 2	"	"	"	64
2	3159	5527 <sup>2</sup>	"	15 12	7 25	3220	2946	61	19	— 2	75	5055	27614	"
"	3160	5527 <sup>1</sup>	"	15 28	7 41	3398	3109	44	14	— 2	78	4900	27769	"
"	3161	5525	"	15 45	7 58	4030	3687	62	19	0	81	4318	28351	"
"	3162	5523	"	15 56	8 09	3275	2997	65	20	0	83	5009	27360	"
"	3163 <sup>1</sup>	5521	"	16 10	8 23	1413	1293	40	12	0	85	6723	25946	"
"	3163 <sup>2</sup>	"	"	16 13	"	7509	6871	"	"	0	"	"	"	"

\* Prefecture Boundary.

"	3164	5519	"	16 26	8 36	5710	5225	38	12	0	87	8371	24298	"
"	3165	5517	"	16 41	8 51	3073	2812	0	0	2	90	-10797	21872	"
"	3166	5515	"	16 59	9 09	0820	0750	59	18	2	93	-12844	19825	"
"	3167	5512	"	17 29	9 39	0724	0662	42	13	2	98	-12942	19727	"
"	3168	5510	"	17 43	9 53	1867	1708	74	23	3	101	-11888	20781	"
"	3169	5508	"	17 57	10 07	1890	1729	37	11	3	103	-11881	20788	"
"	3170	5505	"	18 18	10 28	2075	1899	48	15	3	107	-11711	20958	"
"	3171	5503	"	18 32	10 42	1840	1684	23	7	3	109	-11936	20733	"
"	3172	5501	"	18 44	10 54	1380	1263	73	23	3	111	-12343	20326	"
"	3173.1	5500	"	18 53	11 03	0905	0828	48	15	3	113	-12788	19881	"
"	3173.2	"	"	18 56	"	2649	2424	"	"	3	115	-13597	19072	"
"	3174	5498	"	19 10	11 17	1766	1616	52	16	3	118	-14545	18124	"
"	3175	J. 5496	"	19 28	11 35	0735	0673	45	14	3	123	-11960	20709	"
"	3176	"	"	19 57	12 04	3572	3268	27	8	4	123	-11960	20709	"
"	3134.2	"	XII 9	10 41	"	4148	3795	"	"	-	6	"	"	"
"	3135	5492	"	11 01	12 24	3459	3165	44	14	-	6	-12587	20082	"
"	3136	5494	"	11 16	12 39	2803	2565	44	14	-	6	-13190	19479	"
"	3137.1	J. 5496	"	11 32	12 55	1365	1249	41	13	-	7	-14510	18159	"
"	3137.2	"	"	11 38	"	7051	6452	"	"	-	7	"	"	"
"	3138	5923	"	12 00	13 17	5916	5413	45	14	-	7	-15552	17117	"
"	3139	5920	"	12 21	13 38	6585	6025	57	18	-	7	-14939	17730	"
"	3140	5918	"	12 41	13 58	6407	5862	54	17	-	6	-15106	17563	"
"	3141	5916	"	13 01	14 18	6566	6008	46	14	-	6	-14966	17703	"
"	3142	5914	"	14 42	15 59	6143	5621	60	19	-	3	-15362	17307	"
"	3143	5912	"	14 59	16 16	4648	4253	58	18	-	3	-16735	15934	"
"	3144	5910	"	15 25	16 42	2241	2051	65	20	-	3	-18939	13730	"
"	3145	5908	"	15 42	16 59	5003	4578	45	14	-	1	-16419	16250	"
"	3146	5906	"	16 00	17 17	6372	5830	55	17	-	1	-15167	17502	"
"	3147	5904	"	16 17	17 34	7303	6682	47	15	-	1	-14320	18349	"
"	3148	5902	"	17 00	18 17	6409	5864	64	20	-	0	-15139	17530	"
"	3149	5900	"	17 18	18 35	4188	3832	52	16	0	189	-17178	15491	"
"	3150.1	5898	"	17 38	18 55	7246	6630	52	16	2	192	-14381	18288	"
"	3150.2	"	"	17 42	"	1445	1322	"	"	2	194	-14334	18335	"
"	3151	5896	"	18 00	19 13	1501	1373	50	15	2	194	-14334	18335	"
"	3152	5894	"	18 18	19 31	1425	1304	69	21	2	198	-14400	18269	"

\* Morioka Ken Gikai, Entrance.

Route 26<sub>14</sub> Prefecture Boundary (No. 2482)—B.M. 6958—B.M.J. 6031.

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$	$0.3086 \times h$	$E.T.$	$2.83 \times \Sigma \delta T$ Drift	$\Sigma \delta g$	$g$	Field Note No.
1	2482	P.B.	1952	12 54 <sup>h</sup> 0 00 <sup>m</sup>	0 00 <sup>h</sup> 0 00 <sup>m</sup>	3603	3297	27	8	— 1	0	0	28325	54
"	2483	6966	"	13 42	48	5282	4833	38	12	— 1	2	1538	29863	"
"	2484-1	6964	"	13 55	1 01	6152	5629	61	19	— 1	3	2340	30665	"
"	2484-2	"	"	14 01	3711	3711	3396	"	"	— 1	3	4341	32666	"
"	2485	6962	"	14 12	1 12	5893	5392	77	24	— 1	3	4341	32666	"
"	2486-1		"	14 58	1 58	7863	7195	—	—	— 2	6	6116	34441	"
"	2486-2		"	15 02	1776	1776	1625	—	—	— 2	6	7012	35337	"
"	2487	6181	"	15 18	2 14	2737	2504	54	17	— 2	6	7012	35337	"
"	2488-1	6185	"	15 38	2 34	1295	1185	47	15	— 5	7	5687	34012	55
"	2488-2	"	"	15 45	2856	2856	2613	"	"	— 5	7	5687	34012	"
"	2489	6958	"	16 58	3 47	5742	5254	52	16	— 7	11	8323	36648	"
"	2494	"	"	19 09	4 06	5768	5278	"	"	— 9	12	8075	36400	"
"	Hachinoe 2495		"	19 28	5507	5507	5039	27	8	— 9	12	8075	36400	"
"	" 2496		IX 24	6 58	5587	5587	5112	"	"	— 3	17	4344	32669	"
"	" 2497	J. 6031	"	8 52	6 00	1506	1378	61	19	— 6	17	4344	32669	"

Route 26<sub>15</sub> B.M. 6958—B.M. 6950—B.M. 6958.

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$	$0.3086 \times h$	$E.T.$	$10.00 \times \Sigma \delta T$ Drift	$\Sigma \delta g$	$g$	Field Note No.
1	2489	6958	1952	16 58 <sup>h</sup> 0 00 <sup>m</sup>	0 00 <sup>h</sup> 0 00 <sup>m</sup>	5742	5254	52	16	— 7	0	0	36648	55
"	2490	6956	"	17 17	19	4956	4535	83	26	— 7	3	— 712	35936	"
"	2491	6954	"	17 38	40	4310	3944	48	15	— 9	7	— 1320	35328	"
"	2492	6951	"	18 05	1 07	3958	3622	33	10	— 9	11	— 1651	34997	"
"	2493	6950	"	18 18	1 20	5137	4700	44	14	— 9	13	— 571	36077	"
"	2494	6958	"	19 09	2 11	5768	5278	52	16	— 9	22	0	36648	"

Route 271 Morioka (No. 3177)—B.M. 5490—B.M. 5470—B.M. 6827—B.M.J. 3—B.M. 6900—B.M. 6932—B.M. 6950.  
 Table VI. Results along the Route 27. (0.01 mgal.).

Pref.	No.	B.M.	Date 1952	Time h <sup>m</sup>	$\Sigma\delta T$ h <sup>m</sup>	SD	$0.9150 \times$ SD	h (cm)	$0.3086 \times$ h	E.T. Drift	$0.87 \times$ $\Sigma\delta T$	$\Sigma\delta g$	g 980.	Field Note No.
2	3177	*	XII 11	9 53	0 00	3670	3358	27	8	4	0	0	20709	64
"	3178	5490	"	10 01	8	3690	3376	121	37	4	0	47	20756	"
"	3179	W.S.**	"	10 32	39	3143	2876	27	8	6	1	-485	20224	"
"	3180	5488	"	11 04	1 11	3936	3601	44	14	6	1	246	20955	"
"	3181	5485	"	11 22	1 29	5516	5047	60	19	6	1	1697	22406	"
"	3182	5483	"	11 33	1 40	4047	3703	60	19	7	1	352	21061	"
"	3183	5481	"	11 48	1 55	4437	4060	91	28	7	2	717	21426	"
"	3184	5480	"	11 57	2 04	4349	3979	47	15	7	2	623	21332	"
"	3185	5478	"	12 06	2 13	3389	3101	60	19	7	2	-251	20458	"
"	3186	5476	"	12 18	2 25	2343	2144	67	21	7	2	-1206	19503	"
"	3187. <sup>1</sup>	5474	"	12 29	2 36	1560	1427	21	6	7	2	-1938	18771	"
"	3187. <sup>2</sup>	"	"	12 32	7065	6464	"	"	"	7	"	"	"	"
"	3188	5472	"	12 45	2 49	6435	5888	74	23	7	2	-2497	18212	"
"	3189	5470	"	13 59	4 03	5952	5446	66	20	6	4	-2943	17766	"
"	3213. <sup>2</sup>	"	XII 12	14 00	2880	2635	64	20	7	7	"	"	65	"
"	3214	6847	"	14 44	4 47	4917	4499	54	17	6	4	-1081	19628	"
"	3215	6845	"	14 55	4 58	5022	4595	64	20	6	4	-982	19727	"
"	3216	6843	"	15 11	5 14	5174	4734	71	22	6	5	-842	19867	"
"	3217	6840	"	15 50	5 53	3748	3429	81	25	3	5	-2141	18568	"
"	3218	6838	"	16 04	6 07	2095	1917	69	21	3	5	-3657	17052	"
"	3219	6836	"	16 17	6 20	3040	2782	47	15	3	5	-2798	17911	"
"	3220	6834	"	16 29	6 32	3091	2828	70	22	3	6	-2746	17963	"
"	3221	6832	"	16 41	6 44	2886	2641	44	14	1	6	-2937	17772	"
"	3222	6830	"	16 57	7 00	2023	1851	68	21	1	6	-3720	16989	"
"	3223	"	XII 13	9 01	2110	1931	70	22	22	3	"	"	"	"

\* Morioka Ken Gikai, Entrance.  
 \*\* Weather Station Seismometer Room, on the Surface of the Concrete Block for Seismometer Installation.

Table VI. (Continued)

Pref.	No.	B.M.	Date 1952	Time	$\sum \delta T$	$SD$	$\frac{0.9150}{\times}$ $SD$	$h$ (cm)	$\frac{0.3086}{\times}$ $h$	$E.T.$	$\frac{0.87 \times}{\sum \delta T}$ Drift	$\sum \delta g$	$g$ 980.	Field Note No.
"	3224	6829	XII 13	9 18	7 17	1634	1495	77	24	- 3	6	-4154	16555	65
"	3225.1	6827	"	9 35	7 34	1220	1116	74	23	- 4	7	-4536	16173	"
"	3230	"	"	11 30	"	3618	3310	68	21	- 7	"	"	"	"
"	3231.1	6817	"	15 55	11 59	6008	5497	67	21	- 2	10	-2347	18362	"
"	3231.2	"	"	15 58	"	0174	0159	"	"	- 2	"	"	"	"
"	3232	6815	"	16 11	12 12	3672	3360	77	24	- 2	11	856	21565	"
"	3233.1	6813	"	16 26	12 27	5903	5401	51	16	- 2	11	2889	23598	"
"	3233.2	"	"	16 29	"	0174	0159	"	"	- 2	"	"	"	"
"	3234	6811	"	16 46	12 44	1720	1574	54	17	- 2	11	4305	25014	"
"	3235	J. 3	"	17 05	13 03	2586	2366	70	22	- 2	11	5102	25811	"
"	3253	"	XII 15	13 42	"	4125	3774	"	"	- 9	"	"	"	"
"	3254	6859	"	14 14	13 35	4264	3902	92	28	- 9	12	5235	25944	"
"	3255	6861	"	14 33	13 54	4521	4137	62	19	- 9	12	5461	26170	66
"	3256	6868	"	15 32	14 53	4788	4381	53	16	- 8	13	5702	26411	"
"	3257	6869	"	15 47	15 08	5931	5427	152	47	- 8	13	6779	27488	"
"	3258	6872	"	16 10	15 31	6337	5798	64	20	- 8	13	7123	27832	"
"	3259	6875	"	16 39	16 00	5664	5183	61	19	- 5	14	6509	27218	"
"	3260.1	6876	"	16 49	16 10	6138	5616	77	24	- 5	14	6947	27656	"
"	3260.2	"	"	16 55	"	1200	1098	"	"	- 5	14	"	"	"
"	3261	6879	"	17 17	16 32	1744	1596	75	23	- 5	14	7444	28153	"
"	3262	6881	"	17 34	16 49	2047	1873	48	15	0	15	7717	28426	"
"	3263	6884	"	18 10	17 25	2678	2450	60	19	0	15	8298	29007	"
"	3264	"	XII 16	8 54	"	2801	2563	58	18	- 7	"	"	"	"
"	3265	W.S.*	"	9 17	17 48	2022	1850	58	18	- 7	15	7585	28294	"
"	3266	6886	"	9 48	18 19	2873	2629	44	14	- 5	16	8361	29070	"

\* Weather Station Bench Mark.



"	3267	6888	"	10 10	18 41	3483	3187	53	16	5	16	8921	29530	"
"	3268-1	6891	"	10 45	19 16	4090	3742	96	30	- 4	17	9490	30199	"
"	3268-2	"	"	10 49	"	4770	4365	"	"	- 4	"	"	"	"
"	3269	6894	"	11 10	19 37	1537	1406	54	17	- 4	17	6518	27227	"
"	3270	6897	"	11 42	20 09	5765	5275	67	21	- 5	18	10389	31098	"
"	3271-1	6900	"	12 27	20 54	6188	5662	63	19	- 5	18	10774	31483	"
"	3271-2	"	"	12 30	"	1029	0942	"	"	- 7	"	"	"	"
"	3272	6932	"	17 53	26 17	5654	5173	71	22	- 4	23	15006	35715	"
"	3286	"	XII 18	9 19	26 33	5824	5329	72	22	- 9	"	"	"	"
"	3287	6934	"	9 35	26 33	6421	5875	76	23	- 8	23	15554	36263	"
"	3288	6937	"	10 36	27 34	5168	4729	74	23	- 6	24	14409	35118	"
"	3289	6939	"	11 01	27 59	5739	5251	70	22	- 6	24	14930	35639	"
"	3290-1	6941	"	11 24	28 22	6918	6330	57	18	- 6	25	16004	36713	"
"	3290-2	"	"	11 28	"	3172	2902	"	"	- 6	"	"	"	"
"	3291	6944	"	12 00	28 54	3029	2772	19	6	- 5	25	15863	36572	"
"	3292	6946	"	12 20	29 14	2915	2667	67	21	- 5	25	15773	36482	"
"	3293	6948	"	13 52	30 46	3034	2776	77	24	- 6	27	15882	36591	"
1	3294-1	6950	"	14 11	31 05	2479	2268	59	18	- 6	27	15368	36077	"

Route 27<sub>2</sub> B.M. 6932-B.M. 6907-B.M. 6932.

Pref.	No.	B.M.	Date	Time	$\Sigma\delta T$	SD	$0.915(\times SD)$	$h$	$0.3086(\times h)$	E.T.	$\Sigma\delta T$	$\Sigma\delta g$	$g$	Field Note No.
2	3273	6932	XII 17	9 10 <sup>h m</sup>	0 00	5759	5269	72	22	- 8	0	0	35715	66
"	3274	6930	"	9 30	20	4175	3820	9	3	- 6	- 1	-1465	34250	"
"	3275	6928	"	9 45	35	2564	2712	69	21	- 6	- 2	-2554	33161	"
"	3276	6926	"	10 00	50	4126	3775	49	15	- 6	- 3	-1496	34219	"
"	3277	6924	"	10 15	1 05	4154	3801	55	17	- 6	- 4	-1467	34248	"
"	3278	6922	"	10 34	1 24	3341	3057	71	22	- 5	- 5	-2204	33511	"
"	3279	6919	"	11 00	1 50	4037	0400	68	21	- 5	- 7	-4860	30855	"
"	3280-1	6917	"	11 21	2 11	3009	2753	83	26	- 5	- 8	-2501	33214	"
"	3280-2	"	"	11 28	4 54	6726	6154	"	"	- 5	- 8	-8057	27658	"
"	3281	6907	"	14 11	"	0669	0612	16	5	- 8	- 18	"	"	"

Table VI. (Continued)

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$	$0.3086 \times h$	$E.T.$	$-3.72 \times \Sigma \delta T$	$\Sigma \delta g$	$g$	Field Note No.
			1952					(cm)					980.	
2	3282	6908	XII 17	<sup>h</sup> 14 29	<sup>m</sup> 5 12	1876	1717	62	19	8	-19	-6937	28778	66
"	3283	6909	"	14 44	5 27	5267	4819	68	21	9	-20	-3833	31882	"
"	3284-1	6919	"	16 45	7 28	4114	3764	74	23	10	-28	-4879	30836	"
"	3284-2	"	"	16 48	"	0391	0358	"	"	-10	"	"	"	"
"	3285	6932	"	17 55	8 35	5716	5230	73	23	7	-32	0	35715	"
Route 27 <sub>3</sub> B.M.J. 3—Prefecture Boundary (No. 3248)—B.M.J. 3.														
Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$	$0.3086 \times h$	$E.T.$	$0.83 \times \Sigma \delta T$	$\Sigma \delta g$	$g$	Field Note No.
			1952					(cm)					980.	
2	3236	J. 3	XII 14	<sup>h</sup> 8 50	<sup>m</sup> 0 00	2667	2440	69	21	3	0	0	25811	65
"	3237	6808	"	9 20	30	2379	2177	64	20	3	0	-264	25347	"
"	3238	6804	"	10 44	1 54	1263	1156	63	19	4	2	-1289	24522	"
"	3239-1	6802	"	11 30	2 40	1791	1639	55	17	6	2	-810	25001	"
"	3239-2	"	"	11 38	"	6529	5974	"	"	6	"	"	"	"
"	3240	6799	"	12 30	3 32	5267	4819	65	20	7	3	-1964	23847	"
"	3241-1	"	"	13 16	4 18	6555	5998	27	8	7	4	-798	25013	"
"	3241-2	"	"	13 19	"	7490	6853	"	"	7	"	"	"	"
"	3242	6793	"	14 17	5 16	3237	2962	44	14	8	4	-4684	21127	"
"	3243	6790	"	14 35	5 34	5008	4582	47	15	8	5	-3064	22747	"
"	3244	6788	"	15 29	6 28	5325	4872	102	31	8	5	-2758	23053	"
"	3245	6787	"	15 47	6 46	4616	4224	193	60	5	6	-3375	22436	"
"	3246	6782	"	16 20	7 19	4192	3836	49	15	5	6	-3808	22003	"
"	3247	6779	"	16 48	7 47	3763	3443	75	23	1	6	-4189	21622	"
"	3248	P.B.**	"	17 12	8 11	2836	2595	27	8	1	7	-5053	20758	"

\* Entrance of the Okkirai Primary School.

\*\* Prefecture Boundary.

"	3249	6790	"	18 46	9 45	5026	4599	44	14	9	8	-3034	22777	"
"	3250.2	"	XII 15	9 03	9 30	5976	5468	47	15	5	8	-7847	17964	"
"	3251	6794	"	10 12	11 14	0713	0652	55	17	4	9	-1929	23882	"
"	3252.1	6799	"	10 32	10 34	7178	6568	66	20	4	9			"
"	3252.2	"	"	10 34	13 42	2010	1839	"	"	4	12	0	25811	"
"	3253	J. 3	"	13 42	14 22	4125	3774	70	22	9				"

Route 27<sub>4</sub> B.M. 6827—B.M. 6820—B.M. 6827.

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	SD	$\frac{0.9150}{SD}$	$h$	$\frac{0.3086}{h}$	E.T.	$\frac{-4.44}{\Sigma \delta T}$	$\Sigma \delta g$	$g$	Field Note No.
2	3225.2	6827	XII 13	9 39 <sup>h m</sup>	0 00	5973	5465	74	23	4	0	0	16173	65
"	3226	6825	"	9 51	12	5241	4796	58	18	4	-1	-673	15500	"
"	3227	6823	"	10 09	30	4245	3884	56	17	4	-2	-1585	14588	"
"	3228	6820	"	10 39	1 00	1552	1420	75	23	5	-4	-4042	12131	"
"	3229.1	6821	"	10 54	1 15	2503	2290	64	20	5	-6	-3173	13000	"
"	3229.2	"	"	10 56		0151	0138	"	"	5				"
"	3230	6827	"	11 30	1 49	3618	3310	68	21	7	-8	0	16173	"

Route 27<sub>5</sub> B.M. 5470—B.M.J. 5466—B.M. 5470.

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	SD	$\frac{0.9150}{SD}$	$h$	$\frac{0.3086}{h}$	E.T.	$\frac{-5.83}{\Sigma \delta T}$	$\Sigma \delta g$	$g$	Field Note No.
2	3189	5470	XII 11	13 59 <sup>h m</sup>	0 00	5952	5446	66	20	6	0	0	17766	64
"	3190	5468	"	14 10	11	5865	5366	67	21	6	-1	-78	17688	"
"	3191	J. 5466	"	14 21	22	6566	6008	69	21	6	-2	565	18331	"
"	3212	"	XII 12	13 08		6720	6149	70	22	7	-7	0	17766	65
"	3213.1	5470	"	13 56	1 10	6099	5581	64	20	7	-7	0	17766	"

Route 27<sub>e</sub> B.M.J. 5466—B.M. 5536—B.M. 6854—B.M.J. 5466.

Pref.	No.	B.M.	Date 1952	Time	$\Sigma\delta T$	$\frac{0.9150}{SD}$	$h$ (cm)	$0.3086 \times h$	$\frac{1.74 \times \Sigma\delta T}{E.T.}$	$\Sigma\delta g$	$g$ 980.	Field Note No.
				<sup>h</sup> <sup>m</sup>								
2	3206	J. 5466	XII 12	10 52	0 00	6713	70	22	4	0	18331	65
"	3207	5529	"	11 13	21	5061	60	19	4	1	16816	"
"	3208	5531	"	11 20	28	4149	67	21	4	1	15983	"
"	3209	5533	"	11 32	40	2493	64	20	6	1	14677	"
"	3210	5536	"	11 51	59	2025	67	21	6	2	14041	"
"	3211	6854	"	12 47	1 55	7248	76	23	7	3	18816	"
"	3212	J. 5466	"	13 08	2 16	6720	70	22	7	4	18331	"

Route 27<sub>f</sub> B.M.J. 5466—B.M. 5441—B.M.J. 5466.

Pref.	No.	B.M.	Date 1952	Time	$\Sigma\delta T$	$\frac{0.9150}{SD}$	$h$ (cm)	$0.3086 \times h$	$\frac{6.29 \times \Sigma\delta T}{E.T.}$	$\Sigma\delta g$	$g$ 980.	Field Note No.
				<sup>h</sup> <sup>m</sup>								
2	3191	J. 5466	XII 11	14 21	0 00	6566	69	21	6	0	18331	64
"	3192	5464	"	14 49	28	5422	64	20	4	3	17282	"
"	3193	5462	"	15 05	44	3807	59	18	4	4	15801	"
"	3194	5460	"	15 17	56	4461	69	21	4	6	16401	65
"	3195	5458	"	15 30	1 09	4783	51	16	1	8	16691	"
"	3196	Mizusawa I.L.O.*	"	15 55	1 34	4081	27	8	1	10	16039	"
"	3197	5455	"	16 11	50	4591	4201	13	1	11	16510	"
"	3198	5453	"	16 25	2 04	3994	3655	62	1	13	15968	"
"	3199	5451	"	16 42	2 21	5567	5094	68	2	15	17410	"
"	3200	5447	"	17 10	2 49	6053	5538	48	2	18	17845	"
"	3201	5445	"	17 30	3 09	6231	5701	59	5	20	18012	"
"	3202	5443	"	18 00	3 39	5697	5213	65	5	23	17523	"
"	3203	5441	"	18 23	4 02	3053	2793	67	5	25	15102	"
"	3204	5443	"	18 38	4 17	5701	5216	65	6	27	17523	"
"	3205	"	XII 12	8 58	8 58	5812	5318	76	23	-1	-808	"
"	3206	J. 5466	"	10 52	6 11	6713	6142	70	22	0	18331	"

\* International Latitude Observatory, Underground Room for Tiltmeter Observation.

Table VII. Results along the Route 30, (0.01 mgal.).  
Route 30<sub>g</sub> B.M.J. 2052—B.M. 2094—B.M.J. 2052.

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$\frac{0.9150}{SD}$	$h$ (cm)	$\frac{0.3086}{h}$	E.T.	$5.24 \times \Sigma \delta T$ Drift	$\Sigma \delta g$	$g$	Field Note No.
			1953										979.	
8	3579	J. 2052	III 12	<sup>h</sup> 10 09	<sup>m</sup> 0 00	2457	2248	93	29	0	0	0	94354	69
"	3580	2054	"	10 21	12	1803	1650	59	18	0	1	610	93754	"
"	3581	2056	"	10 31	22	1670	1528	52	16	- 1	2	- 736	93628	"
"	3582 <sub>1</sub>	2058	"	10 45	36	0564	0516	71	22	- 1	3	- 1743	92621	"
"	3582 <sub>2</sub>	"	"	10 49		6458	5909	71	"	- 1				"
"	3583	2060	"	11 00	47	5367	4911	66	20	- 1	4	- 2744	91620	"
"	3584	2062	"	11 12	59	4977	4554	69	21	- 1	5	- 3101	91263	"
"	3585	2064	"	11 22	1 09	4598	4207	9	3	- 1	6	- 3467	90897	"
"	3586	2066	"	11 33	1 20	4405	4031	63	19	- 3	7	- 3630	90734	"
"	3587	2068	"	11 42	1 29	4227	3868	43	13	- 3	8	- 3800	90564	"
"	3588	2070	"	11 52	1 39	3002	2747	61	19	- 3	9	4916	89448	"
"	3589	2072	"	12 10	1 57	2255	2063	58	18	- 3	10	- 5602	88762	"
"	3590	2074	"	12 20	2 07	1769	1619	55	17	- 3	11	- 6048	88316	"
"	3591	2076	"	12 30	2 17	1905	1743	38	12	- 6	12	- 5933	88431	"
"	3592	2078	"	12 40	2 27	2580	2361	51	16	- 6	13	- 5312	89052	"
"	3593	2080	"	12 50	2 37	3080	2818	47	15	- 6	14	- 4857	89507	"
"	3594	2082	"	13 35	3 22	4439	4062	55	17	- 7	18	- 3616	90748	"
"	3595	2084	"	13 46	3 33	4783	4376	47	15	- 7	19	- 3305	91059	"
"	3596	2086	"	13 56	3 43	4326	3958	32	10	- 7	19	- 3728	90636	"
"	3597	2088	"	14 33	4 20	3438	3146	55	17	- 7	23	- 4537	89827	"
6	3598	2091	"	15 10	4 57	3163	2894	56	17	- 7	26	- 4792	89572	"
"	3599	2094	"	15 27	5 14	5345	4891	56	17	- 7	27	- 2796	91568	"
8	3600	2086	"	16 16	6 03	4339	3970	31	10	- 5	32	- 3727	90637	"
"	3601	2082	"	17 07	6 54	4457	4078	53	16	- 2	36	- 3614	90750	"
"	3602 <sub>1</sub>	"	III 13	11 39	8 09	2209	2021	56	17	- 1				"
"	3603	J. 2052	"	12 54		6157	5634	93	29	- 3	43	0	94364	"

Table VIII. Results along the Route 32. (0.01 mgal.)  
Route 32<sub>1</sub> B.M.J. 10—B.M. 6656—B.M.J. 10.

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$12.35 \times \Sigma \delta T$ Drift	$\Sigma \delta g$	$g$ 979.	Field Note No.
6	4119	J. 10	1953	13 42 <sup>h</sup> 13 42 <sup>m</sup>	0 00 <sup>h</sup> 0 00 <sup>m</sup>	5918	5415	66	20	5	0	0	84678	76
"	4120	6667	"	14 35	53	4822	4412	57	17	4	11	-1018	83660	"
"	4121 <sub>1</sub>	6664	"	14 51	1 09	1768	1618	51	16	4	15	-3817	80861	"
"	4121 <sub>2</sub>	"	"	14 54	"	7748	7089	"	"	4	"	"	"	"
"	4122	6662	"	15 18	1 33	5351	4896	58	18	4	20	-6013	78665	"
8	4123	6658	"	15 42	1 57	5472	5007	63	19	3	25	-5907	78771	"
"	4124 <sub>1</sub>	6656	"	16 03	2 18	6868	6284	66	20	3	28	-4632	80046	"
"	4124 <sub>2</sub>	"	"	16 08	"	0137	0125	"	"	3	"	"	"	"
6	4125	J. 10	"	17 14	3 24	5218	4774	64	20	0	42	0	84678	"

Route 32<sub>2</sub> B.M.J. 4264—B.M.J. 10—Sei 4—B.M.J. 4264.

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$10.36 \times \Sigma \delta T$ Drift	$\Sigma \delta g$	$g$ 979.	Field Note No.
6	4108	J. 4264	1953	9 31 <sup>h</sup> 9 31 <sup>m</sup>	0 00 <sup>h</sup> 0 00 <sup>m</sup>	5100	4667	73	23	4	0	0	92732	76
"	4109	Wakamatsu W.S.*	"	10 04	33	5094	4661	34	10	4	6	25	92707	"
"	4110	6689	"	10 24	53	5037	4609	73	23	4	9	67	92665	"
"	4111	6687	"	10 35	1 04	5330	4877	65	20	2	11	198	92930	"
"	4112	F. 1**	"	11 09	1 38	3965	3628	49	15	2	17	-1062	91670	"
"	4113	6680	"	11 56	2 25	2349	2149	59	18	1	25	-2543	90189	"
"	4114 <sub>1</sub>	"	"	12 35	3 04	0091	0083	75	23	3	32	-4609	88123	"
"	4114 <sub>2</sub>	"	"	12 38	"	5398	4939	"	"	3	33	4908	87824	"
"	4115	6677	"	12 44	3 10	5077	4645	60	19	3	35	-6218	86514	"
"	4116	6674	"	13 00	3 26	3642	3332	78	24	3	"	"	"	"

\* Weather Station, Nail of the Shelter No. 1.

\*\* Fukushima Prefecture Bench Mark.

"	4117	6672	"	13 12	3 38	3202	2930	76	23	3	37	6623	86109	"
"	4118-1	6670	"	13 27	3 53	2950	2699	68	21	3	40	6859	85873	"
"	4118-2	"	"	13 29	"	7223	6609	"	"	3	"	"	"	"
"	4119	J. 10	"	13 42	4 06	5918	5415	66	20	5	42	8054	84678	"
"	4125	"	"	17 14	"	5218	4774	64	20	0	"	"	"	"
"	4126	6693	"	17 30	4 22	4163	3809	60	19	3	46	9027	83705	"
"	4127-1	6695	"	17 48	4 40	0095	0087	57	18	3	49	12753	79979	77
"	4127-2	"	"	17 53	"	5351	4905	"	"	3	"	"	"	"
"	4128-1	6704	"	18 51	5 38	4164	3810	58	18	7	58	13861	78871	"
"	4128-2	"	"	18 58	"	0142	0130	"	"	7	"	"	"	"
"	4129	6706	"	19 12	5 52	4099	3751	66	20	7	61	10241	82491	"
"	4130	6707	"	19 26	6 06	5528	5058	60	19	7	63	8937	83795	"
"	4131	"	VIII 1	8 28	"	5613	5136	59	18	2	"	"	"	"
"	4132	6709	"	8 43	6 21	6487	5936	53	16	0	66	8144	84588	"
"	4133-1	6711	"	8 55	6 33	7130	6524	52	16	0	68	7558	85174	"
"	4133-2	"	"	9 00	"	0423	0387	"	"	0	"	"	"	"
"	4134	6713	"	9 13	6 46	1718	1572	54	17	0	70	6374	86358	"
"	4135	6715	"	9 29	7 02	2516	2302	59	18	0	73	5646	87086	"
"	4136	6717	"	9 42	7 15	3341	3057	51	16	2	76	4898	87834	"
"	4137	6719	"	9 54	7 27	3797	3474	60	19	2	78	4480	88252	"
"	4138	6721	"	10 07	7 40	4555	4168	70	22	2	80	3785	88947	"
"	4139	Sei 34	"	10 56	8 29	4939	4519	54	17	2	88	3447	89285	"
"	4140	Sei 28	"	11 57	9 30	6196	5669	61	19	2	98	2305	90427	"
"	4141	Sei 24	"	12 22	9 55	5965	5458	43	13	2	103	2527	90205	"
"	4142	Sei 20	"	12 55	10 28	6140	5618	62	19	1	109	2356	90366	"
"	4143-1	"	"	13 30	11 03	7812	7148	75	23	1	115	836	91896	"
"	4143-2	Sei 10	"	13 32	"	1436	1314	"	"	1	"	"	"	"
"	4144	Sei 4	"	14 50	12 21	1748	1599	54	17	1	128	570	92162	"
"	4145	J. 4264	"	15 30	13 01	1884	1724	54	17	1	135	454	92278	"
"	4146	"	"	16 30	14 01	2385	2182	73	23	1	145	0	92732	"

B.M. Printed in Gothic Type are 2nd Order Bench Marks.

Route 32<sub>3</sub> B.M.J. 4264—B.M. 4377—B.M.J. 4264.

Pref.	No.	B.M.	Date 1953	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$9.70 \times \Sigma \delta T$ Drift	$\Sigma \delta g$	$g$ 979.	Field Note No.
6	4094	J. 4264	VII 30	<sup>h</sup> 12 13	0 00	6452	5904	73	23	6	0	0	92732	76
"	4095	4354	"	<sup>h</sup> 13 43	1 30	6401	5857	67	21	9	15	61	92671	"
"	4096	4356	"	<sup>h</sup> 13 56	1 43	6335	5797	61	19	9	16	124	92608	"
"	4097	4358	"	<sup>h</sup> 14 11	1 58	6193	5667	68	21	9	19	255	92477	"
"	4098	4360	"	<sup>h</sup> 14 24	2 11	4775	4369	46	14	9	21	1562	91170	"
"	4099	4362	"	<sup>h</sup> 14 40	2 27	5284	4835	48	15	7	24	1100	91632	"
"	4100	4365	"	<sup>h</sup> 15 10	2 57	2309	2113	63	19	7	29	3823	89909	"
"	4101	4367	"	<sup>h</sup> 15 25	3 12	6946	6356	71	22	7	31	421	93153	"
"	4102.1	4368	"	<sup>h</sup> 16 50	4 37	7571	6927	42	13	—	45	961	93693	"
"	4102.2	"	"	<sup>h</sup> 16 53		1466	1341	"	"	—	1			"
"	4103	4370	"	<sup>h</sup> 17 09	4 53	2365	2164	58	18	1	48	1786	94518	"
"	4104	4372	"	<sup>h</sup> 17 23	5 07	4311	3945	61	19	—	49	3567	96299	"
"	4105	4374	"	<sup>h</sup> 17 45	5 29	4130	3779	65	20	—	53	3393	96125	"
14	4106.1	4377	"	<sup>h</sup> 18 10	5 54	3234	2959	69	21	—	57	2570	95302	"
"	4106.2	"	"	<sup>h</sup> 18 18		7787	7125	"	"	—	6			"
6	4107	J. 4264	VII 31	<sup>h</sup> 1 42	13 18	5043	4614	74	23	5	129	0	92732	"

Route 32<sub>4</sub> B.M.J. 4264—B.M. 4477—B.M.J. 4264.

Pref.	No.	B.M.	Date 1953	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$9.17 \times \Sigma \delta T$ Drift	$\Sigma \delta g$	$g$ 979.	Field Note No.
6	4086	J. 4264	VII 30	<sup>h</sup> 8 37	0 00	6430	5883	73	23	6	0	0	92732	76
"	4087	4465	"	<sup>h</sup> 8 53	16	6733	6161	75	23	—	3	275	93007	"
"	4088	4467	"	<sup>h</sup> 9 08	31	7113	6508	62	19	—	6	616	93348	"
"	4089	4469	"	<sup>h</sup> 9 18	41	7113	6508	71	22	—	6	618	93350	"
"	4090	4471	"	<sup>h</sup> 9 32	55	7025	6428	73	23	—	8	540	93272	"



4091	4092	4093	4094	4473	4476	4477	J. 4264	9 56	1 19	6525	5970	61	19	3	12	74	92806	"	
"	"	"	"	"	"	"	"	10 03	1 26	4817	4408	59	18	3	13	-1490	91242	"	
"	"	"	"	"	"	"	"	11 03	2 26	3570	3267	59	18	3	22	-2636	90096	"	
"	"	"	"	"	"	"	"	12 13	3 36	6452	5904	73	23	6	33	0	92732	"	
Route 32 <sub>3</sub> B.M.J. 2114—B.M.J. 4264—B.M.J. 2114.																			
6	4072	J. 2114	1953	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$	$0.3086 \times h$	$E.T.$	$12.17 \times \Sigma \delta T$	$\Sigma \delta g$	$g$	Field Note No.					
"	4073	4238	VIII 29	<sup>h</sup> 12 53	<sup>h</sup> 0 00	4595	4204	58	18	13	0	0	97409	76					
"	4074	4240	"	13 45	52	3610	3303	49	15	12	11	-916	96493	"					
"	4075. <sub>1</sub>	4242	"	13 58	1 05	3242	2966	47	15	12	13	-1255	96154	"					
"	4075. <sub>2</sub>	"	"	14 10	1 17	0910	0833	62	19	12	16	-3387	94022	"					
"	4076	4244	"	14 27	1 31	7528	6888	53	16	12	18	-3530	93879	"					
"	4077	4246	"	14 40	1 44	5753	5264	71	22	7	21	-5156	92253	"					
"	4078	4248	"	14 58	2 02	3238	2963	50	15	7	24	-7467	89942	"					
"	4079	4250	"	15 10	2 14	1683	1540	55	17	7	27	-8891	88518	"					
"	4080	4253	"	15 33	2 37	1073	0982	65	20	2	32	-9456	87953	"					
"	4081	4255	"	15 45	2 49	1320	1208	50	15	2	34	-9237	88172	"					
"	4082	4257	"	16 12	3 16	1916	1753	88	27	2	40	-8686	88723	"					
"	4083	4259	"	16 31	3 35	2201	2014	60	19	0	44	-8439	88970	"					
"	4084	4262	"	16 51	3 55	5424	4963	68	21	0	47	-5491	91918	"					
"	4085	J. 4264	"	17 09	4 13	6316	5779	72	22	1	51	-4677	92732	"					
"	4147. <sub>2</sub>	"	VIII 2	9 19	6 52	0101	0092	"	"	5	84	0	97409	77					
"	4148	J. 2114	"	11 58		5259	4812	60	19	-2				"					

Route 326 B.M.J. 2114—B.M. 2094—B.M.J. 2114.

Pref.	No.	B.M.	Date 1953	Time	$\sum \delta T$	$SD$	$0.9150$ $\times$ $SD$	$h$ $\times$ $h$	$0.3086$ $\times$ $h$	$E.T.$	$11.55$ $\times$ $\sum \delta T$ Drift	Adjust- ment	$\sum \delta g$	$g$ 979.	Field Note No.
6	4148	J. 2114	VIII 2	11 58 <sup>h m</sup>	0 00	5259	4812	60	19	— 2	0	0	0	97409	77
"	4149	2112	"	12 13	15	4755	4351	47	15	— 2	3	— 1	— 467	96942	"
"	4150	2110	"	12 26	28	4030	3687	58	18	— 2	6	— 3	— 1129	96280	"
"	4151	2108	"	12 40	42	4128	3777	50	15	— 3	8	— 3	— 1045	96364	"
"	4152	2106	"	13 35	1 37	3167	2898	52	16	— 3	18	— 5	— 1931	95478	"
"	4153	2104	"	13 46	1 48	2227	2038	59	18	— 3	21	— 7	— 2790	94619	"
"	4154	2102	"	13 57	1 59	1880	1720	63	19	— 3	23	— 7	— 3109	94300	"
"	4155-1	2100	"	14 10	2 12	1075	0984	65	20	— 3	25	— 9	— 3844	93565	"
"	4155-2	"	"	14 15	"	3280	3001	"	"	— 3	"	"	"	"	"
"	4156	2098	"	14 30	2 27	4625	4232	37	11	— 3	29	— 6	— 2629	94780	"
"	4157	2096	"	14 44	2 41	2714	2483	48	15	— 3	31	— 10	— 4372	93037	"
"	4158	2094	"	14 58	2 55	1102	1008	60	19	— 3	33	— 14	— 5841	91568	"
"	4159	Shirakawa W.S.*	"	16 20	4 17	0918	0840	— 16	— 5	— 3	50	— 14	— 6050	91359	"
"	4160	J. 2114	"	17 53	5 50	7538	6897	60	— 19	— 3	67	— 0	0	97409	"

\* Weather Station, Concrete Foot of the Shelter in the Observation Field.

Route 327 (No. 4060)—B.M.J. 2114—B.M.J. 4201—B.M. 5578—(No. 4220-1).

Pref.	No.	B.M.	Date 1953	Time	$\sum \delta T$	$SD$	$0.9150$ $\times$ $SD$	$h$ $\times$ $h$	$0.3086$ $\times$ $h$	$E.T.$	$8.42$ $\times$ $\sum \delta T$ Drift	Adjust- ment	$\sum \delta g$	$g$ 980.	Field Note No.
6	4060	*	VII 29	9 13 <sup>h m</sup>	0 00	3340	3056	27	8	— 3	0	0	0	02037	75
"	4061	2135	"	9 25	12	3500	3203	68	21	— 3	2	158	02195	"	
"	4062	2133	"	9 40	27	1231	1126	130	40	— 2	4	— 1897	00140	"	
"	4063	2131	"	9 55	42	1269	1161	32	10	— 2	6	— 1894	00143	"	
"	4064-2	"	"	10 36	"	7578	6934	30	9	— 7	"	"	"	"	

\* Fukushima, Nippon Kogyo Bank, Entrance.

"	4065	2129	"	10 49	55	6187	5661	59	18	7	8	979.	"
"	4066	2127	"	11 02	1 08	6878	6293	45	14	7	9	98877	"
"	4067	2123	"	11 45	1 51	4949	4528	38	12	10	16	99504	76
"	4068	2121	"	11 57	2 03	4705	4305	68	21	10	18	97733	"
"	4069	2119	"	12 08	2 14	4341	3972	71	22	11	19	97517	"
"	4070	2117	"	12 28	2 34	4466	4086	66	20	11	22	97185	"
"	4071	2115	"	12 41	2 47	4732	4330	59	18	13	24	97294	"
"	4072	J. 2114	"	12 53	2 59	4595	4204	58	18	13	25	97536	"
"	4161	"	VIII 3	9 21	7649	6999	6135	60	19	6	30	97409	77
"	4162	4235	"	9 56	3 34	6705	6135	52	16	3	30	96534	"
"	4163	4233	"	10 15	3 53	5991	5482	77	24	3	33	95886	"
"	4164	4231	"	10 30	4 08	4603	4212	86	27	1	35	94615	"
"	4165	4229	"	10 46	4 24	4491	4109	51	16	1	37	-7422	"
"	4166	4227	"	11 07	4 45	2863	2620	58	18	1	40	-7538	"
"	4167	4225	"	11 25	5 03	4681	4283	103	32	1	43	-9028	"
"	4168	4228	"	11 40	5 18	6117	5597	55	17	1	45	-7354	"
"	4169	4221	"	13 02	6 40	6619	6056	56	17	2	56	-6057	"
"	4170	4219	"	13 19	6 57	6335	5797	42	13	2	59	-5612	"
"	4171.1	4218	"	13 29	7 07	7176	6566	63	19	2	60	-5878	"
"	4171.2	"	"	13 32	7 07	0283	0259	"	"	4	60	-5104	"
"	4172	4215	"	13 51	7 26	2101	1922	54	17	4	62	95980	"
"	4173	4213	"	14 07	7 42	3064	2804	63	19	4	65	-3445	"
"	4174	4211	"	14 21	7 56	4822	4412	54	17	4	67	99473	"
"	4175.1	4209	"	14 48	8 23	6414	5869	69	21	5	71	980.	"
"	4175.2	"	"	14 53	8 23	0052	0048	"	"	5	71	01077	"
"	4176	4207	"	15 10	8 40	1585	1450	68	21	5	73	02533	"
"	4177	4205	"	15 23	8 53	2066	1890	89	27	5	75	03933	"
"	4178	4203	"	15 36	9 06	2305	2109	49	15	5	77	04377	"
"	4179	J. 4201	"	16 13	9 43	1208	1105	64	20	5	82	2545	"
"	4188	"	VIII 4	9 12	9 43	2663	2437	66	20	10	82	1541	"
"	4189	5627	"	9 22	9 53	2716	2485	68	21	10	83	03578	78
"	4190	5625	"	9 35	10 06	2371	2169	40	12	10	85	1896	"
"	4191	5623	"	9 50	10 21	2498	2286	49	15	8	88	2340	"
"	4192	5621	"	10 13	10 44	2158	1975	62	19	8	90	04582	"
"	4193	5619	"	10 25	10 56	1547	1416	65	20	8	92	1541	"

Table VIII. (Continued)

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$	$0.3086 \times h$	$E.T.$	$8.42 \times \Sigma \delta T$	$\Sigma \delta g$	$g$	Field Note No.
6	4194	5617	VIII 4	10 39	11 10	2241	2051	60	19	4	94	1136	03173	78
"	4195	5615	"	10 55	11 26	2256	2064	50	15	4	96	1143	03180	"
"	4196	5613	"	11 08	11 39	2475	2265	48	15	4	99	1341	03378	"
"	4197	5611	"	11 24	11 55	4048	3704	54	17	4	100	2781	04818	"
"	4198	5609	"	11 36	12 07	4375	4003	30	9	1	102	3067	05104	"
"	4199	5607	"	11 48	12 19	5530	5060	71	22	1	104	4135	06172	"
"	4200	5605	"	12 02	12 33	5332	4879	51	16	1	106	3946	05983	"
"	4201	5603	"	12 16	12 47	5092	4659	30	9	1	108	3717	05754	"
"	4202	5601	"	12 38	13 09	6355	5815	51	16	-	111	4874	06911	"
"	4203	5599	"	12 50	13 21	6592	6032	36	11	-	113	5084	07121	"
"	4204 <sup>1</sup>	5597	"	13 49	14 20	7620	6972	46	14	3	120	6019	08056	"
"	4204 <sup>2</sup>	"	"	13 52	"	1439	1317	"	"	-	3	"	"	"
"	4205	5595	"	14 05	14 33	2341	2142	85	26	3	123	6853	08890	"
"	4206	5593	"	14 18	14 46	3292	3012	40	12	3	125	7707	09744	"
"	4207	5591	"	14 30	14 58	3599	3293	61	19	-	126	7991	10028	"
"	4208	5589	"	14 40	15 08	2580	2361	67	21	6	127	7060	09097	"
"	4209	5586	"	14 57	15 25	2605	2384	54	17	-	130	7076	09113	"
"	4210	5584	"	15 10	15 38	3638	3329	69	21	-	131	8024	10061	"
"	4211	5582	"	15 23	15 51	3793	3471	48	15	-	134	8157	10194	"
"	4212	5580	"	15 35	16 03	4402	4028	63	19	-	136	8715	10752	"
"	4213	5578	"	15 48	16 16	4502	4119	73	23	-	137	8809	10846	"
"	4218 <sup>2</sup>	"	VIII 5	9 51	"	7752	7093	"	"	11	141	4481	06518	"
"	4219 <sup>1</sup>	"	"	10 21	16 46	3051	2792	"	"	11	141	4481	06518	"
"	4219 <sup>2</sup>	"	"	10 24	"	7658	7007	"	"	11	141	4481	06518	"
"	4220 <sup>1</sup>	*	"	11 58	18 20	2773	2537	27	8	5	154	0	02037	"

\* Fukushima, Nippon Kogyô Bank, Entrance.

Route 32<sub>8</sub> B.M.J. 4201—B.M. 4187—B.M.J. 4201.

Pref.	No.	B.M.	Date 1953	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$11.71 \times \Sigma \delta T$ Drift	Adjust- ment	$\Sigma \delta g$	$g$ 980.	Field Note No.
6	4179	J. 4201	VIII 3	16 13 <sup>h</sup> 0 00 <sup>m</sup>	0 00 <sup>h</sup> 0 00 <sup>m</sup>	1208	1105	64	20	— 5	0	0	0	03578	77
"	4180	4199	"	16 40 <sup>h</sup> 16 40 <sup>m</sup>	27	1720	1574	49	15	— 5	6	15	443	04021	"
"	4181	4197	"	16 53 <sup>h</sup> 16 53 <sup>m</sup>	40	1820	1665	71	22	— 5	8	18	536	04114	"
"	4182 <sub>1</sub>	4195	"	17 07 <sup>h</sup> 17 07 <sup>m</sup>	54	0725	0663	50	15	— 5	11	— 15	— 443	03135	"
"	4182 <sub>2</sub>	"	"	17 10 <sup>h</sup> 17 10 <sup>m</sup>		2050	1876	"	"	— 5					"
"	4183	4193	"	17 23 <sup>h</sup> 17 23 <sup>m</sup>	1 07	1782	1631	60	19	— 5	13	— 23	— 678	02900	"
"	4184	4191	"	17 36 <sup>h</sup> 17 36 <sup>m</sup>	1 20	2221	2032	64	20	— 5	15	— 10	— 291	03287	"
"	4185	4189	"	17 55 <sup>h</sup> 17 55 <sup>m</sup>	1 39	2318	2121	47	15	— 5	20	— 17	— 215	03363	"
"	4186	4187	"	18 10 <sup>h</sup> 18 10 <sup>m</sup>	1 54	1979	1811	64	20	— 5	22	— 17	— 512	03066	"
"	4187	J. 4201	"	19 48 <sup>h</sup> 19 48 <sup>m</sup>	3 32	2577	2358	67	21	— 5	41	— 0	— 0	03578	78

Route 32<sub>9</sub> B.M. 5578—B.M. 5572—B.M. 5578.

Pref.	No.	B.M.	Date 1953	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$4.17 \times \Sigma \delta T$ Drift	$\Sigma \delta g$	$g$ 980.	Field Note No.
6	4213	5578	VIII 4	15 48 <sup>h</sup> 0 00 <sup>m</sup>	0 00 <sup>h</sup> 0 00 <sup>m</sup>	4502	4119	73	23	— 7	0	0	10846	78
"	4214	5576	"	16 03 <sup>h</sup> 16 03 <sup>m</sup>	15	4457	4078	54	17	— 7	1	— 48	10798	"
"	4215	5574	"	16 14 <sup>h</sup> 16 14 <sup>m</sup>	26	4155	3802	54	17	— 7	2	— 325	10521	"
"	4216	5572	"	16 31 <sup>h</sup> 16 31 <sup>m</sup>	43	3846	3519	45	14	— 7	3	— 612	10234	"
"	4217	5578	"	17 01 <sup>h</sup> 17 01 <sup>m</sup>	1 13	4508	4125	72	22	— 7	5	— 0	10846	"

Route 32<sub>10</sub> (No. 4051)—B.M. 2147—(No. 4060).

Pref.	No.	B.M.	Date	Time	$\sum \delta T$	SD	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	E.T.	$14.62 \times \sum \delta T$ Drift	$\sum \delta g$	$g$ 980.	Field Note No.
			1953											
6	4051	**	VII 28	<sup>h</sup> 15 04	<sup>h</sup> 0 00	3181	2911	27	8	10	0	0	02037	75
"	4052	Fukushima W.S.**	"	15 23	19	3369	3083	59	18	10	4	178	02215	"
"	4053	2138	"	15 45	41	3031	2773	73	23	5	10	-138	01899	"
"	4054	2140	"	15 57	53	2765	2530	48	15	5	13	-392	01645	"
"	4055	2143	"	16 20	1 16	3069	2808	47	15	5	19	-120	01917	"
"	4056	2145	"	16 35	1 31	3541	3240	67	21	2	22	308	02345	"
"	4057	2147	"	16 47	1 43	3049	2790	28	9	2	25	-157	01880	"
"	4058	2141	"	17 16	2 12	3669	3357	49	15	2	32	409	02446	"
"	4059	"	VII 29	8 48	8 48	3773	3452	"	"	3	"	"	"	"
"	4060	*	"	9 13	2 37	3340	3056	27	8	1	38	0	02037	"

\* Fukushima Nippon Kogyo Bank, Entrance.  
 \*\* Weather Station Bench Mark.

Table IX. Results along the Route 34. (0.01 mgal.).

Route 34<sub>1</sub> B.M.M. 1—B.M.J. 2—Prefecture Boundary (No. 4574)—(No. 4575)—B.M. 5424—Sendai—B.M.M. 1.

Pref.	No.	B.M.	Date	Time	$\sum \delta T$	SD	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	E.T.	$5.56 \times \sum \delta T$ Drift	$\sum \delta g$	$g$ 980.	Field Note No.
			1953											
3	4526	M. 1*	IX 23	<sup>h</sup> 12 26	<sup>h</sup> 0 00	2684	2456	48	15	8	0	0	10381	83
"	4527	5649	"	14 50	2 24	4698	4299	47	15	4	13	1818	12199	"
"	4528	5651	"	15 04	2 38	5875	5376	55	17	4	14	2896	13277	"
"	4529.1		"	15 30	3 04	7077	6475	—	—	8	17	3971	14352	"
"	4529.2		"	15 34		0062	0057	—	—	8				"

\* Miyagi Prefecture Bench Mark.

"	4530	5654	"	15 40	3 10	1130	1034	71	22	- 8	18	4969	15350	"
"	4531	5656	"	15 53	3 23	0309	0283	48	15	- 8	19	4210	14591	"
"	4532.1		"	16 35	4 05	0257	0235	--	--	-11	23	4140	14521	"
"	4532.2		"	16 37		6400	5856	--	--	-11				"
"	4533	5659	"	16 52	4 20	5740	5252	63	19	-11	24	3554	13935	"
"	4534	5661	"	17 17	4 45	5057	4627	68	21	-11	27	2928	13309	"
"	4535	5663	"	17 33	5 01	3668	3356	60	19	-11	28	1654	12035	"
"	4536	5665	"	17 58	5 26	4343	3974	74	23	-11	30	2274	12655	"
"	4537.1		"	19 21	6 49	7418	6787	--	--	- 8	38	5059	15440	"
"	4537.2		"	19 23		2348	2148	--	--	- 8				"
"	4538	5671	"	19 31	6 57	3487	3191	66	20	- 3	39	6126	16507	"
"	4539	J. 2	"	19 45	7 11	5054	4624	62	19	- 3	40	7557	17938	"
"	4550	"	IX 24	20 24		5213	4770	"	"	- 6				"
"	4551	5673	"	20 40	7 27	5690	5206	54	17	0	42	7995	18376	"
"	4552	5675	"	20 55	7 42	5246	4800	48	15	0	43	7586	17967	"
"	4553	5676	"	21 10	7 57	4974	4551	63	19	0	44	7340	17721	"
"	4554	5679	"	21 43	8 30	4352	3982	68	21	6	47	6776	17157	"
"	4555	5682	"	22 04	8 51	5001	4576	54	17	6	49	7364	17745	"
"	4556	5684	"	22 24	9 11	5348	4893	61	19	6	51	7681	18062	"
"	4557	5687	"	23 00	9 47	5565	5092	61	19	11	54	7882	18263	"
"	4558	5689	"	23 17	10 04	5830	5334	62	19	11	56	8122	18503	"
"	4559	5691	"	23 37	10 24	4013	3672	62	19	14	58	6461	16842	"
"	4560	5693	"	23 53	10 40	6382	5840	55	17	14	59	8626	19007	"
"	4561	5696	IX 25	0 15	11 02	6775	6199	58	18	14	61	8984	19365	"
"	4562	"	"	9 34		6865	6281	54	17	- 2				"
"	4563	5698	"	9 52	11 20	6731	6159	61	19	- 2	63	8862	19243	"
"	4564	5700	"	10 09	11 37	6222	5693	59	18	- 2	64	8394	18775	"
"	4565	5702	"	10 28	11 56	6498	5946	58	18	- 2	66	8645	19026	"
"	4566	5705	"	11 05	12 33	6586	6026	57	18	1	70	8724	19105	"
"	4567	5708	"	12 20	13 48	6475	5925	34	10	3	77	8610	18991	"
"	4568.1	5710	"	12 35	14 03	7584	6939	80	25	2	78	9637	20018	"
"	4568.2	"	"	12 43		4005	3665	"	"	2				"
"	4569	6767	"	12 59	14 19	4325	3957	50	15	2	80	9917	20298	"
"	4570	6769	"	13 13	14 33	4380	4008	64	20	2	81	9972	20353	"
"	4571	6771	"	13 28	14 48	4670	4273	71	22	2	82	10238	20619	"

Table IX. (Continued)

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$5.56 \times \Sigma \delta T$ Drift	$\Sigma \delta g$	$g$ 980.	Field Note No.
3	4572	6773	IX 25	14 34 <sup>h</sup> 15 54 <sup>m</sup>	15 54	4992	4568	65	20	- 2	88	10521	20902	83
"	4573	6775	"	14 50	16 10	4805	4397	53	16	- 2	90	10344	20725	"
3-2	4574	P.B.*	"	16 05	17 25	4861	4448	27	8	- 5	97	10377	20758	"
3	4575.1	"	"	18 41	20 01	3677	3364	--	--	-10	111	9266	19647	"
"	4575.2	"	"	18 45		7866	7197	--	--	-10				"
"	4576.1	"	"	20 28	21 44	3395	3106	--	--	- 8	121	5167	15548	"
"	4576.2	"	"	20 34	22 37	7776	7115	--	--	- 3	127	1070	11451	"
"	4577	5424	"	21 37	22 47	3280	3001	54	17	13	138	- 105	10276	84
"	Sendai 4578	"	"	23 37	24 47	2015	1844	--	--	- 5				"
"	" 4579	"	IX 26	10 27		2100	1922	--	--					"
"	4580	Sendai M.O.**	"	10 54	25 14	3382	3095	27	8	- 2	140	1077	11458	"
"	4581	"***	"	11 17	25 37	3384	3096	"	"	- 2	142	1076	11457	"
"	4582.1	" M. 1	"	11 35	25 55	2200	2013	50	15	0	144	0	10381	"

\* Prefecture Boundary.

\*\* Meteorological Observatory Seismometer Room, on the Surface of the Concrete Block for Seismometer Installation.

\*\*\* Meteorological Observatory, on the Block Formerly Used for the Silver Disk Pyrheliometer Observation.

Route 34<sub>2</sub> B.M.J. 2—B.M. 1—B.M.J. 2.

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$5.93 \times \Sigma \delta T$ Drift	$\Sigma \delta g$	$g$ 980.	Field Note No.
3	4540	J. 2	IX 24	9 08 <sup>h</sup> 9 41 <sup>m</sup>	0 00	5133	4697	64	20	- 1	0	0	17938	83
"	4541	Ishinomaki W.S.*	"	10 05	33	3953	3617	27	8	0	4	-1095	16843	"
"	4542	5629	"	10 05	57	5563	5090	74	23	0	6	391	18329	"
"	4543	5631	"	10 22	1 14	6157	5634	53	16	0	7	927	18865	"
"	4544	5635	"	11 00	1 52	5860	5362	53	16	3	11	654	18592	"

\* Weather Station Seismometer Room, on the Surface of the Concrete Block for Seismometer Installation.



"	4545	5638	"	11 39	2 31	6460	5911	61	19	5	15	1204	19142	"
"	4546	5642	"	14 53	5 45	6457	5908	51	16	2	34	1172	19110	"
"	4547	5644	"	15 08	6 00	6617	6055	-38	-12	-2	36	1289	19227	"
"	4548	5646	"	15 25	6 17	6032	5519	53	16	-2	37	780	18718	"
"	4549	1	"	15 56	6 48	6318	5781	61	19	-6	40	1038	18976	"
"	4550	2	J.	20 24	11 16	5213	4770	62	19	-6	67	0	17938	"

Route 34<sub>3</sub> B.M. M. 1—B.M. 5424—B.M. 5441—B.M. M. 1.

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	0.9150		0.3086		E.T.	$\Sigma \delta T$ Drift	Adjustment	$\Sigma \delta g$	$g$	Field Note No.
						SD	$\times$ SD	$h$	$\times h$						
3	4504	M. 1	IX 22	15 33	0 00	3296	3016	49	15	-10	0	0	10381	82	
"	4505	5400	"	16 10	37	3088	2826	26	8	-10	4	2	-203	"	
"	4506	5402	"	16 22	49	4615	4223	63	19	-10	5	-9	1215	"	
"	4507	5404	"	16 40	1 07	4136	3784	47	15	-11	7	-6	766	"	
"	4508	5407	"	16 54	1 21	4769	4364	58	18	-11	9	-10	1351	"	
"	4509	5410	"	17 20	1 47	4964	4542	64	20	-11	11	-12	1531	"	
"	4510	5412	"	17 39	2 06	4420	4044	52	16	-10	13	-8	1024	"	
"	4511	5415	"	17 54	2 21	4338	3969	57	18	-10	15	-7	948	"	
"	4512	5418	"	18 16	2 43	3550	3248	63	19	-10	17	-2	221	"	
"	4513	5420	"	18 31	2 58	4250	3889	69	21	-6	19	-7	871	"	
"	4514	5421	"	18 40	3 07	4758	4354	51	16	-6	20	-10	1333	"	
"	4515	5424	"	19 04	3 31	4485	4104	61	19	-6	22	-8	1082	"	
"	4516	5426	"	19 25	3 52	4867	4453	55	17	-6	25	-11	1429	"	
"	4517	5428	"	19 35	4 02	5190	4749	50	15	0	25	-13	1731	"	
"	4518	5430	"	19 45	4 12	5270	4822	42	13	0	27	-14	1801	"	
"	4519	"	IX 23	8 51		5380	4923	41	13	1	28	-25	3323	"	
"	4520.1	5432	"	9 11	4 32	7042	6443	15	5	1	1		13704	"	
"	4520.2	"	"	9 15		4004	3664	"	"	1	30	-31	4082	"	
"	4521	5435	"	9 30	4 47	4811	4402	55	17	6	32	-30	14463	83	
"	4522	5437	"	9 44	5 01	4712	4311	34	10	6			3981	"	

Table IX. (Continued)

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	E.T.	$6.32 \times \Sigma \delta T$ Drift	Adjustment	$\Sigma \delta g$	$g$ 980.	Field Note No.
3	4523	5439	IX 23	<sup>h</sup> 9 55	<sup>m</sup> 5 12	3770	3450	3	1	6	33	24	3104	13485	83
2	4524.1	5441	"	10 07	5 24	5504	5036	68	21	6	34	36	4721	15102	"
"	4524.2	"	"	10 12	7 85	7123		"	"	6					"
3	4525	5430	"	10 50	6 02	4619	4226	41	13	9	38	14	1793	12174	"
"	4526	M. 1	"	12 26	7 38	2684	2456	48	15	8	48	0	0	10381	"

Route 34 B.M. M. 1—B.M. 3787—B.M. M. 1.

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	E.T.	$5.33 \times \Sigma \delta T$ Drift	Adjustment	$\Sigma \delta g$	$g$ 980.	Field Note No.
3	4491	M. 1	IX 22	<sup>h</sup> 9 26	<sup>m</sup> 0 00	3183	2912	48	15	6	0	0	0	10381	82
"	4492	3769	"	9 48	22	2231	2041	45	14	10	2	3	867	09514	"
"	4493	3771	"	10 01	35	1395	1276	73	23	10	3	5	1622	08759	"
"	4494.1	"	"	10 20	54	0219	0200	—	—	10	5	9	2719	07652	"
"	4494.2	"	"	10 22		7813	7149	—	—	10					"
"	4495	3773	"	10 26	58	7580	6936	54	17	10	5	10	2914	07467	"
"	4496	3775	"	10 40	1 12	5022	4595	35	11	11	6	17	5254	05127	"
"	4497	3778	"	11 00	1 32	4275	3912	39	12	11	8	20	5935	04446	"
"	4498	3780	"	11 12	1 44	3608	3301	35	11	11	9	22	6546	03835	"
"	4499.1	"	"	11 35	2 07	1921	1758	—	—	9	11	27	8099	02282	"
"	4499.2	"	"	11 37		7686	7033	—	—	9					"
"	4500	3784	"	11 49	2 19	7023	6426	71	22	9	12	29	8683	01698	"
5	4501	3787	"	12 13	2 43	2691	2462	40	12	9	14	42	12646	97735	"
3	4502.1	"	"	14 25	4 55	7715	7059	—	—	0	26	27	8097	980.	"
"	4502.2	"	"	14 26	0132	0121		—	—	0				02284	"

"	4503.1	3773	"	15 08	5 37	5812	5318	52	16	- 6	30	-10	- 2911	07470	"
"	4503.2	"	"	15 10	0096	0088	"	49	"	- 6	"	0	"	"	"
"	4504	M. 1	"	15 33	6 00	3296	3016	49	49	-10	32	0	0	10381	"

Route 34<sub>5</sub> B.M. M. 1—B.M.J. 2169—B.M. 5572—B.M.J. 2169—B.M. M. 1.

Pref.	No.	B.M.	Date	Time	$\Sigma \delta T$	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	$E.T.$	$9.41 \times \Sigma \delta T$ Drift	Adjustment	$\Sigma \delta g$	$g$ 980.	Field Note No.
3	4466.2	M. 1	IX 21	9 52	0 00	6348	5808	50	15	12	0	0	0	10381	82
"	4467	2178	"	10 10	18	6874	6290	79	24	12	3	235	253	10634	"
"	4468.1	2176	"	10 38	46	7582	6938	81	25	11	8	544	587	10968	"
"	4468.2	"	"	10 42	"	5757	5268	"	"	11	"	"	"	"	"
"	4469	2173	"	11 04	1 08	6040	5527	73	23	11	10	666	720	11101	"
"	4470	2171	"	11 20	1 24	5738	5250	58	18	11	13	529	572	10953	"
"	4471	J. 2169	"	11 48	1 52	4594	4204	66	20	8	18	24	25	10406	"
"	4481	"	"	17 34	3094	2831	"	"	"	- 8	"	"	"	"	"
"	4482	5561	"	17 51	2 09	1721	1575	54	17	- 8	21	-583	-630	09751	"
"	4483	5563	"	18 10	2 28	1980	1812	76	23	- 8	24	-468	-505	09876	"
"	4484	5565	"	18 25	2 43	1061	0971	60	19	- 8	25	-874	-945	09436	"
"	4485	5567	"	18 38	2 56	1507	1379	39	12	- 4	27	-680	-736	09645	"
"	4486	5569	"	18 50	3 08	2391	2188	61	19	- 4	29	-289	-313	10068	"
"	4487	5571	"	19 03	3 21	2933	2684	41	13	- 4	32	- 55	- 60	10321	"
6	4488	5572	"	19 11	3 29	2750	2516	44	14	- 4	33	-136	-147	10234	"
3	4489	J. 2169	"	20 05	4 23	3118	2853	66	20	0	41	27	29	10410	"
"	4490	M. 1	"	20 48	5 06	3065	2804	48	15	5	48	0	0	10381	"

Route 346 B.M.J. 2169—B.M. 2147—B.M.J. 2169.

Pref.	No.	B.M.	Date 1953	Time h <sup>m</sup>	$\sum \delta T$ h <sup>m</sup>	$SD$	$0.9150 \times SD$	$h$ (cm)	$0.3086 \times h$	E.T.	$5.36 \times \sum \delta T$ Drift	Adjust- ment	$\sum \delta g$	$g$ 980.	Field Note No.
3	4471	J. 2169	IX 21	11 48	0 00	4594	4204	66	20	8	0	0	0	10406	82
"	4472	2167	"	12 00	12	4308	3942	61	19	8	1	5	-259	10147	"
"	4473	2164	"	12 23	35	2585	2365	56	17	8	3	-32	-1813	08593	"
"	4474.1	2161	"	13 35	1 47	1618	1480	65	20	-3	10	-48	-2697	07709	"
"	4474.2	"	"	13 39		6350	5810	"	"	-3					"
"	4475	2158	"	14 10	2 18	6400	5856	44	14	3	12	47	-2660	07746	"
"	4476	2154	"	14 37	2 45	3370	3084	69	21	-7	15	96	-5383	05023	"
"	4477	2152	"	14 54	3 02	3964	3627	56	17	-7	16	87	-4854	05552	"
"	4478.1	2149	"	15 11	3 19	0837	0766	47	15	-7	18	-137	-7669	02737	"
"	4478.2	"	"	15 14		1709	1564	"	"	-7					"
6	4479	2147	"	15 38	3 43	0768	0703	29	9	-10	20	-152	-8526	01880	"
3	4480.1	2161	"	16 31	4 36	7249	6633	65	20	-10	25	-48	-2694	07712	"
"	4480.2	"	"	16 34		0094	0086	"	"	-10					"
"	4481	J. 2169	"	17 34	5 36	3094	2831	66	20	-8	30	0	0	10406	"



(1) Aomori Prefecture

Table X. Synoptic Results for Aomori Prefecture (I)

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	$g$ 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula				
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)		
		40°	139°													
6069	2434	26.2	56.6	13.55	IX 20	30118	3054	3038	100.6	99.0	99.0	2193	86.1	84.5		
6071	2433	27.9	56.8	3.78	"	30067	3018	3014	94.4	94.0	94.0	2219	79.9	79.5		
6073	2432	30.1	57.2	6.32	"	28680	2888	2880	2106	77.4	77.4	2251	63.7	62.9		
6075	2431	32.2	57.0	7.80	"	29490	2973	2964	2138	83.5	82.6	2283	69.0	68.1		
6077	2430	34.0	56.2	13.49	"	30065	3048	3033	2164	88.4	86.9	2309	73.9	72.4		
6079	2429	35.6	55.0	86.31	"	30092	3276	3179	2188	108.8	99.1	2333	94.3	84.6		
6081	2428	37.1	55.1	81.06	"	30264	3277	3186	2211	106.6	97.5	2355	92.2	83.1		
6083	2427	38.8	55.0	4.77	"	31796	3194	3189	2236	95.8	95.3	2381	81.3	80.8		
6085	2426	40.3	57.6	9.88	"	31692	3200	3189	2258	94.2	93.1	2403	79.7	78.6		
6087	2425	41.8	59.0	47.76	"	31497	3297	3244	2281	101.6	96.3	2425	87.2	81.9		
6089	2424	43.9	59.9	12.71	"	32410	3280	3266	2312	96.8	95.4	2456	82.4	81.0		
6091	2423	45.0	01.5	3.33	"	32047	3215	3211	2328	88.7	88.3	2473	74.2	73.8		
6093	2422	45.8	04.3	8.17	"	31825	3208	3199	2340	86.8	85.9	2485	72.3	71.4		
6095	2421	44.4	06.5	4.39	"	29650	2979	2974	2319	66.0	65.5	2464	51.5	51.0		
6098	2420	45.8	10.2	14.90	"	30908	3137	3120	2340	79.7	78.0	2485	65.2	63.5		
6100	2419	46.8	12.0	2.93	"	31597	3169	3165	2355	81.4	81.4	2499	67.0	66.6		
6101	2418	46.4	13.4	2.26	"	31161	3123	3121	2349	77.4	77.2	2494	62.9	62.7		
6102	2416	47.0	14.5	6.47	IX 19	30455	3066	3058	2358	70.8	70.0	2502	56.4	55.6		
6104	2415	47.2	17.0	30.52	"	29875	3082	3048	2361	72.1	68.7	2505	57.7	54.3		
6106	2414	46.7	20.0	12.17	"	30417	3079	3066	2354	72.5	71.2	2498	58.1	56.8		
6108	2413	47.3	22.0	6.20	"	30764	3096	3089	2363	73.3	72.6	2507	58.9	58.2		
6110	2412	48.4	24.3	7.00	"	31437	3165	3158	2379	78.6	77.9	2523	64.2	63.5		
6112	2411	48.3	26.6	9.30	"	32346	3263	3253	2378	88.5	87.5	2522	74.1	73.1		
6115	2402	46.5	29.8	11.19	"	31167	3151	3139	2351	80.0	78.8	2495	65.6	64.4		
6117	2401	45.9	32.0	35.61	"	29189	3029	2989	2342	68.7	64.7	2486	54.3	50.3		

Table X. (Continued)

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula		
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta \theta_0$ (mgal.)	$\Delta \theta_0''$ (mgal.)
J.	2400	40° 45.5	140° 35.4	63.43	IX 19	27003	2896	2825	2336	56.0	48.9	2480	41.6	34.5
	5960	46.6	37.0	55.40	"	28100	2981	2919	2352	62.9	56.7	2496	48.5	42.3
	5962	48.5	38.8	24.41	"	29653	3041	3013	2381	66.0	63.2	2525	51.6	48.8
	5964	49.4	41.2	22.23	"	29754	3044	3019	2394	65.0	62.5	2538	50.6	48.1
	5966	49.4	43.5	2.86	"	30782	3087	3084	2394	69.3	69.0	2538	54.9	54.6
6050	2456	49.5	46.8	2.97	IX 21	33039	3313	3310	2395	91.8	91.5	2540	77.3	77.0
6047	2457	51.5	50.2	18.63	"	33836	3441	3420	2425	101.6	99.5	2569	87.2	85.1
6046	2458	52.2	51.0	2.94	"	34809	3490	3487	2436	105.4	105.1	2580	91.0	90.7
6043	2460	54.9	52.8	30.48	IX 22	35404	3635	3600	2476	115.9	112.4	2620	101.5	98.0
6041	2461	54.9	55.7	10.29	"	36261	3658	3646	2476	118.2	117.0	2620	103.8	102.6
6039	2462	55.5	58.1	6.35	"	35499	3570	3562	2485	108.5	107.7	2629	94.1	93.3
6037	2463	55.5	00.8	8.05	"	34057	3431	3422	2485	94.6	93.7	2629	80.2	79.3
6035	2464	54.5	03.3	19.11	"	33600	3419	3398	2470	94.9	92.8	2614	80.5	78.4
6033	2465	53.2	05.1	15.86	"	33825	3431	3414	2451	98.0	96.3	2595	83.6	81.9
J. 6031	2466	52.0	07.5	10.20	"	32669	3298	3287	2433	86.5	85.4	2577	72.1	71.0
6029	2467	50.1	07.8	34.94	"	31738	3282	3243	2404	87.8	83.9	2549	73.3	69.4
6026	2468	47.4	09.1	70.42	"	30421	3259	3181	2364	89.5	81.7	2508	75.1	67.3
6023	2469	44.2	09.8	29.54	"	30472	3138	3105	2316	82.2	78.9	2461	67.7	64.4
6020	2470	41.2	09.8	35.04	"	29331	3041	3002	2272	76.9	73.0	2416	62.5	58.6
6017	2473	38.6	12.1	62.14	IX 23	28781	3070	3000	2233	83.7	76.7	2378	69.2	62.2
6016	2471	37.5	12.5	72.09	IX 22	28518	3074	2994	2217	85.7	77.7	2361	71.3	63.3
6013	2474	34.7	14.5	33.36	IX 23	28818	2985	2947	2175	81.0	77.2	2320	66.5	62.7
6011	2475	33.7	16.6	85.08	"	27795	3042	2947	2160	88.2	78.7	2305	73.7	64.2
6008	2476	31.1	18.3	77.20	"	27487	2987	2901	2121	86.6	78.0	2266	72.1	63.5
6005	2477	28.6	18.6	53.95	"	28569	3023	2963	2084	93.9	87.9	2229	79.4	73.4
6003	2478	27.3	16.5	69.08	"	28306	3044	2967	2065	97.9	90.2	2210	83.4	75.7
6001	2479	25.7	16.8	141.43	"	27256	3162	3004	2041	112.1	96.3	2186	97.6	81.8
5999	2480	23.9	16.4	33.25	"	30256	3128	3091	2014	111.4	107.7	2159	96.9	93.2
5997	2481	22.3	15.0	47.13	"	28067	2952	2899	1990	96.2	90.9	2136	81.6	76.3

Synoptic Results for Aomori Prefecture (II).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula		
									$\gamma_0$ 980.	$\Delta g_0'$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0'$ (mgal.)
6178	2404	40° 50.3	140° 27.7	8.55	IX 19	32185	3245	3235	2407	83.8	82.8	2552	69.3	68.3
6176	2405	52.2	27.7	7.84	"	32529	3277	3268	2436	84.1	83.2	2580	69.7	68.8
6174	2406	54.1	27.2	10.02	"	33066	3338	3326	2464	87.4	86.2	2608	71.8	71.8
6172	2407	55.9	27.0	16.08	"	33463	3396	3378	2491	90.5	88.7	2635	76.1	74.3
6170	2408	57.9	25.4	13.68	"	33384	3381	3365	2521	86.0	84.4	2665	71.6	70.0
6168	2409	59.7	25.8	4.56	"	33648	3379	3374	2547	83.2	82.7	2691	68.8	68.3
6166	2410	41° 01.7	25.4	4.03	"	34691	3482	3477	2577	90.5	90.0	2721	76.1	75.6

Synoptic Results for Aomori Prefecture (III).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula		
									$\gamma_0$ 980.	$\Delta g_0'$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0'$ (mgal.)
5957	2440	43.2	35.2	27.45	IX 21	26803	2765	2734	2301	45.4	43.3	2446	31.9	28.8
5955	2441	41.9	34.3	22.13	"	26694	2738	2713	2282	45.6	43.1	2427	31.1	28.6
5953	2442	40.4	32.5	19.58	"	26814	2742	2720	2260	48.2	46.0	2404	33.8	31.6
5951	2443	39.3	30.1	21.15	"	27593	2825	2801	2243	58.2	55.8	2388	43.7	41.3
5949	2444	37.6	29.7	23.48	"	27297	2802	2776	2218	58.4	55.8	2363	43.9	41.3
5947	2445	35.7	28.8	39.65	"	27406	2863	2819	2190	67.3	62.9	2334	52.9	48.5
5945	2446	34.2	31.5	41.45	"	26247	2753	2705	2167	58.6	53.9	2312	44.1	39.4
5943	2447	32.7	33.3	52.40	"	26467	2808	2750	2145	66.3	60.5	2290	51.8	46.0
5941	2448	31.2	34.5	76.27	"	27400	2975	2890	2123	85.2	76.7	2268	70.7	62.2
5939	2449	30.3	36.9	106.63	"	24919	2821	2702	2109	71.2	59.3	2254	56.7	44.8
5937	2450	28.3	37.3	143.56	"	23896	2833	2672	2080	75.3	59.2	2225	60.8	44.7
5935	2451	26.2	38.3	181.55	"	23446	2905	2702	2048	85.7	65.4	2193	71.2	50.9



Synoptic Results for Aomori Prefecture (IV).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula												
									$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.										
Aomori	W.S.*	40°	140°	2.70	IX 26	29768	2985	2982	2418	56.7	56.4	2562	42.3	42.0										
	6120														51.0	42.0	2418	56.4	2562	42.3	42.0			
	6121														50.0	43.6	30637	3069	3067	2403	66.4	2547	52.2	52.0
	6123														50.6	42.6	30009	3007	3005	2412	59.5	2556	45.1	44.9
	6125														52.5	41.0	29532	2957	2956	2440	51.7	2584	37.3	37.2
															54.5	40.5	29713	2975	2974	2470	50.5	2614	36.1	36.0
	6127														56.6	40.6	30227	3028	3026	2501	52.7	2645	38.3	38.1
	6129														58.7	39.5	30880	3104	3098	2532	57.2	2677	42.7	42.1
	6131	41°	39.1	3.99	"	31314	3144	3139	2565	57.9	57.4	2709	43.5	43.0										
	6133														00.9	38.9	31930	3213	3206	2594	61.9	2738	47.5	46.8
	6135														02.8	38.3	33334	3338	3337	2627	71.1	2770	56.8	56.7
															05.0									
	6137	07.1	38.2	4.84	"	33546	3370	3364	2658	71.2	70.6	2802	56.8	56.2										
	6139														09.1	38.1	34158	3424	3421	2688	73.6	2831	59.3	59.0
	6141														11.3	38.1	35126	3524	3520	2721	80.3	2864	65.6	65.6
	6144														13.2	35.0	37318	3741	3738	2749	99.2	2893	84.8	84.5
6146	13.0	32.8	36377	3647	3644	2746	90.1	2890	75.7	75.4														
6148	12.0	31.2	34617	3543	3513	2731	81.2	2875	66.8	63.8														
6151	09.9	30.5	34345	3473	3459	2700	77.3	2843	63.0	61.6														

\* Weather Station Seismometer Room, on the Surface of the Concrete Block for Seismometer Installation.

Synoptic Results for Aomori Prefecture (V).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula								
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)						
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)						
		$40^\circ$	$141^\circ$																	
6261	2498	53.0	09.8	12.64	IX 24	32283	3267	3253	2448	81.9	80.5	2592	67.5	65.1						
6259	2499	54.9	11.7	15.10	"	33275	3374	3357	2476	89.8	88.1	2620	75.4	73.7						
6255	2500	58.7	13.8	4.35	"	35715	3585	3580	2532	105.3	104.8	2677	90.8	90.3						
		$41^\circ$																		
6253	2501	00.7	15.0	16.31	"	36526	3703	3685	2562	114.1	112.3	2706	99.7	97.9						
6251	2502	02.8	15.4	14.53	"	36260	3671	3655	2594	107.7	106.1	2738	93.3	91.7						
6246	2503	07.8	16.6	13.39	"	36805	3722	3707	2669	105.3	103.8	2812	91.0	89.5						
6243	2504	10.9	17.2	27.91	"	37016	3788	3757	2715	107.3	104.2	2858	93.0	89.9						
6238	2505	15.6	13.7	5.21	"	36657	3682	3676	2785	89.7	89.1	2928	75.4	74.8						
6236	2506	17.4	13.0	2.28	"	37165	3724	3721	2812	91.2	90.9	2955	76.9	76.6						
6266	2507	21.2	12.5	37.25	"	37743	3889	3848	2869	102.0	97.9	3012	87.7	83.6						
6268	2508	23.0	12.0	6.62	"	38652	3886	3878	2896	99.0	98.2	3039	84.7	83.9						
6270	2509	24.2	10.0	2.12	"	39506	3957	3955	2914	104.3	104.1	3057	90.0	89.8						
6277	2510	28.8	04.1	7.11	"	39972	4019	4011	2983	103.6	102.8	3125	89.4	88.6						
			$140^\circ$																	
6281	2511	29.7	58.8	3.35	"	39849	3995	3992	2996	99.9	99.6	3139	85.6	85.3						
6282	2518	30.5	58.0	2.87	IX 25	40355	4044	4041	3008	103.6	103.3	3151	89.3	89.0						
6285	2517	31.2	54.6	11.03	"	40459	4080	4068	3019	106.1	104.9	3161	91.9	90.7						
6286	2515	30.2	54.9	3.81	IX 24	40182	4030	4026	3004	102.6	102.2	3146	88.4	88.0						
"	2512	"	"	"	"	40184	4030	4026	"	102.6	102.2	"	88.4	88.0						
6288	2513	28.4	53.9	7.96	"	40352	4060	4051	2977	108.3	107.4	3119	94.1	93.2						
6290	2514	26.6	52.6	14.47	"	39838	4029	4012	2950	107.9	106.2	3092	93.7	93.0						

Synoptic Results for Aomori Prefecture (VI).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	$g$ 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula			
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	
		41°	141°		1952										
6318	2519	15.5	09.1	2.39	IX 25	36942	3702	3699	2784	91.8	91.5	2927	77.5	77.2	
6314	2520	12.6	06.0	2.51	"	35863	3594	3591	2740	85.4	85.1	2884	71.0	70.7	
6312	2521	11.2	03.8	4.46	"	36792	3693	3688	2720	97.3	96.8	2863	83.0	82.5	

Synoptic Results for Aomori Prefecture (VII).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	$g$ 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula		
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)
		40°	141°		1952									
6966	2483	29.6	20.7	35.14	IX 23	29863	3095	3055	2099	99.6	95.6	2244	85.1	81.1
6964	2484	30.7	22.7	21.63	"	30665	3133	3109	2115	101.8	99.4	2260	87.3	84.9
6962	2485	30.8	25.2	11.26	"	32666	3301	3289	2117	118.4	117.2	2262	103.9	102.7
6181	2487	31.6	28.5	3.86	"	35337	3546	3541	2129	141.7	141.2	2274	127.2	126.7
6185	2488	35.0	27.6	6.05	"	34012	3420	3413	2179	124.1	123.4	2324	109.6	108.9

Synoptic Results for Aomori Prefecture (VIII).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	$g$ 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula		
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)
		40°	141°		1952									
6958	2489	29.9	30.4	15.42	IX 23	36648	3712	3695	2103	160.9	159.2	2248	146.4	144.7
6956	2490	29.1	32.8	71.40	"	35936	3814	3734	2091	172.3	164.3	2236	157.8	149.8
6954	2491	28.2	35.3	115.42	"	35328	3889	3760	2078	181.1	168.2	2223	166.6	153.7
6951	2492	26.6	38.8	99.79	"	34997	3808	3696	2054	175.4	164.2	2199	160.9	149.7
6950	2493	26.7	40.1	48.18	"	36077	3756	3703	2056	170.0	164.7	2201	155.5	150.2

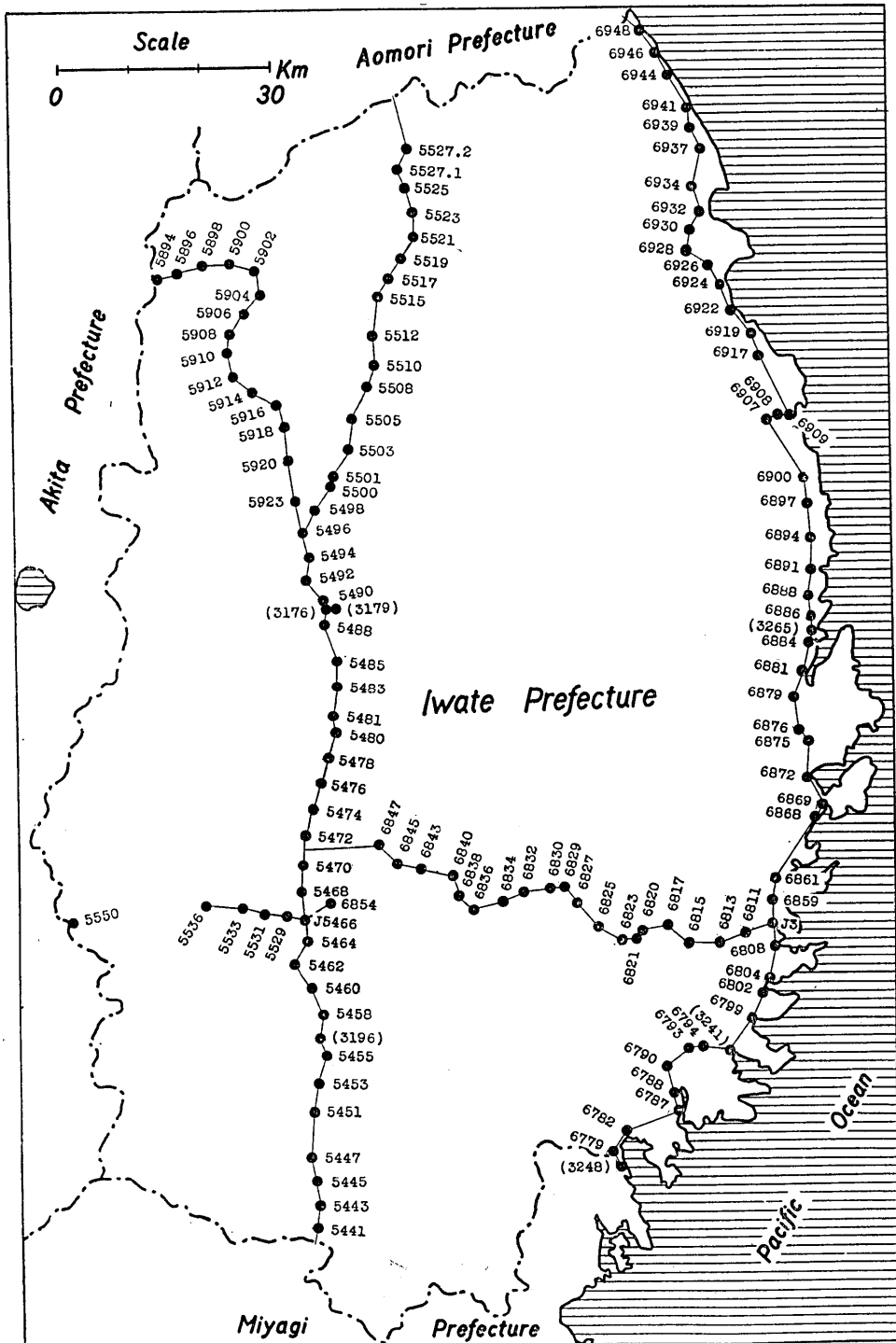


Fig. 11. Gravity Stations in Iwate Prefecture.

(2) Iwate Prefecture.

Table XI. Synoptic Results for Iwate Prefecture (I).

B.M.	No.	$\phi$	$\lambda$	H (m)	Date	g 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula			
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	
		40°	140°		1952										
5894	3152	06.8	53.0	252.65	XII 9	18269	2607	2324	1760	84.7	56.4	1906	70.1	41.8	
5896	3151	07.5	55.3	281.25	"	18335	2701	2387	1770	93.1	61.7	1916	78.5	47.1	
5898	3150	08.0	57.5	308.94	"	18288	2782	2437	1778	100.4	65.9	1923	85.9	51.4	
5900	3149	08.1	00.2	430.35	"	15491	2877	2396	1779	109.8	61.7	1925	95.2	47.1	
5902	3148	07.5	02.5	318.73	"	17530	2737	2380	1770	96.7	61.0	1916	82.1	46.4	
5904	3147	05.6	03.1	300.25	"	18349	2762	2426	1742	102.0	68.4	1888	87.4	53.8	
5906	3146	04.5	01.5	335.72	"	17502	2786	2411	1726	106.0	68.5	1872	91.4	53.9	
5908	3145	02.6	00.3	385.72	"	16250	2815	2384	1698	111.7	68.6	1843	97.2	54.1	
5910	3144	00.9	140°	496.71	"	13730	2906	2350	1672	123.4	67.8	1818	108.8	53.2	
5912	3143	59.4	141°	398.94	"	15934	2825	2378	1650	117.5	72.8	1796	102.9	58.2	
5914	3142	58.1	02.7	292.98	"	17307	2635	2307	1631	100.4	67.6	1777	85.8	53.0	
5916	3141	57.0	05.1	263.46	"	17703	2583	2289	1614	96.9	67.5	1761	82.2	52.8	
5918	3140	55.2	06.0	267.67	"	17563	2582	2283	1588	99.4	69.5	1734	84.8	54.9	
5920	3139	53.2	05.9	256.91	"	17730	2566	2278	1558	100.8	72.0	1704	86.2	57.4	
5923	3138	50.0	07.0	271.44	"	17117	2549	2246	1511	103.8	73.5	1657	89.2	58.9	

Synoptic Results for Iwate Prefecture (II).

B.M.	No.	$\phi$	$\lambda$	H (m)	Date	g 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula		
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)
5527 <sup>2</sup>	3159	16.5	141°	106.86	XII 10	27614	3091	2972	1904	118.7	106.8	2049	104.2	92.3
5527 <sup>1</sup>	3160	15.5	17.8	98.90	"	27769	3082	2971	1889	119.3	108.2	2035	104.7	93.6
5525	3161	13.6	17.5	129.96	"	28351	3236	3091	1861	137.5	123.0	2006	123.0	108.5
5523	3162	11.8	18.3	147.95	"	27660	3223	3057	1834	138.9	122.3	1980	124.3	107.7
5521	3163	09.6	18.7	187.05	"	25946	3172	2963	1802	137.0	116.1	1947	122.5	101.6

Table XI. (Continued)

B.M.	No.	$\phi$	$\lambda$	H (m)	Date	g 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula				
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)		
		$40^\circ$	$141''$		1952											
5519	3164	08.3	17.8	252.95	XII 10	24298	3210	2927	1782	142.8	114.5	128.2	1928	128.2	99.9	
5517	3165	07.1	15.8	330.87	"	21872	3208	2838	1764	144.4	107.4	129.8	1910	129.8	92.8	
5515	3166	05.2	15.3	413.91	"	19825	3260	2797	1736	152.4	106.1	137.8	1882	137.8	91.5	
5512	3167	02.7	14.3	373.13	"	19727	3124	2707	1699	142.5	100.8	145.5	1845	145.5	86.2	
5510	3168	00.5	14.5	301.97	"	20781	3010	2672	1666	134.4	100.6	119.8	1812	119.8	86.0	
		$39^\circ$														
5508	3169	58.6	13.9	262.84	"	20788	2890	2596	1638	125.2	95.8	110.6	1784	110.6	81.2	
5505	3170	55.8	12.3	224.10	"	20958	2787	2537	1597	119.0	94.0	104.4	1743	104.4	79.4	
5503	3171	53.6	12.0	201.97	"	20733	2697	2471	1564	113.3	90.7	98.7	1710	98.7	76.1	
5501	3172	51.8	10.9	191.44	"	20326	2623	2409	1537	108.6	87.2	93.9	1684	93.9	72.5	
5500	3173	50.8	10.4	196.63	"	19881	2595	2375	1522	107.3	85.3	92.6	1669	92.6	70.6	
5498	3174	49.3	08.8	207.64	"	19072	2548	2316	1500	104.8	81.6	90.1	1647	90.1	66.9	
J. 5496	3175	47.4	07.5	241.61	"	18124	2558	2288	1472	108.6	81.6	93.9	1619	93.9	66.9	
	3137	"	"	"	XII 9	18159	2562	2291	"	109.0	81.9	94.3	"	94.3	67.2	
5494	3136	45.3	08.2	180.56	"	19479	2505	2303	1441	106.4	86.2	91.8	1587	91.8	71.6	
5492	3135	43.3	07.6	143.61	"	20082	2451	2291	1411	104.0	88.0	89.3	1558	89.3	73.3	
5490	3178	42.0	09.4	125.81	XII 11	20756	2464	2323	1392	107.2	93.1	92.5	1539	92.5	78.4	
W.S.*	3179	41.5	10.1	152.10	"	20224	2492	2322	1385	110.7	93.7	96.1	1531	96.1	79.1	
5488	3180	40.3	09.5	118.63	"	20955	2462	2329	1367	109.5	96.2	94.8	1514	94.8	81.5	
5485	3181	37.2	10.7	105.05	"	22406	2565	2447	1321	124.4	112.6	109.7	1468	109.7	97.9	
5483	3182	35.1	10.4	101.81	"	21061	2420	2306	1290	113.0	101.6	98.3	1437	98.3	86.9	
5481	3183	33.1	10.4	100.10	"	21426	2452	2340	1260	119.2	108.0	104.5	1407	104.5	93.3	
5480	3184	32.0	10.2	95.79	"	21332	2429	2322	1244	118.5	107.8	103.8	1391	103.8	93.1	
5478	3185	29.8	09.5	87.91	"	20458	2317	2219	1211	110.6	100.8	95.8	1359	95.8	86.0	
5476	3186	27.6	08.7	87.72	"	19503	2221	2123	1179	104.2	94.4	89.5	1326	89.5	79.7	
5474	3187	25.5	08.0	91.67	"	18771	2160	2057	1148	101.2	90.9	86.5	1295	86.5	76.2	

\* Weather Station Seismometer Room, on the Surface of the Concrete Block for Seismometer Installation.

5472	3188	23.6	07.3	71.25	"	18212	2041	1961	1120	92.1	84.1	1267	77.4	69.4
5470	3189	21.6	07.1	85.66	"	17766	2041	1945	1090	95.1	85.5	1238	80.3	70.7
5468	3190	19.4	07.0	87.02	"	17688	2037	1940	1058	97.9	88.2	1205	83.2	73.5
J. 5466	3191	17.3	07.4	63.13	"	18331	2028	1957	1027	100.1	93.0	1174	85.4	78.3
5464	3192	15.3	07.1	55.98	"	17282	1901	1838	0997	90.4	84.1	1145	75.6	69.3
5462	3193	13.3	06.0	74.68	"	15801	1811	1727	0968	84.3	75.9	1115	69.6	61.2
5460	3194	11.4	07.4	53.99	"	16401	1807	1746	0940	86.7	80.6	1087	72.0	65.9
5458	3195	09.7	08.9	51.52	"	16691	1828	1770	0915	91.3	85.5	1062	76.6	70.8
Mizusawa I.L.O.*	3196	07.6	08.1	60.74	"	16039	1791	1723	0884	90.7	83.9	1031	76.0	69.2
5455	3197	06.8	02.1	42.75	"	16510	1783	1735	0872	91.1	86.3	1020	76.3	71.5
5453	3198	04.8	08.4	40.90	"	15968	1723	1677	0842	88.1	83.5	0990	73.3	68.7
5451	3199	02.8	07.6	31.71	"	17410	1639	1803	0813	102.6	99.0	0961	87.8	84.2
5447	3200	59.0	07.2	24.39	"	17845	1860	1833	0757	110.3	107.6	0905	95.5	92.8
5445	3201	57.1	08.0	25.96	"	18012	1881	1852	0729	115.2	112.3	0877	100.4	97.5
5443	3202	55.2	08.2	26.92	"	17523	1835	1805	0701	113.4	110.4	0849	98.6	95.6
5441	3203	53.2	07.4	73.79	"	15102	1738	1655	0671	106.7	98.4	0820	91.8	83.5

\* International Latitude Observatory, Underground Room for Tiltmeter Observation.

Synoptic Results for Iwate Prefecture (III).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula		
									$\gamma_0$ 980.	$\Delta\gamma_0$ (mgal.)	$\Delta\gamma_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta\gamma_0$ (mgal.)	$\Delta\gamma_0''$ (mgal.)
6847	3214	39° 22.9	141° 14.2	108.95	XII 12	19628	2299	2177	1109	119.0	106.8	1257	104.2	92.0
6845	3215	21.6	16.3	129.15	"	19727	2371	2227	1090	128.1	113.7	1238	113.3	98.9
6843	3216	21.2	18.8	140.71	"	19867	2421	2263	1084	133.7	117.9	1232	118.9	103.1
6840	3217	20.6	21.7	199.86	"	18568	2474	2250	1076	139.8	117.4	1223	125.1	102.7
6838	3218	18.9	22.4	266.90	"	17052	2529	2230	1050	147.9	118.0	1198	133.1	103.2
6836	3219	17.9	23.9	221.66	"	17911	2475	2227	1036	143.9	119.1	1183	129.2	104.4
6834	3220	18.4	26.2	229.09	"	17963	2503	2247	1043	146.0	120.4	1190	131.3	105.7
6832	3221	19.2	28.5	241.30	"	17772	2522	2252	1055	146.7	119.7	1202	132.0	105.0
6830	3222	19.4	31.2	255.27	"	16989	2487	2201	1058	142.9	114.3	1205	128.2	99.6
6829	3224	19.8	32.5	273.09	XII 13	16555	2498	2193	1064	143.4	112.9	1211	128.7	98.2

Table XI. (Continued)

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula			
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	
		39°	141°												
6827	3225	18.5	34.4	311.52	XII 13	16173	2579	2230	1044	153.5	118.6	1192	138.7	103.8	
6825	3226	16.8	35.7	374.95	"	15500	2707	2288	1019	168.8	126.9	1167	154.0	112.1	
6823	3227	15.7	37.5	427.56	"	14588	2778	2300	1003	177.5	129.7	1151	162.7	114.9	
6821	3229	15.7	40.0	508.46	"	13000	2869	2300	1003	186.6	129.7	1151	171.8	114.9	
6820	3228	16.3	40.9	557.72	"	12131	2934	2310	1012	192.2	129.8	1160	177.4	115.0	
6817	3231	16.6	43.3	254.91	"	18362	2623	2338	1016	160.7	132.2	1164	145.9	117.4	
6815	3232	15.1	44.9	140.57	"	21565	2590	2433	0994	159.6	143.9	1142	144.8	129.1	
6813	3233	15.0	47.5	68.77	"	23598	2572	2495	0992	158.0	150.3	1140	143.2	135.5	
6811	3234	15.6	50.3	22.68	"	25014	2571	2546	1002	156.9	154.4	1149	142.2	139.7	

Synoptic Results for Iwate Prefecture (IV).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula			
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	
		39°	141°												
6854	3211	18.3	09.6	73.34	XII 12	18816	2108	2026	1042	106.6	98.4	1189	91.9	83.7	
5529	3207	17.5	05.0	73.75	"	16816	1909	1827	1030	87.9	79.7	1177	73.2	65.0	
5531	3208	17.8	02.5	88.71	"	15983	1872	1773	1034	83.8	73.9	1182	69.0	59.1	
5533	3209	18.3	59.9	108.51	"	14677	1803	1681	1042	76.1	63.9	1189	61.4	49.2	
5536	3210	18.0	56.3	150.45	"	14041	1868	1700	1037	83.1	66.3	1185	68.3	51.5	
5550	2977	16.3	43.3	296.09	XI 21	09723	1886	1555	1012	87.4	54.3	1160	72.6	39.5	



Synoptic Results for Iwate Prefecture (V).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g 980.	g'' 980.	HELMERT Formula of 1901			International Formula			
								$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	
6948	3293	40° 25.6	141° 42.8	12.04	XII 18	36591	3683	2039	165.7	164.4	164.4	2185	151.1	149.8
6946	3292	23.8	43.4	20.16	"	36482	3710	2013	169.7	167.5	167.5	2158	155.2	153.0
6944	3291	22.2	44.6	27.42	"	36572	3742	1989	175.3	172.2	172.2	2134	160.8	157.7
6941	3290	19.8	46.4	28.68	"	36713	3760	1953	180.7	177.5	177.5	2098	166.2	163.0
6939	3289	18.0	46.7	99.24	"	35639	3870	1926	194.4	183.3	183.3	2072	179.8	168.7
6937	3288	16.2	48.0	150.86	"	35118	3977	1900	207.7	190.9	190.9	2045	193.2	176.4
6934	3287	13.4	47.2	15.24	"	36263	3673	1858	181.5	179.8	179.8	2003	167.0	165.3
6932	3273	11.7	47.3	3.54	XII 17	35715	3582	1833	174.9	174.5	174.5	1978	160.4	160.0
6930	3274	10.0	46.7	25.69	"	34250	3476	1807	169.7	166.9	166.9	1953	155.1	152.3
6928	3275	08.2	46.6	62.66	"	33161	3510	1781	172.9	165.8	165.8	1926	158.4	151.3
6926	3276	07.1	48.8	16.78	"	34219	3474	1764	171.0	169.1	169.1	1910	156.4	154.5
6924	3277	05.5	50.0	8.39	"	34248	3451	1741	171.0	170.0	170.0	1886	156.5	155.5
6922	3278	03.9	50.6	37.09	"	33511	3466	1717	174.9	170.7	170.7	1863	160.3	156.1
6919	3279	02.0	52.4	153.35	"	30855	3559	1689	187.0	169.8	169.8	1835	172.4	155.2
"	3284	"	"	"	"	30836	3557	"	186.8	169.6	169.6	"	172.2	155.0
6917	3280	00.3	53.4	10.76	"	33214	3355	1663	169.2	168.0	168.0	1809	154.6	153.4
6909	3283	56.0	56.3	30.51	"	31882	3282	1600	168.2	164.8	164.8	1746	153.6	150.2
6908	3282	55.1	55.1	181.33	"	28778	3437	1600	183.7	163.5	163.5	1746	169.1	148.9
6907	3281	55.8	53.8	225.93	"	27658	3463	1597	186.6	161.3	161.3	1743	172.0	146.7
6900	3271	50.6	57.9	3.87	XII 16	31483	3160	1519	164.1	163.7	163.7	1666	149.4	149.0
6897	3270	48.6	57.9	16.15	"	31098	3160	1490	167.0	165.2	165.2	1636	152.4	150.6
6894	3269	46.0	57.6	200.32	"	27227	3341	1451	189.0	166.6	166.6	1598	174.3	151.9
6891	3268	43.7	58.1	5.86	"	30199	3038	1417	162.1	161.4	161.4	1564	147.4	146.7
6888	3267	41.2	58.2	4.95	"	29630	2978	1380	159.8	159.3	159.3	1527	145.1	144.6
6886	3266	39.6	58.2	15.82	"	29070	2956	1357	159.9	158.1	158.1	1503	145.3	143.5

Table XI. (Continued)

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula		
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)
Miyako	3265	39° 38.4	141° 58.1	42.70	XII 16	28294	2961	2913	1339	162.2	157.4	1486	147.5	142.7
	3263	38.4	57.8	3.62	XII 15	29007	2912	2908	1339	157.3	156.9	1486	142.6	142.2
	3262	36.0	57.2	1.66	"	28426	2848	2846	1303	154.3	154.3	1450	139.8	139.6
	3261	34.3	56.4	6.12	"	28153	2834	2827	1278	155.6	154.9	1425	140.9	140.2
6876	3260	31.3	56.2	44.11	"	27656	2902	2852	1234	166.8	161.8	1381	152.1	147.1
6875	3259	30.7	57.1	73.92	"	27218	2950	2867	1225	172.5	164.2	1372	157.8	149.5
6872	3258	28.0	57.3	6.88	"	27832	2804	2797	1185	161.9	161.2	1332	147.2	146.5
6869	3257	25.4	58.5	22.77	"	27488	2819	2794	1146	167.3	164.8	1294	152.5	150.0
6868	3256	24.6	58.0	47.86	"	26411	2789	2735	1135	165.4	160.0	1282	150.7	145.3
6861	3255	20.1	53.8	1.91	"	26170	2623	2621	1068	155.5	155.3	1216	140.7	140.5
6859	3254	18.2	53.6	2.85	"	25944	2603	2600	1040	156.3	156.0	1188	141.5	141.2
J. 3	3236	16.3	53.0	2.41	XII 14	25811	2589	2586	1012	157.7	157.4	1160	142.9	142.6
6808	3237	14.8	53.5	13.07	"	25547	2595	2580	0990	160.5	159.0	1137	145.8	144.3
6804	3238	12.3	52.5	45.00	"	24522	2591	2541	0953	163.8	158.8	1101	149.0	144.0
6802	3239	11.4	52.0	11.42	"	25001	2535	2523	0940	159.5	158.3	1087	144.8	143.6
6799	3240	09.3	51.1	34.98	"	23847	2493	2454	0909	158.4	154.5	1056	143.7	139.8
"	3252	"	"	"	XII 15	23882	2496	2457	"	158.7	154.8	"	144.0	140.1
6794	3251	07.4	46.3	322.50	"	17964	2792	2431	0881	191.1	155.0	1029	176.3	140.2
6793	3242	07.3	45.1	136.05	XII 14	21127	2533	2380	0879	165.4	150.1	1027	150.6	135.3
6790	3243	05.4	42.5	10.89	"	22747	2308	2296	0851	145.7	144.5	0999	130.9	129.7
"	3249	"	"	"	"	22777	2311	2299	"	146.0	144.8	"	131.2	130.0
6788	3244	03.5	43.5	2.66	"	23053	2314	2311	0823	149.1	148.8	0971	134.3	134.0
6787	3245	02.4	43.6	4.38	"	22436	2257	2252	0807	145.0	144.5	0955	130.2	129.7
6782	3246	00.6	38.0	2.30	"	22003	2207	2205	0780	142.7	142.5	0928	127.9	127.7
6779	3247	59.3	37.0	7.36	"	21622	2185	2177	0761	142.4	141.6	0909	127.6	126.8

\* Weather Station Bench Mark.

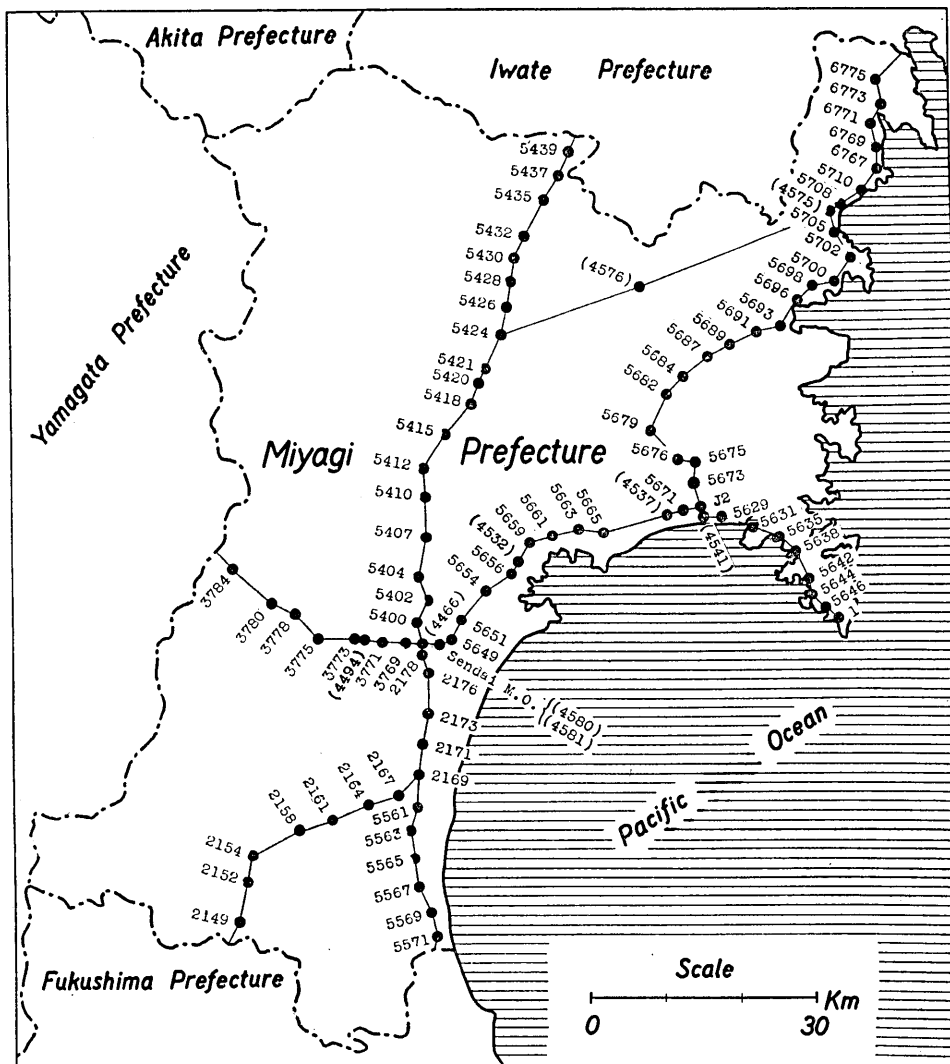


Fig. 12. Gravity Stations in Miyagi Prefecture.

(震研彙報 別冊 第四号 図版 坪井・実川・田島)

(3) Miyagi Prefecture  
Table XII. Synoptic Results for Miyagi Prefecture (I).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	$g$ 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula						
									$\gamma_0$ 980.	$\Delta g_0'$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0'$ (mgal.)	$\Delta g_0''$ (mgal.)				
		38°	141°															
6775	4573	56.6	34.7	20.87	IX 25	20725	2137	2114	0721	141.6	139.3	0870	126.7	124.4				
6773	4572	54.7	35.2	1.30	"	20902	2094	2093	0692	140.1	140.0	0842	125.2	125.1				
6771	4571	53.3	34.3	2.16	"	20619	2069	2066	0673	139.6	139.3	0821	124.8	124.5				
6769	4570	51.6	35.0	21.40	"	20353	2101	2077	0648	145.3	142.9	0795	130.5	128.1				
6767	4569	49.6	34.8	17.56	"	20298	2084	2064	0618	146.6	144.6	0767	131.7	129.7				
5710	4568	48.3	33.3	17.77	"	20018	2057	2037	0599	145.8	143.8	0748	130.9	128.9				
5708	4567	47.4	31.2	54.67	"	18991	2068	2007	0586	148.2	142.1	0735	133.3	127.2				
5705	4566	45.5	30.4	38.76	"	19105	2030	1987	0558	147.2	142.9	0707	132.3	128.0				
5702	4565	43.4	31.2	41.21	"	19026	2030	1984	0527	150.3	145.7	0676	135.4	130.8				
5700	4564	41.9	30.7	47.32	"	18775	2024	1971	0505	151.9	146.6	0654	137.0	131.7				
5698	4563	41.6	28.8	11.64	"	19243	1960	1947	0501	145.9	144.6	0649	131.1	129.8				
5696	4562	40.5	27.5	2.22	"	19365	1943	1941	0485	145.8	145.6	0633	131.0	130.8				
5693	4560	38.7	25.7	11.19	IX 24	19007	1935	1923	0458	147.7	146.5	0607	132.8	131.6				
5691	4559	38.4	23.2	110.32	"	16842	2025	1901	0454	157.1	144.7	0602	142.3	129.9				
5689	4558	37.4	20.8	11.31	"	18503	1885	1873	0439	144.6	143.4	0588	129.7	128.5				
5687	4557	36.4	18.8	9.51	"	18263	1856	1845	0424	143.2	142.1	0573	128.3	127.2				
5684	4556	35.1	16.5	4.65	"	18062	1821	1815	0405	141.6	141.0	0554	126.7	126.1				
5682	4555	33.6	14.8	4.18	"	17745	1787	1783	0383	140.4	140.0	0532	125.5	125.1				
5679	4554	31.3	13.8	3.75	"	17157	1727	1723	0349	137.8	137.4	0498	122.9	122.5				
5676	4553	29.3	16.1	2.33	"	17721	1779	1777	0320	145.9	145.7	0469	131.0	130.8				
5675	4552	29.0	17.4	2.27	"	17967	1804	1801	0316	148.8	148.5	0465	133.9	133.6				
5673	4551	27.6	17.7	4.99	"	18376	1853	1847	0295	155.8	155.2	0444	140.9	140.3				
J. 2	4539	25.9	18.1	1.86	IX 23	17938	1800	1797	0270	153.0	152.7	0419	138.1	137.8				
5671	4538	25.6	16.3	3.03	"	16507	1660	1657	0256	139.4	139.1	0415	124.5	124.2				
5665	4536	24.2	09.3	2.87	"	12655	1274	1271	0245	102.9	102.6	0394	88.0	87.7				

Table XII. (Continued)

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	$g$ 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula			
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	
		38°	141°												
5663	4535	24.5	07.0	23.03	IX 23	12035	1275	1249	0249	102.6	100.0	0399	87.6	85.0	
5661	4534	23.9	04.5	6.93	"	13309	1352	1345	0241	111.1	110.4	0390	96.2	95.5	
5659	4533	23.4	02.6	21.94	"	13935	1461	1437	0233	122.8	120.4	0383	107.8	105.4	
5656	4531	20.9	00.8	43.08	"	14591	1592	1544	0197	139.5	134.7	0346	124.6	119.8	
5654	4530	19.6	59.0	10.47	"	15350	1567	1556	0177	139.0	137.9	0327	124.0	122.9	
5651	4528	17.5	56.4	10.11	"	13277	1359	1348	0147	121.2	120.1	0297	106.2	105.1	
5649	4527	16.0	54.8	26.14	"	12199	1301	1271	0125	117.6	114.6	0275	102.6	99.6	
Sendai	M.O.**	15.6	54.0	39.26	IX 26	11458	1267	1223	0119	114.8	110.4	0269	99.8	95.4	
"	"	"	54.0	"	"	11457	"	"	"	"	"	"	"	"	

\* Meteorological Observatory Seismometer Room, on the Surface of the Concrete Block for Seismometer Installation.

\*\* Meteorological Observatory, on the Block Formerly Used for the Silver Disk Pyrheliometer Observation.

Synoptic Results for Miyagi Prefecture (II).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	$g$ 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula			
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	
		38°	141°												
Ishinomaki	W.S.*	25.5	18.2	43.30	IX 24	16843	1818	1769	0264	155.4	150.5	0414	140.4	135.5	
5629	4542	25.0	20.0	2.18	"	18329	1840	1837	0257	158.3	158.0	0406	143.4	143.1	
5631	4543	24.7	22.4	1.35	"	18865	1891	1889	0252	163.9	163.7	0402	148.9	148.7	
5635	4544	23.6	25.1	32.43	"	18592	1959	1923	0236	172.3	168.7	0386	157.3	153.7	
5638	4545	22.7	26.7	8.81	"	19142	1941	1932	0223	171.8	170.9	0373	156.8	155.9	
5642	4546	20.8	28.0	2.99	"	19110	1920	1917	0195	172.5	172.2	0345	157.5	157.2	
5640	4547	19.5	28.7	4.11	"	19227	1935	1931	0176	175.9	175.5	0326	160.9	160.5	
5646	4548	18.3	29.5	19.70	"	18718	1933	1911	0158	177.5	175.3	0308	162.5	160.3	
I	4549	17.7	30.5	2.85	"	18976	1906	1903	0150	175.6	175.3	0299	160.7	160.4	

\* Weather Station Seismometer Room, on the Surface of the Concrete Block for Seismometer Installation.

Synoptic Results for Miyagi Prefecture (III).

B.M.	No.	$\phi$	$\lambda$	H (m)	Date	g 980.	g <sub>0</sub> 980.	g <sub>0</sub> '' 980.	HELMERT Formula of 1901			International Formula		
									γ <sub>0</sub> 980.	Δg <sub>0</sub> (mgal.)	Δg <sub>0</sub> '' (mgal.)	γ <sub>0</sub> 980.	Δg <sub>0</sub> (mgal.)	Δg <sub>0</sub> '' (mgal.)
5439	4523	38° 51.3	141° 06.2	103.53	IX 23	13485	1668	1552	0643	102.5	90.9	0792	87.6	76.0
5437	4522	49.8	05.2	32.61	"	14362	1537	1500	0621	91.6	87.9	0770	76.7	73.0
5435	4521	47.7	04.2	16.13	"	14463	1496	1478	0590	90.6	88.8	0739	75.7	73.9
5432	4520	45.3	02.1	21.42	"	13704	1437	1413	0555	88.2	85.8	0704	73.3	70.9
5430	4519	43.7	01.3	52.82	"	12182	1381	1322	0532	84.9	79.0	0680	70.1	64.2
"	4525	"	"	"	"	12174	1380	1321	"	84.8	78.9	"	70.0	64.1
5428	4517	42.0	00.8	37.43	IX 22	12112	1327	1285	0507	82.0	77.8	0655	67.2	63.0
5426	4516	40.3	00.8	33.09	"	11810	1283	1246	0482	80.1	76.4	0630	65.3	61.6
5424	4515	38.3	00.0	43.51	"	11463	1281	1232	0452	82.9	78.0	0601	68.0	63.1
"	4577	"	"	"	IX 25	11451	1279	1231	"	82.7	77.9	"	67.8	63.0
5421	4514	35.7	58.8	20.07	IX 22	11714	1233	1211	0414	81.9	79.7	0563	67.0	64.8
5420	4513	34.9	58.3	19.83	"	11252	1186	1164	0402	78.4	76.2	0551	63.5	61.3
5418	4512	32.9	57.4	17.73	"	10602	1115	1095	0373	74.2	72.2	0522	59.3	57.3
5415	4511	31.0	54.8	23.02	"	11329	1204	1178	0345	85.9	83.3	0494	71.0	68.4
5412	4510	28.5	52.7	34.41	"	11405	1247	1208	0308	93.9	90.0	0457	79.0	75.1
5410	4509	26.6	53.2	29.63	"	11912	1283	1249	0280	100.3	96.9	0430	85.3	81.9
5407	4508	23.8	53.3	29.53	"	11732	1264	1231	0239	102.5	99.2	0389	87.5	84.2
5404	4507	21.0	52.6	48.34	"	11147	1264	1210	0198	106.6	101.2	0348	91.6	86.2
5402	4506	19.0	53.5	21.90	"	11596	1227	1203	0169	105.8	103.4	0318	90.9	88.5
5400	4505	17.0	52.4	49.38	"	10178	1170	1115	0139	103.1	97.6	0289	88.1	82.6

Synoptic Results for Miyagi Prefecture (IV).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula		
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)
3784	4500	38° 21.2	140° 35.9	383.08	IX 22	01698	1352	0923	0201	115.1	72.2	0351	100.1	57.2
3780	4498	18.7	39.0	234.94	"	03835	1109	0846	0164	94.5	68.2	0314	79.5	53.2
3778	4497	17.6	41.3	191.65	"	04446	1036	0822	0148	88.8	67.4	0298	73.8	52.4
3775	4496	16.2	43.5	146.18	"	05127	0964	0800	0128	83.6	67.2	0277	68.7	52.3
3773	4495	16.1	46.2	107.98	"	07467	1080	0959	0126	95.4	83.3	0276	80.4	68.3
"	4503	"	"	"	"	07470	1080	0959	"	95.4	83.3	"	80.4	68.3
3771	4493	15.9	48.8	74.80	"	08759	1107	1023	0123	98.4	90.0	0273	83.4	75.0
3769	4492	16.0	51.0	60.12	"	09514	1137	1070	0125	101.2	94.5	0275	86.2	79.5

Synoptic Results for Miyagi Prefecture (V).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula		
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)
2178	4467	38° 15.2	140° 52.7	35.67	IX 21	10634	1174	1134	0113	106.1	102.1	0263	91.1	87.1
2176	4468	13.7	53.3	12.70	"	10968	1136	1122	0091	104.5	103.1	0241	89.5	88.1
2173	4469	10.5	53.3	6.14	"	11101	1129	1122	0044	108.5	107.8	0194	93.5	92.8
2171	4470	08.4	52.8	3.94	"	10953	1108	1103	0014	109.4	108.9	0164	94.4	93.9
J. 2169	4471	06.3	52.2	4.47	"	10406	1054	1049	9983	107.1	106.6	0133	92.1	91.6
"	4489	"	"	"	"	10410	1055	1050	"	107.2	106.7	"	92.2	91.7
2167	4472	04.9	50.5	6.63	"	10147	1035	1028	9962	107.3	106.6	0112	92.3	91.6
2164	4473	03.8	47.2	12.31	"	08593	0897	0884	9946	95.1	93.8	0096	80.1	78.8
2161	4474	02.8	44.3	18.71	"	07709	0829	0808	9932	89.7	87.6	0082	74.7	72.6
"	4480	"	"	"	"	07712	0829	0808	"	89.7	87.6	"	74.7	72.6

2158	4475	02.2	40.9	26.35	"	07746	0856	0826	9923	93.3	90.3	0073	78.3	75.3
2154	4476	00.4	37.3	48.60	"	05023	0652	0598	9897	75.5	70.1	0047	60.5	55.1
2152	4477	58.6 37°	37.0	65.90	"	05552	0759	0685	9870	88.9	81.5	0021	73.8	66.4
2149	4478	55.6	36.3	144.70	"	02737	0720	0558	9826	89.4	73.2	979 9977	74.3	58.1

Synopsis Results for Miyagi Prefecture (VI).

B.M.	No.	$\phi$	$\lambda$	H (m)	Date	g 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901		International Formula			
									$\gamma_0$ 979.	$\Delta g_0$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0'$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0'$ (mgal.)
5561	4482	04.4	52.2	4.80	IX 21	09751	0990	0985	9955	103.5	103.0	0105	88.5	88.0
5563	4483	02.3	51.5	4.34	"	09876	1001	0996	9924	107.7	107.2	0075	92.6	92.1
5565	4484	00.4	52.0	6.60	"	09436	0964	0957	9897	106.7	106.0	0047	91.7	91.0
5567	4485	58.3 37°	52.7	8.53	"	09645	0991	0981	9866	112.5	111.5	0016	97.5	96.5
5569	4486	56.3	53.8	11.19	"	10068	1041	1029	9837	120.4	119.2	9987	105.4	104.2
5571	4487	54.6	54.5	6.13	"	10321	1051	1044	9812	123.9	123.2	9962	108.9	108.2



(4) Akita Prefecture.

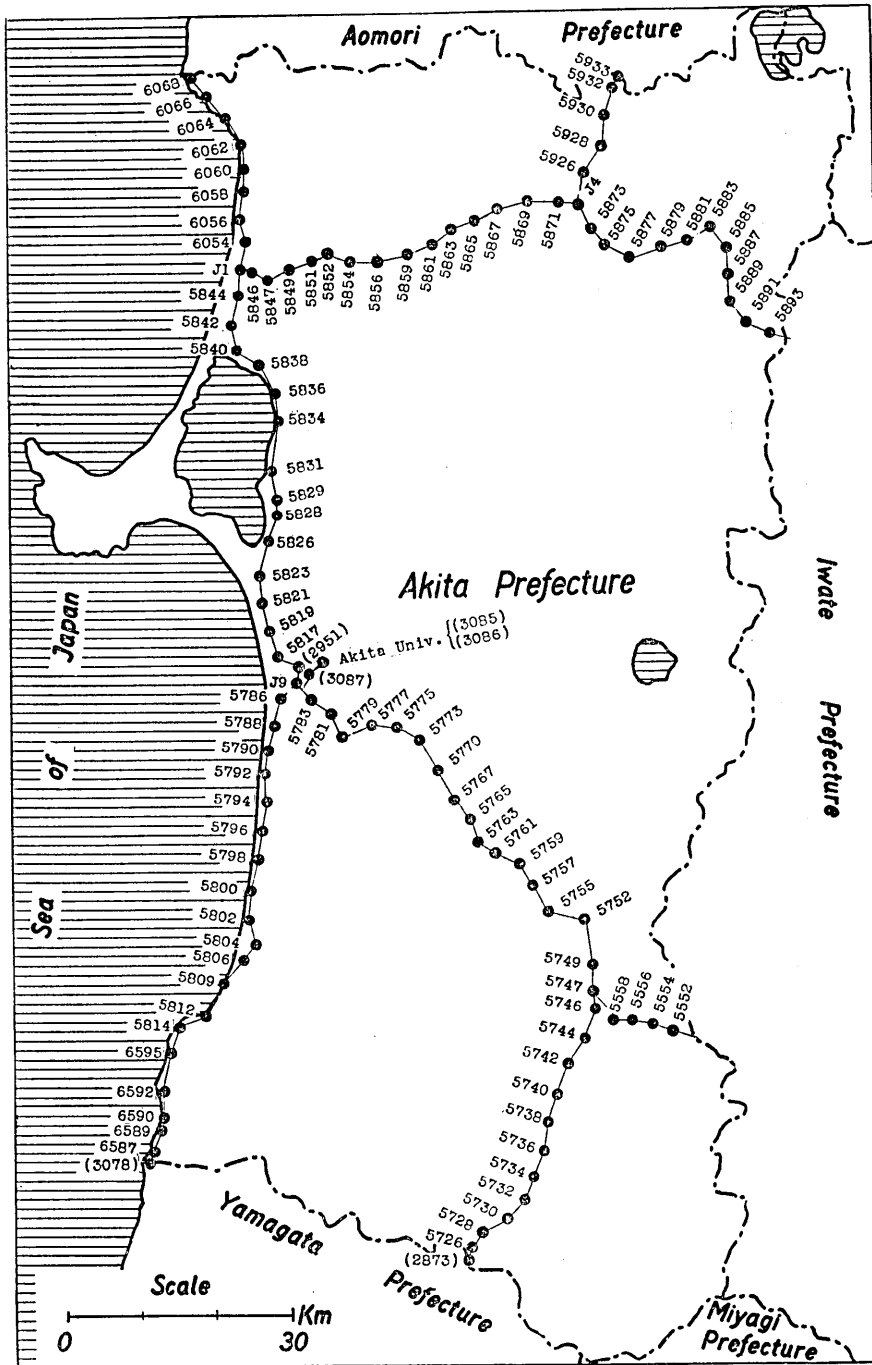


Fig. 13. Gravity Stations in Akita Prefecture.

Table XIII. Synoptic Results for Akita Prefecture (I).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	$g$ 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula			
									$\Delta g_0'$ (mgal.)	$\Delta g_0''$ (mgal.)	$\Delta g_0'''$ (mgal.)	$\gamma_0$ 980.	$\Delta \gamma_0$ (mgal.)	$\Delta \gamma_0''$ (mgal.)	
									$\gamma_0$ 980.	$\Delta \gamma_0'$ (mgal.)	$\Delta \gamma_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta \gamma_0$ (mgal.)	$\Delta \gamma_0''$ (mgal.)	
6068 6066	3020	40° 25.3	139° 57.0	48.51	1952	29612	3111	3057	2035	107.6	102.2	2180	93.1	87.7	
	3019	24.0	58.5	19.38	"	29606	3020	2999	2016	100.4	98.3	2161	85.9	83.8	
	6064 6062	3018	22.8	00.0	24.29	"	28973	2972	2945	1993	97.4	94.7	2143	82.9	80.2
		3017	21.0	01.8	5.76	"	27653	2783	2777	1971	81.2	80.6	2116	66.7	66.1
	6060	19.2	02.2	8.43	"	25981	2624	2615	1944	68.0	67.1	2089	53.5	52.6	
	6058 6056 6054 J. 5844	3015	17.7	02.3	21.23	"	24470	2513	2489	1922	59.1	56.7	2037	44.6	42.2
3014		15.8	01.8	12.47	"	23308	2359	2355	1894	47.5	46.1	2039	33.0	31.6	
3013		14.0	02.0	5.66	"	22880	2306	2299	1867	43.9	43.2	2012	29.4	28.7	
3012		12.2	01.6	9.75	"	22452	2275	2264	1840	43.5	42.4	1986	28.9	27.8	
3009		10.1	01.7	6.21	XI 22	22453	2265	2258	1809	45.6	44.9	1955	31.0	30.3	
5842 5840 5838 5836 5834	3008	08.0	00.9	12.41	"	22314	2270	2256	1778	49.2	47.8	1923	34.7	33.3	
	3007	05.9	01.0	5.95	"	22932	2315	2308	1747	56.8	56.1	1892	42.3	41.6	
	3006	04.7	03.3	3.87	"	24300	2442	2433	1729	71.3	70.9	1875	56.7	56.3	
	3005	02.9	05.0	5.13	"	24514	2467	2462	1702	76.5	76.0	1848	61.9	61.4	
	3004	00.7	05.0	4.83	"	25011	2516	2511	1669	84.7	84.2	1815	70.1	69.6	
5831 5829 5828 5826 5823	3003	39° 57.5	04.7	3.93	"	25134	2526	2521	1622	90.4	89.9	1768	75.8	75.3	
	3002	55.5	05.0	3.40	"	23145	2325	2321	1592	73.3	72.9	1738	58.7	58.3	
	3001	54.3	04.9	3.77	"	22237	2235	2231	1574	66.1	65.7	1721	51.4	51.0	
	3000	52.4	04.3	3.11	"	21404	2150	2147	1546	60.4	60.1	1692	45.8	45.5	
	2998	49.9	03.4	12.15	"	19305	1988	1954	1509	45.9	44.5	1655	31.3	29.9	
5821 5819 5817 Akita W.S.* J. 9	2997	47.9	03.9	11.29	"	18576	1892	1880	1479	41.3	40.1	1626	26.6	25.4	
	2996	45.9	04.5	3.79	"	18412	1853	1849	1450	40.3	39.9	1596	25.7	25.3	
	2995	44.0	05.3	28.89	"	17826	1872	1840	1422	45.0	41.8	1568	30.4	27.2	
	2951	43.1	06.1	9.90	XI 20	18571	1888	1877	1408	48.0	46.9	1555	33.3	32.2	
	2994	42.5	06.4	8.50	XI 22	18617	1888	1878	1399	48.9	47.9	1546	34.2	33.2	

\* Weather Station, on the Block for the Pyrheliometer Observation.

Table XIII. (Continued)

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula		
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)
5786	2952	39° , 41.0	140° , 05.3	12.03	XI 20	17906	1828	1814	1377	45.1	43.7	1524	30.4	29.0
5788	2953	38.9	04.6	14.41	"	17329	1777	1761	1346	43.1	41.5	1493	28.4	26.8
5790	3063	37.0	04.1	22.34	XI 25	16841	1753	1728	1318	43.5	41.0	1465	28.8	26.3
5792	3064	35.2	03.9	23.23	"	16624	1734	1708	1291	44.3	41.7	1438	29.6	27.0
5794	3065	33.2	03.6	14.39	"	16459	1690	1674	1262	42.8	41.2	1409	28.1	26.5
5796	3066	31.1	03.3	30.34	"	15407	1634	1600	1231	40.3	36.9	1378	25.6	22.2
5798	3067	29.0	02.9	18.24	"	15256	1582	1562	1200	38.2	36.2	1347	23.5	21.5
5800	3068	27.0	02.4	15.92	"	14848	1534	1516	1170	36.4	34.6	1317	21.7	19.9
5802	3069	24.9	02.0	25.54	"	13920	1471	1442	1139	33.2	30.3	1286	18.5	15.6
5804	3070	23.3	02.8	6.50	"	14754	1496	1488	1115	38.1	37.3	1263	23.3	22.5
"	3081	"	"	"	"	14750	1495	1488	"	38.0	37.3	"	23.2	22.5
5806	3080	21.7	01.6	47.74	"	12706	1418	1365	1092	32.6	27.3	1239	17.9	12.6
5809	3071	19.9	59.8	10.47	"	13106	1343	1331	1065	27.8	26.6	1213	13.0	11.8
5812	3072	17.3	57.9	3.81	"	13244	1336	1332	1027	30.9	30.5	1174	16.2	15.8
5814	3073	16.4	56.0	10.75	"	13386	1372	1360	1013	35.9	34.7	1161	21.1	19.9
6595	3074	14.7	55.2	6.02	"	13729	1392	1385	0988	40.4	39.7	1136	25.6	24.9
6592	3075	12.0	54.3	6.14	"	14301	1449	1442	0948	50.1	49.4	1096	35.3	34.6
6590	3076	10.1	54.5	6.67	"	15244	1545	1538	0920	62.5	61.8	1068	47.7	47.0
6589	3079	09.2	54.0	10.49	"	15329	1565	1554	0907	65.8	64.7	1055	51.0	49.9
6587	3077	07.5	53.1	20.44	"	14107	1474	1451	0882	59.2	56.9	1030	44.4	42.1

Synoptic Results for Akita Prefecture (II).

B.M.	No.	$\phi$	$\lambda$	H (m)	Date	g 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula			
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	
		40°	140°		1952										
5846	3024	11.4	02.9	8.15	XI 23	22708	2296	2287	1828	46.8	45.9	1974	32.2	31.3	
5847	3059	11.2	04.2	8.55	XI 24	23115	2338	2328	1825	51.3	50.3	1971	36.7	35.7	
5849	3025	12.0	06.8	9.78	XI 23	25785	2609	2598	1837	77.2	76.1	1983	62.6	61.5	
5851	3026	12.6	09.1	10.71	"	24740	2507	2495	1846	66.1	64.9	1992	51.5	50.3	
5852	3027	13.2	10.1	11.81	"	24731	2510	2496	1855	65.5	64.1	2001	50.9	49.5	
5854	3028	12.3	12.4	16.28	"	24747	2525	2507	1842	68.3	66.5	1987	53.8	52.0	
5856	3029	12.3	14.7	17.20	"	25038	2557	2538	1842	71.5	69.6	1987	57.0	55.1	
5859	3030	12.7	17.2	33.20	"	25434	2646	2609	1848	79.8	76.1	1993	65.3	61.6	
5861	3031	13.2	20.0	30.44	"	25051	2599	2565	1855	74.4	71.0	2001	59.8	56.4	
5863	3032	14.7	22.0	38.89	"	24924	2612	2569	1877	73.5	69.2	2023	58.9	54.6	
5865	3033	15.3	24.1	42.19	"	25737	2704	2657	1886	81.8	77.1	2032	67.2	62.5	
5867	3034	16.1	26.8	46.66	"	26496	2794	2741	1898	89.6	84.3	2044	75.0	69.7	
5869	3035	16.5	29.2	44.87	"	26450	2784	2733	1904	88.0	82.9	2049	73.5	68.4	
5871	3036	16.3	32.1	58.70	"	25240	2705	2639	1901	80.4	73.8	2046	65.9	59.3	

Synoptic Results for Akita Prefecture (III).

B.M.	No.	$\phi$	$\lambda$	H (m)	Date	g 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula		
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)
		40°	140°		1952									
5933	3043	24.9	37.1	227.19	XI 24	23238	3025	2771	2029	99.6	74.2	2174	85.1	59.7
5932	3042	24.0	36.7	175.77	"	24621	3005	2808	2016	98.9	79.2	2161	84.4	64.7
5930	3041	21.7	35.7	124.23	"	25447	2928	2789	1981	94.7	80.8	2127	80.1	66.2
5928	3040	19.8	35.1	88.09	"	25896	2861	2763	1953	90.8	81.0	2098	76.3	66.5
5926	3039	18.1	34.0	67.42	"	25742	2782	2707	1928	85.4	77.9	2073	70.9	63.4

Table XIII. (Continued)

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g 980.	g <sub>0</sub> 980.	g <sub>0</sub> '' 980.	HELMERT Formula of 1901			International Formula		
									$\gamma_0$ 980.	$\Delta g_0'$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0'$ (mgal.)	$\Delta g_0''$ (mgal.)
J.	4	40° 16.1	140° 33.5	60.88	1952	24971	2685	2617	1898	78.7	71.9	2044	64.1	57.3
	5873	14.0	35.1	57.13	XI 24	24398	2616	2552	1867	74.9	68.5	2012	60.4	54.0
	5875	12.9	36.8	67.98	"	24072	2617	2541	1851	76.6	69.0	1996	62.1	54.5
	5877	12.7	39.4	76.83	"	23778	2615	2529	1848	76.7	68.1	1993	62.2	53.6
	5879	13.6	41.6	82.32	"	23972	2651	2559	1861	79.0	69.8	2006	64.5	55.3
5881	13.5	44.1	90.26	"	23541	2633	2532	1859	77.4	67.3	2005	62.8	52.7	
5883	14.7	45.1	111.30	"	23842	2728	2603	1877	85.1	72.6	2023	70.5	58.0	
5885	13.0	47.5	119.37	"	21796	2548	2414	1852	69.6	56.2	1998	55.0	41.6	
5887	11.2	47.6	137.33	"	21057	2530	2376	1825	70.5	55.1	1971	55.9	40.5	
5889	09.1	48.1	162.59	"	19740	2476	2294	1794	68.2	50.0	1940	53.6	35.4	
5891	07.7	49.2	198.38	"	19674	2580	2358	1773	80.7	58.5	1919	66.1	43.9	
5893	07.1	51.9	237.60	"	18314	2565	2299	1764	80.1	53.5	1910	65.5	38.9	

Synoptic Results for Akita Prefecture (IV).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g 980.	g <sub>0</sub> 980.	g <sub>0</sub> '' 980.	HELMERT Formula of 1901			International Formula			
									$\gamma_0$ 980.	$\Delta g_0'$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0'$ (mgal.)	$\Delta g_0''$ (mgal.)	
5783	2956	39° 41.1	140° 07.7	5.50	XI 21	18740	1891	1885	1379	51.2	50.6	1525	36.6	36.0	
	5781	40.1	09.9	35.11	"	18511	1959	1920	1364	59.5	55.6	1511	44.8	40.9	
	5779	38.4	11.3	12.18	"	19316	1969	1956	1339	63.0	61.7	1486	48.3	47.0	
	5777	2959	39.0	13.7	20.20	"	18641	1926	1904	1348	57.8	55.6	1494	43.2	41.0
	5775	2960	39.0	16.1	31.76	"	18112	1909	1874	1348	56.1	52.6	1494	41.5	38.0
5773	2961	38.1	18.3	92.43	"	16715	1957	1853	1334	62.3	51.9	1481	47.6	37.2	
5770	2962	35.4	19.9	54.42	"	18671	2035	1974	1294	74.1	68.0	1441	59.4	53.3	
5767	2963	33.5	21.3	21.17	"	17824	1848	1824	1266	58.2	55.8	1413	43.5	41.1	
5765	2964	32.3	23.0	16.49	"	18101	1861	1843	1248	61.3	59.5	1395	46.6	44.8	
5763	2965	30.4	23.3	17.53	"	17984	1853	1833	1220	63.3	61.3	1367	48.6	46.6	

5761	2966	29.3	25.6	23.86	"	18194	1893	1866	1204	68.9	66.2	1351	54.2	51.5
5759	2967	28.5	27.7	24.25	"	17961	1871	1844	1192	67.9	65.2	1339	53.2	50.5
5757	2968	26.8	28.8	26.05	"	17434	1824	1795	1167	65.7	62.8	1314	51.0	48.1
5755	2969	25.3	30.3	27.59	"	16957	1781	1750	1145	63.6	60.5	1292	48.9	45.8
5752	2970	24.3	33.7	57.63	"	16030	1781	1716	1130	65.1	58.6	1277	50.4	43.9
5749	2971	21.4	34.0	74.43	"	15606	1790	1707	1087	70.3	62.0	1235	55.5	47.2
5747	2972	19.3	34.1	56.74	"	15866	1762	1698	1056	70.6	64.2	1204	55.8	49.4
5746	2979	17.7	34.0	75.94	"	15218	1756	1671	1033	72.3	63.8	1180	57.6	49.1
5744	2980	15.9	33.2	89.42	"	14217	1698	1598	1006	69.2	59.2	1154	54.4	44.4
5742	2981	14.0	32.1	86.49	"	13723	1639	1542	0978	66.1	56.4	1126	51.3	41.6
5740	2982	12.1	30.9	87.72	"	14380	1709	1611	0950	75.9	66.1	1098	61.1	51.3
5738	2983	10.2	29.8	85.73	"	14280	1693	1597	0922	77.1	67.5	1070	62.3	52.7
5736	2985	07.9	29.5	107.32	XI 22	13488	1680	1560	0888	79.2	67.2	1036	64.4	52.4
5734	2986	05.9	29.0	112.33	"	13139	1661	1535	0858	80.3	67.7	1006	65.5	52.9
5732	2987	04.1	27.8	136.40	"	11413	1562	1410	0832	73.0	57.8	0980	58.2	43.0
5730	2988	02.9	25.7	160.64	"	10379	1534	1354	0814	72.0	54.0	0962	57.2	39.2
5728	2989	02.0	23.6	216.16	"	09734	1641	1399	0801	84.0	59.8	0919	69.2	45.0
"	2992	"	"	"	"	09742	1641	1399	"	84.0	59.8	"	69.2	45.0
5726	2990	00.4	22.5	336.34	"	07757	1814	1437	0777	103.7	66.0	0926	88.8	51.1

Synoptic Results for Akita Prefecture (V).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula			
									$\gamma_0$ 980.	$\Delta\gamma_0$ (mgal.)	$\Delta\gamma_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta\gamma_0$ (mgal.)	$\Delta\gamma_0''$ (mgal.)	
		39°	140°												
5558	2973	17.3	35.9	89.48	XI 21	15548	1831	1731	1027	80.4	70.4	1174	65.7	55.7	
5556	2974	16.9	37.9	134.24	"	14677	1882	1732	1021	86.1	71.1	1168	71.4	56.4	
5554	2975	17.5	39.2	144.69	"	14407	1887	1725	1030	85.7	69.5	1177	71.0	54.8	
5552	2976	16.7	41.0	213.55	"	12757	1935	1695	1018	91.7	67.8	1165	77.0	53.1	

(5) Yamagata Prefecture,

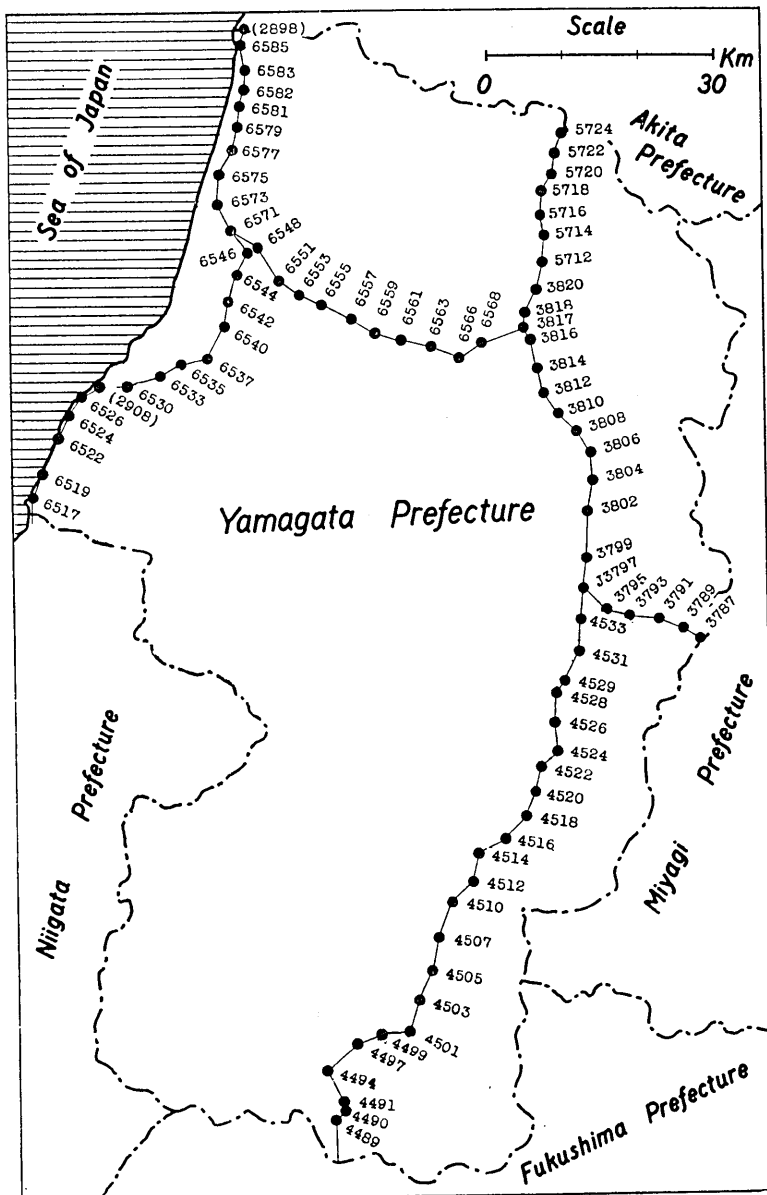


Fig. 14. Gravity Stations in Yamagata Prefecture.

Table XIV. Synoptic Results for Yamagata Prefecture (1).

B.M.	No.	$\phi$	$\lambda$	H (m)	Date	g 980.	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula		
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)
6585	2897	39° 05.7	139° 53.0	10.11	XI 8	13237	1355	1344	0856	49.9	48.8	1003	35.2	34.1
6583	2896	04.0	53.1	2.90	"	12527	1262	1258	0830	43.2	42.8	0978	28.4	28.0
6582	2895	03.2	53.4	11.41	"	11680	1203	1190	0819	38.4	37.1	0967	23.6	22.3
6581	2894	02.3	53.1	23.67	"	10763	1149	1123	0805	34.4	31.8	0953	19.6	17.0
6579	2893	00.4	52.6	9.93	"	10114	1042	1031	0777	26.5	25.4	0926	11.6	10.5
6577	2892	38° 58.5	52.2	8.82	"	09337	0961	0951	0749	21.2	20.2	0898	6.3	5.3
6575	2891	56.7	50.3	2.76	"	08924	0901	0898	0723	17.8	17.5	0871	3.0	2.7
6573	2890	54.5	50.6	3.23	"	08463	0856	0853	0690	16.6	16.3	0839	1.7	1.4
6571	2886	52.3	51.9	5.32	XI 7	08326	0849	0843	0658	19.1	18.5	0806	4.3	3.7
6548	2885	51.4	53.9	6.87	"	09017	0923	0915	0645	27.8	27.0	0793	13.0	12.2
6546	2900	50.9	53.1	6.42	XI 8	08820	0902	0895	0637	26.5	25.8	0786	11.6	10.9
6544	2901	49.2	51.5	6.30	"	08514	0871	0864	0612	25.9	25.2	0761	11.0	10.3
6542	2902	47.4	51.4	9.96	"	08653	0896	0885	0586	31.0	29.9	0735	16.1	15.0
6540	2903	45.5	51.3	12.21	"	09028	0941	0927	0558	38.3	36.9	0707	23.4	22.0
6537	2904	43.6	48.6	15.81	"	10162	1065	1047	0530	53.5	51.7	0679	38.6	36.8
6535	2905	43.3	46.4	15.20	"	10372	1084	1067	0526	55.8	54.1	0674	41.0	39.3
6533	2906	42.4	44.6	19.58	"	10477	1108	1086	0512	59.6	57.4	0661	44.7	42.5
6530	2907	41.6	41.5	42.51	"	10795	1211	1163	0501	71.0	66.2	0649	56.2	51.4
6526	2909	40.9	37.8	26.76	"	11104	1193	1163	0490	70.3	67.3	0639	55.4	52.4
6524	2910	39.5	36.6	8.45	"	11129	1139	1130	0470	66.9	66.0	0619	52.0	51.1
6522	2911	37.6	35.6	5.68	"	10997	1117	1111	0442	67.5	66.9	0591	52.6	52.0
"	2914	"	"	"	"	10998	1117	1111	"	67.5	66.9	"	52.6	52.0
6519	2912	35.0	34.0	8.18	"	10583	1084	1074	0404	68.0	67.0	0553	53.1	52.1
6517	2913	33.3	33.0	4.38	"	10522	1066	1061	0379	68.7	68.2	0528	53.8	53.3



Synoptic Results for Yamagata Prefecture (II).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g 980.	g <sub>0</sub> 980.	g <sub>0</sub> '' 980.	HELMERT Formula of 1901			International Formula			
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	
		38°	139°												
6551	2884	48.7	56.0	12.20	XI 7	09033	0941	0927	0605	33.6	32.2	0754	18.7	17.3	
6553	2883	47.6	58.1	16.41	XI 9	09155	0966	0948	0589	37.7	35.9	0737	22.9	21.1	
6555	2882	47.3	00.5	25.80	XI 7	09916	1071	1042	0584	48.7	45.8	0733	33.8	30.9	
6557	2881	46.1	02.4	28.34	"	11112	1199	1167	0567	63.2	60.0	0715	48.4	45.2	
6559	2880	44.9	04.6	30.66	"	11759	1271	1236	0549	72.2	68.7	0698	57.3	53.8	
6561	2879	44.6	07.0	35.52	"	11668	1276	1237	0545	73.1	69.2	0693	58.3	54.4	
6563	2878	44.1	09.3	35.82	"	11536	1264	1224	0537	72.7	68.7	0686	57.8	53.8	
6566	2877	43.5	12.3	38.20	"	10412	1159	1116	0529	63.0	58.7	0677	48.2	43.9	
6568	2876	44.2	14.7	80.06	"	08020	1049	0960	0539	51.0	42.1	0688	36.1	27.2	

Synoptic Results for Yamagata Prefecture (III).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g 980.	g <sub>0</sub> 980.	g <sub>0</sub> '' 980.	HELMERT Formula of 1901			International Formula		
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)
		38°	140°											
5724	2872	59.1	21.9	259.65	XI 7	09207	1722	1432	0758	96.4	67.4	0906	81.6	52.6
5722	2871	57.7	21.5	363.64	"	07049	1827	1420	0738	108.9	68.2	0886	94.1	53.4
5720	2870	56.6	21.5	231.47	"	09364	1651	1392	0721	93.0	67.1	0870	78.1	52.2
5718	2869	55.0	20.2	172.86	"	09638	1497	1304	0698	79.9	60.6	0846	65.1	45.8
5716	2868	53.7	20.0	252.13	"	07690	1547	1265	0679	86.8	58.6	0827	72.0	43.8
5714	2867	52.1	20.2	159.93	"	09038	1397	1218	0655	74.2	56.3	0804	59.3	41.4
5712	2866	50.6	20.1	184.94	"	08195	1390	1183	0633	75.7	55.0	0781	60.9	40.2
3820	2865	48.4	19.5	153.43	"	07440	1218	1046	0601	61.7	44.5	0749	46.9	29.7
3818	2863	46.5	18.4	111.07	XI 6	07483	1091	0967	0573	51.8	39.4	0721	37.0	24.6
J. 3817	2875	45.6	18.1	97.57	XI 7	07429	1044	0935	0559	48.5	37.6	0708	33.6	22.7

Gravity Survey along the Lines of Precise Levels.

3816	2862	44.7	18.7	111.06	XI 6	06960	1039	0914	0546	49.3	36.8	0695	34.4	21.9
3814	2861	42.5	19.1	101.25	"	06856	0998	0885	0514	48.4	37.1	0663	33.5	22.2
3812	2860	40.6	19.8	142.77	"	05612	1002	0842	0486	51.6	35.6	0635	36.7	20.7
3810	2859	39.4	21.1	61.97	"	07023	0894	0824	0468	42.6	35.6	0617	27.7	20.7
3808	2858	37.9	23.0	83.50	"	06385	0896	0803	0446	45.0	35.7	0595	30.1	20.8
3806	2857	36.2	24.5	98.73	"	06493	0954	0844	0421	53.3	42.3	0570	38.4	27.4
3804	2856	34.2	24.5	98.86	"	06385	0944	0833	0392	55.2	44.1	0541	40.3	29.2
3802	2855	32.1	24.1	103.84	"	06286	0949	0833	0361	58.8	47.2	0510	43.9	32.3
3799	2854	28.8	23.7	88.23	"	06864	0959	0860	0313	64.6	54.7	0462	49.7	39.8
J. 3797	2846	26.7	23.4	101.68	"	05501	0864	0750	0282	58.2	46.8	0431	43.3	31.9
4533	2845	24.3	23.0	112.50	"	04550	0802	0676	0247	55.5	42.9	0396	40.6	28.0
4531	2844	22.0	22.5	104.46	"	05532	0876	0759	0213	66.3	54.6	0362	51.4	39.7
4529	2843	19.9	21.9	111.67	"	03860	0731	0606	0182	54.9	42.4	0332	39.9	27.4
4528	2842	18.9	20.9	105.50	"	03595	0685	0567	0167	51.8	40.0	0317	36.8	25.0
4526	2841	16.8	20.6	111.80	"	03330	0678	0553	0137	54.1	41.6	0286	39.2	26.7
4524	2840	14.9	20.5	145.93	XI 9	02632	0714	0550	0109	60.5	44.1	0258	45.6	29.2
4522	2818	13.6	19.0	121.28	XI 5	02157	0590	0454	0090	50.0	36.4	0239	35.1	21.5
4520	2819	11.4	18.3	138.76	"	02557	0684	0529	0057	62.7	47.2	0207	47.7	32.2
4518	2820	09.6	17.4	172.84	"	02080	0741	0548	0031	71.0	51.7	0181	56.0	36.7
4516	2821	08.1	15.8	191.12	"	01731	0763	0549	0009	75.4	54.0	0159	60.4	39.0
4514	2822	07.4	13.4	245.78	"	00423	0801	0526	979.	80.2	52.7	0149	65.2	37.7
4512	2823	05.4	12.6	278.18	"	99206	0779	0468	9970	80.9	49.8	0120	65.9	34.8
4510	2824	04.0	11.1	292.19	"	97366	0638	0311	9949	68.9	36.2	0099	53.9	21.2
4507	2825	01.1	09.4	211.71	"	98618	0515	0278	9907	60.8	37.1	0057	45.8	22.1
4505	2826	58.8	08.5	218.12	"	98772	0550	0306	9873	67.7	43.3	0023	52.7	28.3
4503	2827	56.7	07.5	227.58	"	98706	0573	0318	9842	73.1	47.6	979.	58.0	32.5
4501	2828	54.7	06.6	246.08	"	97807	0540	0265	9813	72.7	45.2	9964	57.6	30.1
4499	2829	54.7	04.1	273.98	"	96308	0476	0170	9813	66.3	35.7	9964	51.2	20.6
4497	2830	54.0	01.8	327.24	"	96306	0476	0170	"	66.3	35.7	"	51.2	20.6
						93600	0370	0004	9803	56.7	20.1	9954	41.6	5.0

Table XIV. (Continued)

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g	g <sub>0</sub> 980.	g <sub>0</sub> '' 980.	HELMERT Formula of 1901			International Formula		
									$\gamma_0$ 979.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 979.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)
4497	2835	37° 54.0	140° 01.8	327.24	XI 5	93601	0370	0004	9803	56.7	20.1	9954	41.6	5.0
4494	2831	52.1	139° 59.1	414.34	"	92702	0549	0085	9775	77.4	31.0	9926	62.3	15.9
4491	2832	49.7	140° 00.4	524.26	"	90319	0650	0063	9740	91.0	32.3	9891	75.9	17.2
4490	2833	48.7	00.0	570.28	"	89116	0672	0033	9726	94.6	30.7	9876	79.6	15.7
4489	2834	47.8	139° 59.6	648.17	"	87451	0745	0020	9713	103.2	30.7	9863	88.2	15.7

Synoptic Results for Yamagata Prefecture (IV).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g	g <sub>0</sub> 980.	g <sub>0</sub> '' 980.	HELMERT Formula of 1901			International Formula		
									$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 980.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)
3795	2847	38° 25.2	140° 25.3	160.15	XI 6	04306	0925	0746	0260	66.5	48.6	0409	51.6	33.7
3793	2848	24.8	27.9	235.04	"	03888	1114	0851	0254	86.0	59.7	0403	71.1	44.8
3791	2849	24.5	30.2	286.04	"	04057	1288	0968	0249	103.9	71.9	0399	88.9	56.9
"	2852	"	"	"	"	04067	1289	0969	"	104.0	72.0	"	89.0	57.0
3789	2850	23.7	32.4	371.00	"	02161	1361	0946	0238	112.3	70.8	0387	97.4	55.9
3787	2851	22.8	34.0	601.28	"	97735	1629	0956	0224	140.5	73.2	0374	125.5	58.2

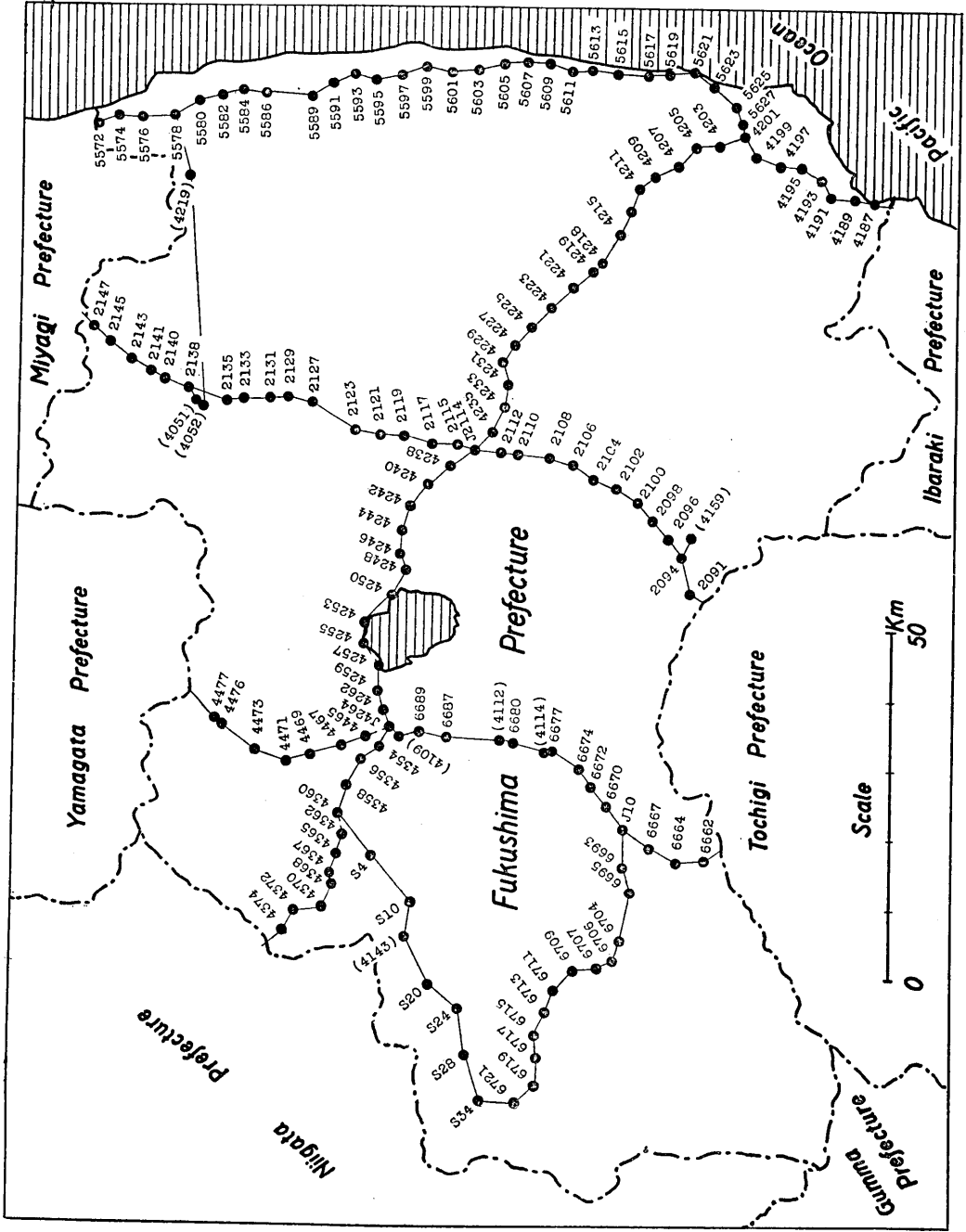


Fig. 15. Gravity Stations in Fukushima Prefecture.

(6) Fukushima Prefecture.  
Table XV. Synoptic Results for Fukushima Prefecture (I).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g 980.	g <sub>0</sub> 980.	g <sub>0</sub> '' 980.	HELMERT Formula of 1901			International Formula								
									$\gamma_0$ 979.	$\Delta g_0$ (mgal.)	$\Delta g_0'$ (mgal.)	$\gamma_0$ 979.	$\Delta g_0$ (mgal.)	$\Delta g_0'$ (mgal.)						
		36°	140°																	
4187	4186	51.8	47.5	10.31	VIII 3	03066	0338	0327	8899	143.9	142.8	9052	128.6	127.5						
4189	4185	53.8	47.9	2.25	"	03363	0343	0341	8928	141.5	141.3	9081	126.2	126.0						
4191	4184	55.8	48.0	7.71	"	03287	0353	0344	8957	139.6	138.7	9109	124.4	123.5						
4193	4183	57.0	49.8	24.51	"	02900	0366	0338	8974	139.2	136.4	9127	123.9	121.1						
4195	4182	58.6	50.8	26.72	"	03135	0396	0366	8997	139.9	136.9	9150	124.6	121.6						
		37°																		
4197	4181	00.4	50.9	13.61	"	04114	0453	0438	9023	143.0	141.5	9176	127.7	126.2						
4199	4180	02.1	51.7	11.67	"	04021	0438	0425	9048	139.0	137.7	9200	123.8	122.5						
J. 4201	4179	03.0	53.7	9.15	"	03578	0386	0376	9061	132.5	131.5	9213	117.3	116.3						
4203	4178	04.9	52.8	14.79	"	04582	0504	0487	9089	141.5	139.8	9241	126.3	124.6						
4205	4177	06.9	52.5	25.37	"	04377	0516	0488	9118	139.8	137.0	9270	124.6	121.8						
4207	4176	08.2	50.8	48.95	"	03933	0544	0490	9137	140.7	135.3	9289	125.5	120.1						
4209	4175	09.9	49.7	112.49	"	02533	0600	0475	9161	143.9	131.4	9313	128.7	116.2						
4211	4174	11.3	48.7	172.60	"	01077	0640	0447	9182	145.8	126.5	9333	130.7	111.4						
4213	4173	11.8	46.4	263.16	"	99473	0759	0465	9189	157.0	127.6	9341	141.8	112.4						
4215	4172	12.6	44.1	310.19	"	98592	0816	0469	9200	161.6	126.9	9352	146.4	111.7						
4218	4171	14.0	41.4	396.51	"	96933	0917	0473	9221	169.6	125.2	9372	154.5	110.1						
4219	4170	14.6	40.6	433.30	"	96159	0953	0468	9229	172.4	123.9	9381	157.2	108.7						
4221	4169	16.1	38.9	428.10	"	96425	0964	0465	9251	171.3	123.4	9403	156.1	108.2						
4223	4168	17.8	37.3	438.25	"	95980	0950	0460	9276	167.4	118.4	9427	142.3	103.3						
4225	4167	19.2	35.4	473.25	"	94683	0929	0399	9296	163.3	110.3	9448	148.1	95.1						
4227	4166	20.4	33.8	523.99	"	93009	0918	0332	9314	160.4	101.8	9465	145.3	86.7						
4229	4165	21.7	31.7	432.94	"	94499	0786	0302	9333	145.3	96.9	9484	130.2	81.8						
4231	4164	21.3	29.5	383.22	"	94615	0644	0215	9327	131.7	88.8	9478	116.6	73.7						
4233	4163	21.7	27.4	303.63	"	95886	0526	0186	9333	119.3	85.3	9484	104.2	70.2						
4235	4162	22.3	25.0	236.71	"	95534	0384	0119	9341	104.3	77.8	9493	89.1	62.6						

Table XV. (Continued)

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g	$g_0$	$g_0''$	HELMERT Formula of 1901			International Formula		
									$\gamma_0$ 979.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 979.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)
J.	2114	37° 24.0	140° 23.3	226.94	VIII 3	97409	0441	0187	9366	107.5	82.1	9517	92.4	67.0
	4238	25.5	21.7	253.68	VII 29	96493	0432	0148	9388	104.4	76.0	9539	89.3	60.9
	4240	27.3	20.2	264.95	"	96154	0433	0137	9414	101.9	72.3	9565	85.8	57.2
	4242	28.7	18.0	285.53	"	94022	0283	9964	9434	84.9	53.0	9586	69.7	37.8
	4244	29.3	15.7	334.84	"	93879	0421	0047	9443	97.8	60.4	9594	82.7	45.3
4246	29.5	13.1	421.35	"	92253	0526	0054	9446	108.0	60.8	9597	92.9	45.7	
4248	28.9	11.7	521.70	"	89942	0604	0020	9437	116.7	58.3	9588	101.6	43.2	
4250	29.4	09.1	517.79	"	88518	0450	9870	9445	100.5	42.5	9595	85.4	27.4	
4253	32.0	06.3	515.32	"	87953	0386	9809	9482	90.4	32.7	9634	75.2	17.5	
4255	31.8	03.7	517.46	"	88172	0414	9835	9479	93.5	35.6	9631	78.3	20.4	
4257	31.1	02.0	519.93	"	88723	0477	9895	9469	100.8	42.6	9620	85.7	27.5	
4259	31.0	59.5	509.77	"	88970	0470	9900	9468	100.2	43.2	9319	85.1	28.1	
4262	30.8	57.7	304.06	"	91918	0130	9790	9465	66.5	32.5	9616	51.4	17.4	
J.	4264	29.7	55.8	218.60	VII 30	92732	9948	9703	9449	49.9	25.4	9600	34.8	10.3
	4354	31.2	53.9	194.09	"	92671	9866	9649	9471	39.5	17.8	9322	24.4	2.7
	4356	32.9	52.2	183.96	"	92608	9829	9623	9495	33.4	12.8	9647	18.2	- 2.4
4358	33.5	49.7	176.95	"	92477	9794	9596	9504	29.0	9.2	9655	13.9	- 5.9	
4360	34.0	47.3	239.40	"	91170	9856	9588	9511	34.5	7.7	9663	19.3	- 7.5	
4362	33.2	45.7	212.46	"	91632	9819	9581	9500	31.9	8.1	9651	16.8	- 7.0	
4365	33.7	43.3	383.69	"	88909	0075	9646	9507	56.8	13.9	9658	41.7	- 1.2	

Synoptic Results for Fukushima Prefecture (II).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g	g <sub>0</sub>	g <sub>0</sub> ''	HELMERT Formula of 1901			International Formula			
									$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 979.	$\Delta g_0$ (mgal.)	$\gamma_0$ 979.	$\Delta g_0''$ (mgal.)	
	4367	4101	34.4	41.7	239.81	"	93153	0055 979.	9787	9517	53.8	27.0	9668	38.7	11.9
4368	4102	34.0	40.5	188.95	"	93693	9952	9741	9511	44.1	23.0	9663	28.9	7.8	
4370	4103	35.2	38.4	160.61	"	94518	9947 980.	9768	9529	41.8	23.9	9680	26.7	8.8	
4372	4104	37.2	38.1	155.00	"	96299	0108	9935	9558	55.0	37.7	9709	39.9	22.6	
4374	4105	37.9	36.2	163.49	"	96125	0117	9934	9568	54.9	36.6	9719	39.8	21.5	
		37°	140°												
5627	4189	03.2	54.9	8.28	VIII 4	03626	0388	0379	9064	132.4	131.5	9216	117.2	116.3	
5625	4190	04.1	57.2	3.93	"	03297	0342	0337	9077	126.5	126.0	9229	111.3	110.8	
5623	4191	05.7	59.0	3.38	"	03414	0352	0348	9100	125.2	124.8	9252	110.0	109.6	
			141°												
5621	4192	07.3	00.0	5.78	"	03105	0328	0322	9124	120.4	119.8	9276	105.2	104.6	
5619	4193	09.2	00.1	6.13	"	02545	0273	0267	9151	112.2	111.6	9303	97.0	96.4	
			140°												
5617	4194	10.9	59.9	15.82	"	03173	0366	0348	9176	119.0	117.2	9328	103.8	102.0	
			141°												
5615	4195	12.7	00.2	9.83	"	03180	0348	0337	9202	114.6	113.5	9354	99.4	98.3	
5613	4196	14.5	00.1	30.51	"	03378	0432	0398	9228	120.4	117.0	9380	105.2	101.8	
5611	4197	16.6	00.2	29.91	"	04818	0574	0541	9258	131.6	128.3	9410	116.4	113.1	
5609	4198	18.3	00.5	52.48	"	05104	0672	0514	9283	138.9	133.1	9435	123.7	117.9	
			140°												
5607	4199	20.1	00.8	13.68	"	06172	0659	0644	9309	135.0	133.5	9461	119.8	118.3	
5605	4200	22.0	00.7	26.84	"	05983	0681	0651	9337	134.4	131.4	9488	119.3	116.3	
5603	4201	23.8	00.3	45.60	"	05754	0716	0665	9363	135.3	130.2	9514	120.2	115.1	
5601	4202	25.8	00.1	23.07	"	06911	0762	0737	9392	137.0	134.5	9544	121.8	119.3	
5599	4203	27.8	00.7	8.84	"	07121	0739	0730	9421	131.8	130.9	9573	116.6	115.7	

Table XV. (Continued)

B.M.	No.	$\phi$	$\lambda$	H (m)	Date	g	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula		
									$\gamma_0$ 979.	$\Delta g_0'$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 979.	$\Delta g_0'$ (mgal.)	$\Delta g_0''$ (mgal.)
		37°	140°		1953	980.	980.	980.						
5597	4204	29.8	59.7	13.40	VIII 4	08056	0847	0832	9450	139.7	138.2	9602	124.5	123.0
5595	4205	31.5	59.3	9.64	"	08890	0919	0908	9475	144.4	143.3	9626	129.3	128.2
5593	4206	33.4	59.9	4.22	"	09744	0987	0983	9503	148.4	148.0	9654	133.3	132.9
5591	4207	35.1	59.0	16.47	"	10028	1054	1035	9528	152.6	150.7	9679	137.5	135.6
5589	4208	36.7	57.5	46.10	"	09097	1052	1000	9551	150.1	144.9	9702	135.0	129.8
5586	4209	39.8	57.9	37.49	"	09113	1027	0985	9596	143.1	138.9	9747	128.0	123.8
5584	4210	41.8	58.3	7.10	"	10061	1028	1020	9625	140.3	139.5	9776	125.2	124.4
5582	4211	43.7	57.3	17.40	"	10194	1073	1054	9653	142.0	140.1	9804	126.9	125.0
5580	4212	45.6	56.8	7.62	"	10752	1099	1090	9680	141.9	141.0	9831	126.8	125.9
5578	4213	47.5	55.6	7.98	"	10846	1109	1100	9708	140.1	139.2	9859	125.0	124.1
5576	4214	49.5	55.3	4.29	"	10798	1093	1088	9737	135.6	135.1	9888	120.5	120.0
5574	4215	51.7	55.4	14.72	"	10521	1098	1081	9769	132.9	131.2	9920	117.8	116.1
5572	4216	53.5	54.3	14.07	"	10234	1067	1051	9796	127.1	125.5	9946	112.1	110.5

Synoptic Results for Fukushima Prefecture (III).

B.M.	No.	$\phi$	$\lambda$	H (m)	Date	g	$g_0$ 980.	$g_0''$ 980.	HELMERT Formula of 1901			International Formula		
									$\gamma_0$ 979.	$\Delta g_0'$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 979.	$\Delta g_0'$ (mgal.)	$\Delta g_0''$ (mgal.)
		37°	140°		1953	979.	980.	980.						
2115	4071	25.2	23.7	232.12	VII 29	97536	0470	0210	9383	108.7	82.7	9535	93.5	67.5
2117	4070	27.2	23.5	249.50	"	97294	0499	0220	9413	108.6	80.7	9564	93.5	65.6
2119	4069	29.0	24.2	211.32	"	97185	0371	0134	9439	93.2	69.5	9590	78.1	54.4
2121	4068	31.0	24.5	207.89	"	97517	0393	0161	9468	92.5	69.3	9619	77.4	54.2
2123	4067	33.0	24.8	237.49	"	97733	0506	0240	9497	100.9	74.3	9648	85.8	59.2



2127	4066	35.9	27.4	199.91	"	99504	0567	0344	9539	102.8	80.5	9690	87.7	65.4
2129	4065	37.8	28.0	190.67	"	98877	0476	0263	9567	90.9	69.6	9718	75.8	54.5
2131	4064	39.6	28.0	184.49	"	980.	00143	0377	9593	99.1	78.4	9744	84.0	63.3
2133	4062	41.6	27.9	177.81	"	00140	0563	0364	9622	94.1	74.2	9773	79.0	59.1
2135	4061	43.5	27.7	70.23	"	02195	0436	0358	9650	78.6	70.8	9801	63.5	55.7
Fukushima	4052	45.4	28.5	67.30	VII 28	02215	0429	0354	9678	75.1	67.6	9828	60.1	52.6
2138	4053	46.2	29.2	62.21	"	01899	0382	0312	9689	69.3	62.3	9840	54.2	47.2
2140	4054	48.2	29.7	61.28	"	01645	0354	0285	9718	63.6	56.7	9869	48.5	41.6
2141	4058	49.1	30.3	62.06	"	02446	0436	0367	9732	70.4	63.5	9882	55.4	48.5
2143	4055	50.9	31.0	95.02	"	01917	0485	0379	9738	72.7	62.1	9908	57.7	47.1
2145	4056	52.6	33.1	73.15	"	02345	0460	0378	9783	67.7	59.5	9933	52.7	44.5
2147	4057	54.0	34.1	151.78	"	01880	0656	0487	9803	85.3	68.4	9954	70.2	53.3

\* Weather Station Bench Mark.

Synoptic Results for Fukushima Prefecture (IV).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g		$g_0$		HELMERT Formula of 1901		International Formula		
						979.	980.	980.	980.	$\gamma_0$ 979.	$\Delta g_0''$ (mgal.)	$\gamma_0$ 979.	$\Delta g_0''$ (mgal.)	
2112	4149	37° 22.0	140° 22.8	230.04	VIII 2	96942	0404	0147	9337	106.7	81.0	9488	91.6	65.9
2110	4150	19.9	22.7	234.64	"	96280	0352	0090	9306	104.6	78.4	9458	89.4	63.2
2108	4151	18.0	22.7	240.51	"	96364	0379	0110	9279	110.0	83.1	9430	94.9	68.0
2106	4152	16.2	21.9	269.76	"	95478	0380	0078	9253	112.7	82.5	9404	97.6	67.4
2104	4153	14.3	20.5	276.37	"	94619	0315	0005	9225	109.0	78.0	9377	93.8	62.8
2102	4154	12.5	19.8	288.25	"	94300	0320	979.	9199	112.1	79.8	9351	96.9	64.6
2100	4155	11.0	18.1	299.80	"	93565	0282	9946	9177	110.5	76.9	9329	95.3	61.7
2098	4156	09.8	16.5	311.86	"	94780	0440	0091	9160	128.0	93.1	9312	112.8	77.9
2096	4157	08.5	14.7	336.53	"	93037	0342	9966	9141	120.1	82.5	9293	104.9	67.3
2094	4158	07.5	13.1	357.02	"	91568	0259	9859	9126	113.3	73.3	9278	98.1	58.1
Shirakawa	4159	07.1	13.5	353.70	"	91359	0227	9832	9121	110.6	71.1	9273	95.4	55.9
W.S.*	3598	06.9	09.2	419.30	III 12	89572	0251	9782	9118	113.3	66.4	9270	98.1	51.2

\* Weather Station, Concrete Foot of the Shelter in the Observation Field.

Synoptic Results for Fukushima Prefecture (V).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g	$g_0$	$g_0''$	HELMERT Formula			International Formula			
									$\gamma_0$ 979.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 979.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	
		$37^\circ$	$139^\circ$		1953										
4465	4087	31.8	55.2	194.45	VIII 30	93007	9901	9683	9479	42.2	20.4	9631	27.0	5.2	
4467	4088	33.8	54.4	180.93	"	93348	9893	9691	9509	38.4	18.2	9660	23.3	3.1	
4469	4089	35.7	53.4	180.27	"	93350	9891	9690	9536	35.5	15.4	9687	20.4	0.3	
4471	4090	37.9	52.6	197.36	"	93272	9936	9716	9568	36.8	14.8	9719	21.7	0.3	
4473	4091	39.8	53.2	231.43	"	92806	9995	9736	9596	39.9	14.0	9747	24.8	1.1	
4476	4092	42.7	55.6	383.49	"	91242	980.	9879	9638	67.0	24.1	9789	51.9	9.0	
4477	4093	43.5	56.6	468.97	"	90096	0457	9932	9650	80.7	28.2	9801	65.6	13.1	

Synoptic Results for Fukushima Prefecture (VI).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g	$g_0$	$g_0''$	HELMERT Formula			International Formula		
									$\gamma_0$ 979.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 979.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)
		$37^\circ$	$139^\circ$		1953									
Wakamatsu W.S.*	4109	29.1	54.5	212.00	VIII 31	92707	9925	9688	9440	48.5	24.8	9591	33.4	9.7
6689	4110	27.3	55.5	230.91	"	92665	9979	9721	9414	56.5	30.7	9565	41.4	15.6
6687	4111	25.2	55.2	252.73	"	92930	0073	9790	9383	69.0	40.7	9535	53.8	25.5
6680	4113	19.6	55.4	370.07	"	90189	0161	9747	9302	85.9	44.5	9454	70.7	29.3
6677	4115	17.5	54.3	426.96	"	87824	0100	9622	9272	82.8	35.0	9423	67.7	19.9
6674	4116	15.5	52.3	466.91	"	86514	0092	9570	9243	84.9	32.7	9394	69.8	17.6
6672	4117	14.0	50.6	496.78	"	86109	0144	9588	9221	92.3	36.7	9372	77.2	21.6
6670	4118	13.0	48.6	522.69	"	85873	0200	9615	9206	99.4	40.9	9358	84.2	25.7
J.	6677	11.9	46.3	550.96	"	84678	0168	9552	9190	97.8	36.2	9342	82.6	21.0
6667	4120	09.8	44.7	599.10	"	83660	0215	9544	9160	105.5	38.4	9312	90.3	23.2
6664	4121	07.0	43.1	652.65	"	80861	0100	9370	9119	98.1	25.1	9271	82.9	9.9
6662	4122	05.1	43.8	736.14	"	78665	0138	9315	9092	104.6	22.3	9244	89.4	7.1

\* Weather Station, Nail of the Shelter No. 1.

Synoptic Results for Fukushima Prefecture (VII).

B.M.	No.	$\varphi$	$\lambda$	H (m)	Date	g	$g_0$	$g_0''$	HELMERT Formula of 1901			International Formula			
									$\gamma_0$ 979.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	$\gamma_0$ 979.	$\Delta g_0$ (mgal.)	$\Delta g_0''$ (mgal.)	
		37°	139°												
6693	4126	11.8	42.4	591.91	VII 31	83705	0197	9535	9189	100.8	34.6	9341	85.6	19.4	
6695	4127	11.3	40.0	694.54	"	79979	0141	9364	9182	95.9	18.2	9333	80.8	3.1	
6704	4128	11.8	35.4	736.11	"	78871	0159	9335	9189	97.0	14.6	9341	81.8	0.6	
6706	4129	12.7	33.3	579.19	"	82491	0037	9388	9202	83.5	18.6	9354	68.3	3.4	
6707	4130	13.3	32.7	527.12	"	83795	0006	9416	9211	79.5	20.5	9362	64.4	5.4	
6709	4132	15.5	32.7	500.90	VIII 1	84588	0005	9444	9243	76.2	20.1	9394	61.1	5.0	
6711	4133	16.9	30.9	473.99	"	85174	9980	9450	9263	71.7	18.7	9414	56.6	3.6	
6713	4134	17.6	28.5	452.72	"	86358	0033	9526	9273	76.0	25.3	9425	60.8	10.1	
6715	4135	18.5	26.3	441.91	"	87085	0072	9578	9286	78.6	29.2	9438	63.4	14.0	
6717	4136	18.2	23.7	411.16	"	87834	0052	9592	9282	77.0	31.0	9433	61.9	15.9	
6719	4137	18.3	21.6	395.16	"	88252	0045	9603	9283	76.2	32.0	9435	61.0	16.8	
6721	4138	19.7	19.7	377.01	"	88947	0058	9636	9303	75.5	33.3	9455	60.3	18.1	
Sei 34	4139	22.3	19.7	362.79	"	89285	0048	9642	9341	70.7	30.1	9493	55.5	14.9	
Sei 28	4140	23.6	24.1	336.10	"	90427	0080	9704	9360	72.0	34.4	9512	56.8	19.2	
Sei 24	4141	24.0	28.5	322.72	"	90205	0016	9655	9366	65.0	28.9	9517	49.9	13.8	
Sei 20	4142	26.8	30.9	303.36	"	90366	9973	9633	9407	56.6	22.6	9558	41.5	7.5	
Sei 10	4144	28.2	39.1	244.04	"	92162	9969	9696	9427	54.2	26.9	9578	39.1	11.8	
Sei 4	4145	31.4	43.5	198.78	"	92278	9841	9619	9474	36.7	14.5	9625	21.6	- 0.6	

B.M. Printed in Gothic Type are 2nd Order Bench Marks.

## ウォルドン重力計による日本全国の重力測定

## 第七報 東北地方

坪井忠二・実川 顕・田島広一

これは、東北地方 667 点における重力測定結果をまとめたものである。測定と計算との方法は、第一報に述べてあるのとほとんど同じであるから、ここにはくりかえさない。結果は第 III 表～第 IX 表（ルート別）、第 X 表～第 XV 表（県別）に示してある。ブーゲー異常の分布は、第 4 図にくわしく示してある。第 5 図はその略図である。

これらの図からわかる主なことがらは、次のとおりである。

- 1)  $\Delta g_0''$  は、東北地方全般にわたってプラスである。このことは、地殻が薄いことを意味する。
- 2)  $\Delta g_0''$  は東方に増加する。その増加の割合は、北上、阿武隈両山地と奥羽山脈との間にある低部において特に大きく、 $20 \times 10^{-9}$  に達する。この  $\Delta g_0''$  急変の線は東北地方から南に下り、関東地方に入り、その略中央で急にむきをかえて東に走る。この重要な線を盛岡・白河線と名付ける。この場所の地下構造は第 7 図又は第 8 図のようなものであろう。第四紀以後の火山がこの線に並行して配列し、また地震がこの線の東側に多く発生していることは興味深い。北上・阿武隈両山地は、一つづきのものらしい。
- 3) 盛岡・白河線の西側では、等異常線が乱れている。これはこの地帯に散在する若い地層の影響であると思われる。